

NASA/TM—2000-107479



Flow Quality Studies of the NASA Glenn Research Center Icing Research Tunnel Circuit (1995 Tests)

E. Allen Arrington and Jose C. Gonsalez
NYMA, Inc., Brook Park, Ohio

Bonnie A. Kee-Bowling
Glenn Research Center, Cleveland, Ohio

The NASA STI Program Office . . . in Profile

Since its founding, NASA has been dedicated to the advancement of aeronautics and space science. The NASA Scientific and Technical Information (STI) Program Office plays a key part in helping NASA maintain this important role.

The NASA STI Program Office is operated by Langley Research Center, the Lead Center for NASA's scientific and technical information. The NASA STI Program Office provides access to the NASA STI Database, the largest collection of aeronautical and space science STI in the world. The Program Office is also NASA's institutional mechanism for disseminating the results of its research and development activities. These results are published by NASA in the NASA STI Report Series, which includes the following report types:

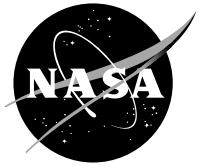
- **TECHNICAL PUBLICATION.** Reports of completed research or a major significant phase of research that present the results of NASA programs and include extensive data or theoretical analysis. Includes compilations of significant scientific and technical data and information deemed to be of continuing reference value. NASA's counterpart of peer-reviewed formal professional papers but has less stringent limitations on manuscript length and extent of graphic presentations.
- **TECHNICAL MEMORANDUM.** Scientific and technical findings that are preliminary or of specialized interest, e.g., quick release reports, working papers, and bibliographies that contain minimal annotation. Does not contain extensive analysis.
- **CONTRACTOR REPORT.** Scientific and technical findings by NASA-sponsored contractors and grantees.

- **CONFERENCE PUBLICATION.** Collected papers from scientific and technical conferences, symposia, seminars, or other meetings sponsored or cosponsored by NASA.
- **SPECIAL PUBLICATION.** Scientific, technical, or historical information from NASA programs, projects, and missions, often concerned with subjects having substantial public interest.
- **TECHNICAL TRANSLATION.** English-language translations of foreign scientific and technical material pertinent to NASA's mission.

Specialized services that complement the STI Program Office's diverse offerings include creating custom thesauri, building customized data bases, organizing and publishing research results . . . even providing videos.

For more information about the NASA STI Program Office, see the following:

- Access the NASA STI Program Home Page at <http://www.sti.nasa.gov>
- E-mail your question via the Internet to help@sti.nasa.gov
- Fax your question to the NASA Access Help Desk at (301) 621-0134
- Telephone the NASA Access Help Desk at (301) 621-0390
- Write to:
NASA Access Help Desk
NASA Center for AeroSpace Information
7121 Standard Drive
Hanover, MD 21076



Flow Quality Studies of the NASA Glenn Research Center Icing Research Tunnel Circuit (1995 Tests)

E. Allen Arrington and Jose C. Gonsalez
NYMA, Inc., Brook Park, Ohio

Bonnie A. Kee-Bowling
Glenn Research Center, Cleveland, Ohio

National Aeronautics and
Space Administration

Glenn Research Center

When this testing was done, the NASA Glenn Research Center was known as the NASA Lewis Research Center. The new name, NASA John H. Glenn Research Center at Lewis Field, became official on March 1, 1999.

Available from

NASA Center for Aerospace Information
7121 Standard Drive
Hanover, MD 21076
Price Code: A08

National Technical Information Service
5285 Port Royal Road
Springfield, VA 22100
Price Code: A08

FLOW QUALITY STUDIES OF THE NASA GLENN¹ RESEARCH CENTER ICING RESEARCH TUNNEL CIRCUIT (1995 TESTS)

E. Allen Arrington and Jose C. Gonzalez
NYMA, Inc.
Brook Park, Ohio 44142

Bonnie A. Kee-Bowling
National Aeronautics and Space Administration
Glenn Research Center
Cleveland, Ohio 44135

SUMMARY

The purpose of conducting the flow-field surveys described in this report was to more fully document the flow quality in several areas of the tunnel circuit in the NASA Glenn Research Center Icing Research Tunnel. The results from these surveys provide insight into areas of the tunnel that were known to exhibit poor flow quality characteristics and provide data that will be useful to the design of flow quality improvements and a new heat exchanger for the facility.

An instrumented traversing mechanism was used to survey the flow field at several large cross sections of the tunnel loop over the entire speed range of the facility. Flow-field data were collected at five stations in the tunnel loop, including downstream of the fan drive motor housing, upstream and downstream of the heat exchanger, and upstream and downstream of the spraybars located in the settling chamber upstream of the test section. The data collected during these surveys greatly expanded the data base describing the flow quality in each of these areas. The new data matched closely the flow quality trends recorded from earlier tests. Data collected downstream of the heat exchanger and in the settling chamber showed how the configuration of the folded heat exchanger affected the pressure, velocity, and flow angle distributions in these areas. Smoke flow visualization was also used to qualitatively study the flow field in an area downstream of the drive fan and in the settling chamber/contraction section.

INTRODUCTION

Detailed flow-field surveys were conducted throughout the tunnel loop of the NASA Glenn Icing Research Tunnel to augment the existing data base on flow quality. These measurements were necessary because in several areas of the tunnel loop there were either known or suspected flow quality problems. Limited data were available from several locations in the tunnel loop, but gaps in the data set restricted the usefulness of these data in answering questions pertaining to facility design for improved flow quality. The data collected during the surveys described in this report were intended to fill the gaps in the existing data base.

Figure 1 shows the six areas of the tunnel loop where flow quality studies were conducted: downstream of the fan, downstream of the drive motor housing, upstream and downstream of the facility heat exchanger, and upstream and downstream of the spraybars, which are located in the settling chamber upstream of the test section. Flow-field measurements were made at five stations around the tunnel circuit by using instrumented plates riding on cables, and flow visualization tests were conducted at two tunnel stations. Each of the stations was the site of multiple surveys with the instrumented plates; at four stations vertical surveys were made, and at three stations horizontal surveys were made. The instruments mounted on the plates sensed the total and static pressures, total temperature, airspeed, flow direction, and turbulence levels. These data provided very detailed quantitative information about the flow field at each station surveyed. Smoke flow visualization provided qualitative data both on the flow field downstream of the fan, where earlier studies indicated poor flow quality, and on the flow field in the settling chamber upstream of the test section.

There was a major concern about the effect of the facility heat exchanger on the overall flow quality in the tunnel. Figure 2 shows an elevation view of the facility primary heat exchanger. The folded design of the heat

¹When this testing was done, the NASA Glenn Research Center was known as the NASA Lewis Research Center. The new name, NASA John H. Glenn Research Center at Lewis Field, became official on March 1, 1999.

exchanger increases the area available for cooling, which is required to create the cold static temperatures needed to produce icing conditions. There are three folds in the main heat exchanger. At each fold, contoured fairings are used to house coolant supply and return piping, thereby reducing the total pressure loss of the heat exchanger. Although the heat exchanger is absolutely necessary to produce the low temperatures needed for icing simulations, it does degrade the aerodynamic flow quality of the facility (ref. 1). In addition to documenting the existing flow quality at these stations in the tunnel loop, we conducted a sensitivity study to determine the effect of the heat exchanger's turning vanes on the flow downstream from the heat exchanger. A symbols list is provided in appendix A to aid the reader.

DESCRIPTION OF FACILITY

The NASA Glenn Research Center Icing Research Tunnel (IRT) is a closed-loop atmospheric tunnel with rectangular cross sections. The airflow is driven by a 25-ft-diameter 12-blade fan that is powered by a 5000-hp electric motor. The tunnel test section is 6-ft high, 9-ft wide, and 20-ft long. The velocity in an empty test section can be varied from 50 to 400 mph (Mach number range of 0.065 to 0.56) at 0 °F. A schematic of the tunnel is shown in figure 1. A 2100-ton heat exchanger (cooler) located in the tunnel leg between corners C and D is used to control the tunnel air temperature. The heat exchanger (see fig. 2) has been designed with folds to increase the amount of cooling area available. Fairings at the heat exchanger folds house inlet and outlet piping for the coolant. A set of eight horizontally oriented spraybars, located upstream of the test section, inject atomized water into the airflow to create icing conditions (no icing conditions were studied in these tests). A complete description of the facility can be found in reference 2.

INSTRUMENTATION AND TEST HARDWARE

Flow-Field Surveys

Several different types of flow-sensing probes were used during the flow-field surveys, including pitot-static probes, thermocouples, hot-wire anemometry probes, and wind anemometers. A traversing plate mechanism was used to position the probes at any point along a particular survey plane. The survey planes studied during these surveys are shown in figure 1. The traversing plate mechanism and each of the probe types are described in the following paragraphs.

Pressure probes.—Standard pitot-static probes were used to sense the total and dynamic pressures. Two pitot-static pressure probes were mounted on each traversing plate. Originally, the pressure probes were on supports that moved the probe heads well off to the sides of the plates to allow for measurements closer to the tunnel surfaces. These probes were replaced with probes that extended directly forward of the plate. This change was made because we felt that the smaller probes might enhance the stability of the plate in the airflow. The transducers used to measure the total and dynamic pressures were mounted on the tunnel floor at the survey station to reduce the length of the pressure tubing. Absolute transducers (0- to 25-in. H₂O range) were used for the total pressure measurements, and differential pressure transducers were used for the dynamic pressure measurements. (Transducers in the 0- to 1-in. H₂O range were used for the first run; all subsequent runs used transducers in the 0- to 5-in. H₂O range.)

Thermocouples.—One Chromel-Alumel (type K) aspirated thermocouple was mounted on each traversing plate to measure the total temperature distribution. Such thermocouples are accurate to ±1 °R.

Wind anemometers.—Vane wind anemometers were used to measure airspeed and two components of flow angle. (A typical wind anemometer is shown in fig. 3.) The wind anemometers were calibrated for airspeed and flow angle prior to the tunnel tests. Linear calibration relationships were used to convert the output from the anemometers directly to engineering units. These instruments are accurate to within ±3.28 ft/sec in airspeed, ±0.35° in pitch angle, and ±0.25° in yaw angle.

Hot-wire anemometry.—Hot-wire anemometry was used to measure the mean airspeed, turbulence levels, and flow direction. Commercially available hot-wire probes (one- and two-component probes), constant temperature anemometers, signal conditioners, and a 12-bit analog-to-digital converter were used. A personal computer with commercially available software controlled the data acquisition and carried out the subsequent data reduction.

Traversing plates.—For obtaining velocity and pressure distribution data across the large sections of the tunnel, a traversing plate mechanism was used. This apparatus consisted of a flat plate supported by cables at the leading

and trailing edges. The cables were attached to channels that were mounted to the tunnel walls. The leading edge cable rode on a pulley driven by a remotely controlled electric motor, so the plate could be positioned at any point across the tunnel. The traverses were operated along both horizontal and vertical surveys. Two traversing plate setups were used simultaneously at each tunnel-loop area surveyed during these studies. Figure 4 shows this apparatus installed downstream of the spraybars in the settling chamber (survey station 5). Two different instrumentation layouts were used for the traversing surveys (see fig. 5), depending on the type of pitot-static probe used. Configuration 1 was used for surveys made downstream of the heat exchanger (station 3) and for some surveys upstream of the spraybars (station 4); configuration 2 was used for all other surveys.

Data system.—Real-time data acquisition and display were provided by Escort D+, the standard data system used in the large test facilities at the NASA Glenn Research Center. This system was used to record the signals from all steady-state analog signals (all pressure transducers, thermocouples, wind anemometers, traverse controls, and tunnel parameters; hot-wire anemometry data were collected by using a separate system, as described previously). The Escort D+ facility microcomputer acquires the data, converts the data to engineering units, executes performance calculations, checks limits on selected channels, and displays the information in alphanumeric and graphical form at a rate of 1 update/sec. For this test, each collected data reading was the average of 20 scans (20 sec) of data.

Flow Visualization

A commercially available hand-held smoke wand system was used to manually place smoke into the airstream for visualization purposes. In this system, liquid propylene glycol is heated to form a superheated vapor, which is forced through an 8-ft-long wand. The vapor condenses to form a viable cloud when it is discharged from the nozzle at the end of the wand. This smoke-generating system permitted visualization of the flow field around the drive motor housing and in the settling chamber upstream of the test section.

TEST PROCEDURES

Prior to the start of the test entry, the hot-wire probes and wind anemometers were calibrated over the expected operating range by using the free-jet calibration rig in cell CE-12 of the Engine Research Building. During installation of the traversing hardware, all appropriate measurements were made to determine the position of the probes during the surveys. Prior to each run, the traversing plate position was calibrated. A simple two-point calibration relating distance from the reference surface (as measured by a tape measure) to the output voltage was used. For vertical surveys, the traverse position was referenced to the tunnel floor; for horizontal surveys, the inside tunnel wall was the reference. The pressure transducers were also zeroed prior to each run (the delta pressure transducer output was set to zero, and the absolute pressure transducer output was set to match the barometric reference pressure).

The test matrix for the flow quality surveys is given in table 1. The order in which the surveys were made can be inferred from the run number column: the first surveys were conducted downstream of the heat exchanger and the last were downstream of the spraybars. (The testing priority was based on the need for the data.) For each test run, the tunnel total temperature was held constant at 40 °F (500 °R). All tests were conducted with an empty test section (no blockage in the test section). No air or water sprays were used during these surveys. Each survey was conducted at airspeed conditions based on test section velocities V_{TS} of 350, 250, 150, and 50 mph (only the data for 350 and 250 mph are presented in this report). Typical test section conditions are listed in table 2. At most of the survey stations, two surveys were made. For the first, the traverse was stopped at discrete points along the survey line, and data were collected from all the instrumentation at each point. The second was a continuous motion survey in which data were collected from only the hot-wire instrumentation. For most test runs, the discrete point surveys were conducted first, starting at the highest test section velocity then stepping down through the velocity schedule. The continuous surveys were conducted next, starting at the lowest velocity setting and stepping up through the range. Data were collected in both directions across the survey line (i.e., from floor to ceiling and back to the floor for a vertical survey). For the discrete point surveys, data were collected every 6 to 12 in. along the initial survey and then in 18- to 36-in. increments along the return survey. One data reading was collected at each survey increment (20 sec of data were averaged for each data reading). For each survey, about 50 data readings were collected. All data were monitored online with the Escort D+ displays. A detailed log was maintained to track any data anomalies that occurred during the testing.

DATA REVIEW AND REDUCTION

The first step of the data analysis process was to review the quality of the collected data. This was done by reviewing graphical output and tabular listings of the data. Any anomalies were noted and investigated. If the cause for the anomaly could be determined and corrected, the appropriate modifications were made in the data analysis software; otherwise, the questionable data were not used in any further analysis. The only major anomaly that was found during the data review was the mismatch of the total pressure levels sensed by the two probes on each traverse. The difference in pressure levels was too small to detect during the data collection. Since the primary intent of the test was to determine the flow quality in the tunnel loop, the data trends—not the absolute values of the data—were of greater importance. In order to better understand the data trends, the measurement offset of one pressure measurement was adjusted so that the absolute pressure levels sensed by the two probes were the same. In doing this, one continuous data trace was created with the data from the two pressure probes. This greatly simplified the task of analyzing the pressure distributions at each station. The offsets were generally small, on the order of 0.010 to 0.020 psia, although larger offsets were required in some cases. Probe 1 readings were used as the reference pressure, and probe 2 data were adjusted to match (there was only one exception to this rule). The differences were probably due to incorrectly setting the transducer offsets prior to each test run and due to temperature changes in the tunnel during the testing (the transducers were mounted inside the tunnel for each test). These small changes to the total pressure levels had no effect on the remaining data analysis. However, the total pressure levels at different traverse positions cannot be compared to determine gradients at a station, nor can data from different stations be compared to determine losses through the tunnel loop.

Static pressure was calculated from the measured total and differential pressures from the following equation:

$$P_s = P_o - \Delta P \quad (1)$$

The Mach number was then determined from the ratio of static to total pressure (eq. (44) from ref. 3) by using $\gamma = 1.4$:

$$M = \sqrt{5 \left[\left(\frac{P_s}{P_o} \right)^{-0.2857} - 1 \right]} \quad (2)$$

Velocity was determined by using the definition of Mach number, $M = V/a$, where a is the speed of sound ($a = (\gamma R T_s)^{0.5}$). The static temperature T_s was calculated by using the following relation (eq. (43) from ref. 3):

$$T_s = \frac{T_o}{1 + 0.2M^2} \quad (3)$$

For any one data point (reading), there were two sets of pressure measurements (one from each of the two pitot-static probes mounted on each traverse) and one temperature measurement. The instrumentation was configured such that the thermocouple was about midway between the two pressure probes, so the one temperature measurement was used in the calculation of velocity at both pressure probe positions. The local velocity was then determined by using

$$V = M \cdot a \quad (4)$$

The output from the thermocouples and wind anemometers was converted to engineering units via calibration curves. The absolute value of the flow angles measured by the wind anemometers was slightly affected by the angle of the plate, however the trends indicated by the data were not.

The hot-wire probes were calibrated in a free jet prior to use in the IRT. The calibration curves related the mean airspeed to the voltage output of the hot-film probe. Once the calibration curves were generated, they were used to transform the raw bridge voltage data into unsteady velocity data. Means and standard deviations of the unsteady velocity data were then computed. Turbulence intensity was computed from these statistical quantities:

$$\bar{u} = \frac{\sum_{i=1}^N u_i}{N} \quad \sigma_u = \frac{\sqrt{\sum(u_i - \bar{u})}}{N-1} \quad TI_u = \frac{\sigma_u}{\bar{u}} - 100\% \quad (5)$$

DISCUSSION OF RESULTS

Flow-Field Surveys

Flow quality measurements were made at stations 2 through 6, as illustrated in figure 1, around the tunnel circuit of the Icing Research Tunnel. At each station, surveys were made across the tunnel cross section in order to document the total and static pressure, total temperature, airspeed, flow direction, and turbulence levels over the operating speed range of the facility. The data collected and the results of the data analysis at each station are discussed in the sections that follow. The data presented in this section—that is, the total and static pressures and total temperature—were normalized by the corresponding test section condition. Because the transducers were placed inside the tunnel, the transducer zeros drifted, so some of the pressure data indicated unreasonable pressure levels (slightly higher total pressures); however, these had only a small effect on the data set, and the overall data trends were unaffected. Only data corresponding to test section airspeeds of 350 and 250 mph are presented in this report (data at 150 and 50 mph are not included). This decision was made primarily for brevity, in that the data trends recorded at the high-speed conditions were also seen at the lower speed conditions and because some of the instrumentation (generally the wind anemometers and in some cases the pitot-static probes) did not always operate reliably at the low airspeeds encountered in the tunnel loop at $V_{TS} = 150$ or 50 mph. A listing of all collected readings is contained in appendix B. Appendix C has tabular listings of flow-field survey data for the 250 and 350 mph V_{TS} conditions.

Station 2: Downstream of the fan drive motor housing.—Two vertical and two horizontal surveys were made downstream of the drive motor housing. The survey plane was approximately 23.75 ft downstream of the aft end of the housing. The tunnel at the survey plane is 29.17-ft wide by 26.17-ft high. The traverse locations were at intervals approximately one-third the tunnel dimension; the vertical surveys were made at 9.46 and 19.52 ft from the south (inside) tunnel wall, and the horizontal surveys were made at 8.69 and 17.5 ft above the tunnel floor. All surveys were made under standard tunnel operating conditions and with the standard configuration.

The total pressure data along the station 2 vertical surveys are shown in figure 6. These data show a fairly uniform pressure profile over the upper half to two-thirds of the survey, but they indicate a high-pressure region at the lower portion of this station. The effect is more evident at the traverse location nearer the inside tunnel wall. The high-pressure region decreases with decreasing airspeed. Figure 7, which presents the static pressure data along the vertical surveys at station 2, shows a fair amount of data scatter at the $V_{TS} = 350$ mph setting, probably because the transducers are located inside the tunnel. These data indicate that there is a static pressure gradient in the vertical plane, with the higher pressures occurring near the ceiling.

Figure 8 contains the velocity data from the pressure probes along the vertical surveys at station 2. The reason for the discrepancy between the total pressure and velocity levels measured by the two probes on traverse 1 is not known. These data show that there is a large velocity gradient in the vertical plane, with lower airspeeds closer to the tunnel ceiling. This result is consistent with the trends shown by the total and static pressure data. The gradient is more severe closer to the inside tunnel wall.

Velocity measured by the wind anemometer is shown in figure 9. These data match the pressure probe data very closely in both magnitude and trend, confirming the strong negative gradient from floor to ceiling. Comparison of the pressure probe data and wind anemometer data from traverse 1 shows that the results from the pressure probe closer to the inside tunnel wall (probe 2 for this configuration) and those from the wind anemometer closely agree at all conditions. (This implies that the difference in the airspeeds measured by pressure probes 1 and 2 on traverse 1 was due to some problem associated with probe 1, which makes the data from that probe suspect for this configuration.)

Total temperature data along the vertical surveys at station 2 are given in figure 10. In general, these data show a uniform temperature profile in the vertical plane with variations of less than 2 °R, although there was a 4 °R gradient measured near the inside tunnel wall at the $V_{TS} = 350$ mph setting (higher temperatures were measured near the tunnel floor).

For a better understanding of the flow angularity data downstream of the drive motor housing, where the effects of the fan rotation are very prominent, see the definitions of the expected flow direction components in figure 11.

Positive pitch flow angle is defined as upflow, and positive yaw (crossflow) angle is defined as flow from the inside to the outside tunnel wall. Figure 12 shows the pitch flow angle along the vertical surveys at station 2. The expected distribution would be pitch angles that are larger near the midpoint of the vertical surveys than near the tunnel floor or ceiling. Downward flow (negative pitch angles) would be expected along the inside tunnel wall (traverse 1) with upflow (positive pitch angles) along the outside tunnel wall (traverse 2). This is the general trend indicated by the data, although traverse 1 data does indicate positive pitch flow angles (this could be due to the angle of incidence of the traverse plate, which was not measured or otherwise accounted for in the data reduction).

The yaw flow angle distributions along the vertical surveys at station 2 are given in figure 13. The data show that there is a negative yaw angle along the upper portion of the survey (flow from outside to inside wall), a positive yaw flow angle along the lower portion of the survey, and a 0° yaw angle at the center of the survey for all test conditions. These results are consistent with yaw angle expectations based on the swirl produced by the fan rotation. The maximum yaw angle recorded was approximately 10° in both the positive and negative directions. The data also indicate more of a gradient in yaw angle along the upper portion of the surveys; along the lower portion the distribution is more uniform. The difference in the shape of the distribution above and below the centerline may be due to the drive motor housing supports, which may straighten the flow somewhat below the centerline.

Results from the hot-wire anemometry measurements are presented in figures 14 through 18. Figure 14 shows the mean axial velocity distribution measured by the hot-wire probes along the vertical surveys made at station 2. These data agree very well in magnitude and trend with the velocities recorded by the pressure probes and wind anemometer. Figure 15 shows that the vertical velocity gradient is apparent for all test conditions, that the gradient is more pronounced along the inside wall traverse, and that higher mean velocities were recorded nearer the inside tunnel wall.

The pitch flow angles measured by the hot-wire probes are presented in figure 16. Again, these data closely agree with the wind anemometer pitch flow angle data in both magnitude and distribution. The axial turbulence intensity for this test configuration is given in figure 17, which shows that axial turbulence intensity increases with distance from the tunnel floor (the local velocity at this station decreases with distance from the tunnel floor). The axial turbulence varies from about 10 percent near the floor to as high as 30 percent toward the ceiling. Also, slightly higher axial turbulence levels were recorded along traverse 2, nearer the outside tunnel wall (lower velocities were recorded along traverse 2 than along traverse 1). Similar trends were seen for turbulence levels in the vertical direction for these surveys (fig. 18). These trends are due to the disturbances caused by the drive motor housing and to the poor airflow distribution out of the fan along the outside tunnel wall.

Figures 19 and 20 show the total and static pressure ratio distributions, respectively, for the horizontal surveys made downstream of the drive motor housing. The data from traverse 1 (upper survey) indicate a fairly uniform total pressure distribution across the tunnel for all the conditions; however, traverse 2 (lower survey) data indicate uniform total pressure distributions only for the $V_{TS} = 150$ and 50 mph settings. At the $V_{TS} = 350$ and 250 mph settings, higher total pressure levels were recorded along the inside half of the survey. At the $V_{TS} = 350$ mph setting, the data show a higher total pressure region along the lower traverse between 100 and 200 in. from the inside tunnel wall. The static pressure distributions show fairly uniform distributions (variations on the order of 0.010 psia), although there is a slight static pressure gradient at the $V_{TS} = 250$ mph setting, with higher static pressures nearer the inside tunnel wall (the data scatter at the $V_{TS} = 350$ mph setting masks any trend in the distribution).

The pressure probe velocity data from the horizontal surveys are given in figure 21.² The data indicate that the airspeed is much higher along the inside half of the survey plane, especially for traverse 2 (lower survey). The velocity peak at about 140 in. from the inside tunnel wall corresponds to the position of the high total pressure levels shown in figure 19. This high velocity is probably due to the presence of the drive motor housing supports. The low velocities recorded near the outside tunnel wall confirm results from past studies (ref. 1) and the current flow visualization. The wind anemometer velocity data (fig. 22) agree closely with the pressure probe velocity data in both trend and magnitude. Comparison of the wind anemometer data and pressure probe data on traverse 1 shows that pressure probe 2 and the wind anemometer agree (as was the case for the vertical surveys at this station; data from probe 1 is considered suspect).

The horizontal total temperature distributions (fig. 23) indicate a gradient across the tunnel, with higher temperatures recorded near the inside tunnel wall. The gradient is most evident at the $V_{TS} = 350$ mph setting, where a 3° gradient was recorded for traverse 2 (lower survey) and a 2° gradient for the upper traverse. The magnitude of the gradient decreases with decreasing velocity.

²As a check of the data quality, the velocities measured along the vertical and horizontal surveys were compared where the survey lines intersected. For all cases checked, the velocity readings agreed to ± 1 ft/sec or better.

Pitch and yaw flow angle data are presented in figures 24 and 25, respectively. The fan rotation was expected to induce a swirl to the flow that would produce a negative pitch component (downflow) along the inside portion of the survey and a positive (upflow) pitch component along the outside portion of the survey (fig. 11). Thus, the pitch angle distribution would vary from large flow angles near the tunnel walls to 0° angles near the center of the survey. The pitch angle data indicate this trend for the inside portion of the survey, with large negative pitch angles near the inside tunnel wall and the magnitude of the pitch angle gradually approaching zero near the center of the tunnel. However, the pitch angle does not continue to increase to a large positive value over the outside portion of the survey. Along this part of the survey, the pitch angle remains constant or decreases slightly.

In the horizontal surveys, the yaw angle was expected to remain virtually constant—with higher angles near the tunnel centerline, negative angles along traverse 1 (upper survey), and positive angles (outflow) along traverse 2 (lower survey). The data (fig. 25) indicate that such is the case, although at all test conditions, the yaw angles recorded along the inside portion of the surveys were higher than those along the outside portion for both traverses. The fact that both the pitch and yaw data in the outside half of the tunnel downstream of the drive motor housing did not indicate flow angles that follow the swirl induced by the fan is an indication of low flow quality in that area. The flow angle data from the horizontal surveys indicate reversed flow at some points between the drive motor housing and the outside wall.

Results from the hot-wire probe measurements along the horizontal surveys at station 2 are given in figures 26 through 30. The mean axial velocity data (fig. 26) agree with the pressure probe and wind anemometer data in both magnitude and trend (for traverse 1, the hot-wire data agree with pitot-static probe 2, as does the wind anemometer). The three sets of independent velocity data all show that there was a definite deficit region toward the outside of the tunnel, most likely caused by the drive motor housing supports blocking the whirl flow. The yaw flow angle measurements by the hot-wire probes along the horizontal surveys (fig. 28) provide a clear presentation of the yaw angle for this configuration. These data, which also agree with the wind anemometer flow angle data for both traverses in all test cases, show positive angles (outflow) along the lower traverse (traverse 2) and negative angles (inflow) for the upper traverse (traverse 1) between the inside wall and the drive motor housing. Between the drive motor housing and the outside tunnel wall, the data from both traverses reveal a change in the flow direction that the fan swirl would be expected to induce; this is indicative of poor flow quality.

Figure 29 shows the axial turbulence intensity for the horizontal surveys. The turbulence levels are the same for the $V_{TS} = 350$ and 250 mph test conditions. For both the upper and lower traverses, the turbulence levels along the inside portion of the survey are about 20 percent for all test conditions (slightly less for the lower traverse), but then they increase beyond the drive motor housing to 30 percent near the outside tunnel wall. This is another indication of the poor flow quality in that area of the tunnel. The crossflow turbulence intensity data (fig. 30) indicate 10 percent levels near the inside tunnel wall, increasing to about 20 percent near the outside tunnel wall.

Station 3: Upstream of the heat exchanger.—Two vertical surveys were made upstream of the heat exchanger. In this leg of the tunnel circuit, the tunnel is 29.17-ft wide by 26.17-ft high; however, because of the configuration of the heat exchanger and turning vanes, the actual survey area was 12.33-ft wide by 26.17-ft high.³ The survey plane was approximately 2.42-ft upstream of the leading edge of the heat exchanger fairings. The traverse locations were at 5.56 and 12.33 ft from the outside (west) tunnel wall. All surveys were made under standard tunnel operating conditions and with the standard configuration.

The total pressure distributions along the vertical surveys conducted upstream of the heat exchanger (fig. 31) indicate a gradient at the higher velocity settings, with higher total pressure levels recorded near the tunnel floor. At $V_{TS} = 350$ mph, the gradient is about 0.020 psia; it decreased to about 0.010 psia at 250 mph. More severe gradients were recorded along traverse 2 (closer to the inside tunnel wall). At the lower velocity settings, the total pressure distribution was uniform.

Figure 32 shows the vertical static pressure distributions at station 3. As is typical of this data set, there is a good deal of scatter in the static pressure data at 350 mph. The scatter in the static pressure data was significantly reduced at the lower velocities. At 250 mph, a vertical gradient occurred (higher pressures near the floor), with a nonuniform distribution over the gradient. These nonuniformities could be caused by the presence of the heat exchanger (pressure disturbances associated with the shape of the heat exchanger and the fairings at the heat exchanger folds). The

³There are two heat exchangers in the tunnel loop between the C and D corners: the large outer heat exchanger, which has three folds, and a smaller inner heat exchanger, which has six folds. The two heat exchangers are separated by a wall (called the splitter wall). The surveys described in this report were made upstream and downstream of the outer heat exchanger, that is, between the outside tunnel wall and the heat exchanger splitter wall. The width of the survey plane at station 3 is the distance from the outside tunnel wall to the corner C turning vanes at the actual measurement plane.

variation in the static pressure along the vertical surveys at 250 mph are about 0.018 psia. At the lower velocity settings, the gradient trend was not recorded, but there was some variation in the static pressure distribution due to the heat exchanger pressure disturbances.

Velocity data from both the pitot-static probes and the wind anemometers indicate a gradient along the vertical surveys upstream of the heat exchanger (figs. 33 and 34, respectively). Higher velocities were recorded near the tunnel floor at all test section velocities, with traverse 2 (closer to inside tunnel wall) showing higher velocities than traverse 1. The velocities measured near the floor were twice as high as those measured near the tunnel ceiling. At all test conditions, the velocity increased with distance from the floor to a height of about 70 in., then steadily decreased toward the tunnel ceiling. This is the same trend recorded in earlier studies (ref. 1). The exact cause of the gradient is not known, but it is thought to be related to poor flow quality along the outside tunnel wall from the drive motor housing through corner C, as documented in this and earlier studies (ref. 1).

Figure 35 shows the vertical total temperature distribution at station 3. These data show that for both traverses and at all test conditions, the total temperature variation is on the order of 2 °R or less. The shape of the distributions and the magnitude of the variations from the two traverses at each test condition closely agree.

Data from pitch and yaw flow angle surveys are shown in figures 36 and 37, respectively. The pitch flow angle data from the two traverses indicate very different distributions; traverse 1 data (nearer to the outside wall) indicate large positive pitch angles (upflow), whereas traverse 2 data indicate large negative pitch angles (downflow). The distributions from the two traverses are a mirror image of one another, but the data do not correlate well with the hotwire data or with data from earlier tests. The yaw angle data distributions (fig. 37) again indicate mirror image distributions from traverses 1 and 2. Since both the pitch and yaw distributions are mirror images, it is possible that one anemometer was incorrectly installed (mounted inverted or wired improperly). At this point, it is not possible to determine if this was the case. There are some similarities between the current pitch and yaw data and the data collected in an earlier study (ref. 1), but there is not enough consistency in the trends to indicate where the problem was or how the data could be logically corrected. The flow angle data collected at station 3 are included here for completeness, although they are believed to be of little value.

Results from the hot-wire anemometer are presented in figures 38 through 42. The mean axial velocity magnitude and distribution for both traverses (fig. 38) very closely match both the pitot-static probe and wind anemometer data. The hot-wire data show slightly higher velocities along traverse 1 than was measured by the wind anemometer. The mean velocity in the vertical plane (pitch direction) indicates upflow over most of the survey, except near the tunnel ceiling where downflow is indicated (fig. 39). These trends in vertical velocity are also exhibited in the pitch angle data measured by the hot-wire probes (fig. 40). The axial and vertical turbulence levels at station 3 (see figs. 41 and 42) are similar for the $V_{TS} = 350$ and 250 mph settings. For these test conditions, axial turbulence varies from 10 to 18 percent, and vertical turbulence varies between 6 and 14 percent. Axial turbulence varies around a mean value, whereas the vertical turbulence shows a slight gradient trend with higher turbulence recorded near the tunnel ceiling along both traverses.

Station 4: Downstream of the heat exchanger.—The tunnel and test configurations downstream of the facility heat exchanger are very similar to those upstream of the heat exchanger. Two vertical surveys were made downstream of the heat exchanger. The survey plane was approximately 2.04-ft downstream of the trailing edge of the heat exchanger fairings. Traverses were made at 5.35 and 12.11 ft from the west (outside) tunnel wall. All surveys were made under standard tunnel operating conditions; however, it should be noted that the heat exchanger was working at only a fraction of its capacity. The tests were all conducted at a nominal 500 °R (40 °F) setting; for icing tests, total temperatures as low as -20 °F are required. Several surveys were made to determine the effect on the flow quality due to the configuration of the heat exchanger's exit guide vanes.

Figure 43 shows the total pressure distributions downstream of the heat exchanger at the two vertical survey locations. The data indicate that the heat exchanger configuration does have an adverse effect on the total pressure distribution. The distributions are similar for both traverse locations, with a large deficit region at the center of the tunnel and two smaller disturbances at 80 and 230 in. (6.7 and 19.2 ft, respectively) from the floor. Each of the total pressure distortions was caused by the fairings at the folds of the heat exchanger—the large deficit region by the fairing over the centerline fold of the heat exchanger, and the two smaller disturbances by the fairings at the off-centerline folds.

The disturbances caused by the heat exchanger are more dominant at the higher test section velocity settings. At the 350 mph setting, the centerline total pressure deficit is approximately 0.014 psia; at 250 mph, it is on the order of 0.007 psia. At the lower test section velocity settings, the presence of the heat exchanger is still apparent, but the magnitude of the disturbances is much less severe. Figure 44 shows the static pressure data along the two surveys. There was a lot of scatter in the data at 350 mph, but we cannot be certain that this is due only to the heat exchanger

effects. At 250 mph and lower settings, the amount of data scatter is less, and the static pressure profiles are fairly uniform.

Velocity data measured by the pitot-static probes are shown in figure 45, and those measured by the wind anemometer are shown in figure 46. As with the total pressure, the velocity distributions for both survey locations are very similar. These data very clearly show the effect of the folded heat exchanger on the tunnel flow quality. Deficit regions corresponding to the height of the fairings at the heat exchanger folds are evident at both the $V_{TS} = 350$ and 250 mph settings. The airspeed recorded in the large centerline deficit is about half of the peak airspeed measured along the survey. The velocity data also clearly show the wake region of the off-centerline fold fairings at approximately 80 and 230 in. above the tunnel floor.

The total temperature distributions from vertical surveys downstream of the heat exchanger are shown in figure 47. These data show large variations in the total temperature over most of the survey at the $V_{TS} = 350$ mph setting, but the magnitude of the variations and the affected survey length decrease at lower velocity settings. At the highest velocity setting, uniform temperature distributions were recorded over only the upper fourth of the surveys. Over the lower three-fourths of the surveys, temperature variations of 10 to 15 °R were measured for both traverses (with slightly higher variations along traverse 1, nearer to the outside tunnel wall). At $V_{TS} = 250$ mph, the uniform portion of the temperature distribution increased to the upper third of the survey, and the largest variations were restricted to the lower quarter of the survey. Over most of the survey, the variations were on the order of 5 °R, although variations of up to 15 °R were recorded along the lower quarter of the survey. The poor temperature distributions downstream of the heat exchanger may be partially due to the exceptionally low coolant flow through the heat exchanger during these flow quality tests, which affects the uniformity of the heat transfer over this area.

Pitch flow angle data at this station are shown in figure 48. At all V_{TS} settings, the flow followed the folds of the heat exchanger at both traverse locations. For example, the pitch flow angle from 0 to about 80 in. above the tunnel floor was positive (upflow), which matches the orientation of the lowest element of the heat exchanger. From 80 to 160 in. above the floor, negative (downward) flow angles were recorded, which again matches the orientation of the second heat exchanger element, and so on. This indicates that the heat exchanger exit guide vanes tend to "overturn" the flow, causing it to follow the contours of the heat exchanger rather than flow axially into the tunnel duct.

The yaw (crossflow) angle data exhibit essentially uniform distributions along the vertical survey for all test conditions (at $V_{TS} = 50$ mph, the wind anemometer was apparently not functioning; see fig. 49). The only discontinuities in the distributions were due to the wakes of the fairings at the heat exchanger bends at 78, 156, and 234 in. above the tunnel floor. Traverse 1 (nearer to the outside tunnel wall) revealed a yaw angle of virtually zero over the survey. Traverse 2 revealed negative yaw angles (flow toward the inside tunnel wall) of the order of 5° because the flow was being influenced by the corner D turning vanes (the flow was starting to make the turn around corner D). The results of additional studies to determine the effects of the heat exchanger exit guide vanes on the flow quality at station 4 are contained in appendix D.

Station 5: Upstream of the spraybars.—Three horizontal and three vertical surveys were made at station 5. Since only two traverse systems were available during the testing, four runs were required to complete the six surveys at station 5. At this station the tunnel measures 29.17-ft wide by 26.17-ft high. The survey plane was located 3.29-ft upstream of the leading edge of the spraybar vertical support struts. The vertical surveys were made at 7.35, 16.42, and 21.92 ft from the north (inside) tunnel wall; the horizontal surveys were made at 6.55, 13.06, and 19.56 ft above the tunnel floor.

Total pressure ratio distributions along the vertical surveys at station 5 are shown in figure 50. The effect of the heat exchanger configuration on the flow quality is still evident in the data along all three vertical surveys made at this station: the centerline deficit area still appears large, but the smaller disturbances caused by the upper and lower folds of the heat exchanger have dissipated. The data also indicate that there were higher pressure levels along the lower portion of the survey than along the upper part. The static pressure data (fig. 51) show a high degree of scatter at the $V_{TS} = 350$ mph setting for the inside wall and centerline surveys (less data scatter was recorded for the outside wall survey); the variation in the data decreased with decreasing velocity.

The velocity distributions from the pitot-static probes and the wind anemometers are presented in figures 52 and 53, respectively. As with the total pressure, the velocity distributions were very much affected by the heat exchanger configuration. The centerline deficit region caused by the middle fold of the heat exchanger is still very apparent in the velocity distributions along all three vertical surveys at station 5. The disturbances caused by the upper and lower heat exchanger folds were not as severe as at station 4, but both are evident along the survey closest to the inside tunnel wall. However, only the lower fold disturbance appears along the survey nearest the outside tunnel wall. These disturbances are not as strong along the centerline vertical survey.

The total temperature distributions (fig. 54) reveal a temperature gradient in the vertical plane, with the higher temperatures near the tunnel ceiling. The gradient is more severe near the outside tunnel wall. There is also another temperature distortion at the tunnel centerline at the $V_{TS} = 350$ mph setting, which is most likely an artifact of the heat exchanger configuration. At $V_{TS} = 350$ mph, the vertical temperature gradient is 6°R along the inside wall survey, 8°R along the centerline survey (the peak variation along the centerline survey is 11°R), and 16°R along the outside wall survey. The magnitude of the gradient and the temperature distortions decreased with the velocity.

Figure 55 shows the pitch flow angle data taken from vertical surveys upstream of the spraybars. Although the data indicate upflow along the entire survey (positive angles), it is likely that there was a bias in the data caused by an offset angle in the traversing plate. In any event, the trend exhibited by the data is correct. The data show that the pitch angle was fairly constant along the surveys, with slightly larger flow angles being recorded along the lower half of the survey (this trend is more noticeable at the higher velocity conditions). The discontinuities recorded at 80 and 240 in. above the tunnel floor in the survey nearest the inside tunnel wall were caused by the heat exchanger fold fairing extensions (junction of the heat exchanger, the turning vanes, and the splitter wall). Similar trends can be seen in the yaw angle data (fig. 56). Constant yaw flow angles were recorded along the centerline and outside wall surveys; the magnitude of the yaw flow angle along these surveys was close to zero ($\pm 2^{\circ}$). The data from the inside wall survey show the discontinuities caused by the heat exchanger fairings.

Figure 57 shows the total pressure ratio distributions along the horizontal surveys upstream of the spraybars. For all conditions and locations, the total pressure distributions are uniform and do not show any gradients or other non-uniformities across the tunnel. The static pressure profiles across the tunnel are shown in figure 58. As at other test locations, there is a high degree of scatter in the static pressure data at the higher velocity conditions, particularly along the upper survey; the reason for the scatter is not known. Because of the scatter in the static pressure data, no firm conclusions could be drawn about the flow quality in terms of static pressure for these data.

The velocity surveys (fig. 59) are the best indicators of the flow quality across the tunnel at this station even though there was some problem with the velocity data along the upper traverse. At $V_{TS} = 350$ mph, the velocity measured along the upper survey was lower than would be expected when compared with the vertical survey data. Also, at all V_{TS} settings, one of the two pitot-static probes along the upper survey was not operating properly and indicated a lower velocity than the other probe did. Otherwise, the velocity data from the horizontal surveys agree well with those from the vertical surveys. The upper and lower surveys indicate higher velocities than the centerline survey does (except at $V_{TS} = 350$ mph, because of the upper survey probe problem), which confirms the distributions from the vertical surveys. The low-velocity region near the inside tunnel wall (between 0 and 60 in. from the inside wall) is the area downstream of the secondary or inner heat exchanger. This portion of the distribution represents the flow exiting the area between the inside tunnel wall and the splitter wall between the primary and secondary heat exchangers.

Along the upper and lower surveys, the velocity decreased over the outside third of the survey (from ≈ 220 to 320 in. from the inside wall), whereas along the centerline survey it increased slightly over this same area. This probably indicates a gradual smoothing of the flow discontinuities caused by the heat exchanger as the distance from the heat exchanger increased. Along the centerline survey, the velocity spike at 60 in. from the inside wall was caused by the splitter wall; the discontinuity between 250 and 270 in. was probably caused by a heat exchanger vertical support strut. The velocity distributions from the wind anemometers (fig. 60) are the same as the distributions from the pressure probes.

Total temperature distributions across the tunnel at station 5 are shown in figure 61. At the $V_{TS} = 350$ mph setting, there is a total temperature gradient of 10 to 15°R across the tunnel along the lower and centerline surveys, with the higher temperatures recorded near the inside tunnel wall (the upper survey thermocouple was inoperative at the test condition). At $V_{TS} = 250$ mph, the gradient along the centerline survey is about 5°R , but there is no gradient apparent along the upper survey; the scatter in the lower survey data makes it difficult to draw a conclusion from these data, although the gradient trend in these data appears similar to that of the centerline survey data. At the lower velocity settings, the variation in the total temperature distributions was on the order of 3°R or less.

The pitch flow angle data (fig. 62) reveal a constant pitch angle of about 2° (upflow) all across the tunnel except immediately downstream of the splitter wall, where a disturbance was recorded along each survey for most test settings (discontinuity occurred at 60 in. from the inside tunnel wall). Other than the effect of the splitter wall, these data indicate no significant flow quality problems. Figure 63 shows the yaw (crossflow) angle distributions across the tunnel. As with the pitch angle, the only major disturbance is that caused by the splitter wall, with the upper survey data being most affected. Away from the area affected by the splitter wall, the data along each survey are fairly uniform, with the lower and upper survey indicating a slight positive flow (toward the outside tunnel wall) and the centerline survey indicating a more pronounced negative flow of up to 5° (toward the inside tunnel wall).

Hot-wire anemometry results are presented in figures 64 through 68. The mean axial velocity data (fig. 64) match very closely the results from the pitot-static and wind anemometer instrumentation. These data also show the low-speed region between the inside tunnel wall and the splitter wall, as well as the gradient trend from the tunnel centerline to the outside tunnel wall along the upper and lower surveys. The hot-wire data from the centerline survey again match the pitot-static and wind anemometer data in magnitude and general distribution. The yaw flow angles measured by the hot-wire probes along the centerline and upper surveys are shown in figure 66. These data clearly show the effect of the splitter wall on the flow field. The magnitude and distribution of the centerline hot-wire data closely match the wind anemometer data from the same survey; the distribution of the hot-wire upper survey data is similar to that of the wind anemometer data, except that the hot-wire data indicate a negative flow angle on the order of 5° (flow toward the inside tunnel wall). The negative yaw flow angle at this station could be an indication of overturning by the D corner turning vanes. Along the centerline survey, turbulence levels on the order of 10 percent (see fig. 67) are indicated. The data vary between 6 and 15 percent for both $V_{TS} = 350$ and 250 mph. The upper survey data indicate lower axial turbulence, ranging from 3 to 12 percent in the center of the tunnel at $V_{TS} = 250$ to 350 mph (higher turbulence levels were also recorded near the tunnel walls). Horizontal turbulence levels are presented in figure 68. The horizontal turbulence varied between 5 and 10 percent along the centerline survey and between 3 and 10 percent along the upper survey at these same velocities.

Station 6: Downstream of the spraybars.—Two horizontal surveys were made at the inlet of the bellmouth-contraction section. The survey plane was 4.56 ft downstream of the leading edge of the spraybar system support strut. Although the traversing plates were physically mounted in the bellmouth, the survey plane was taken to be the exit of the settling chamber (the tunnel at this station was 29.17 ft wide by 26.17 ft high). The traverse locations were 8.72 and 17.22 ft from the tunnel floor (roughly one-third and two-thirds of the tunnel height). All surveys were made under standard tunnel operating conditions.

Figure 69 shows the total pressure ratio distributions across the tunnel at the bellmouth inlet. Here the total pressure is fairly uniform across the tunnel, although there is a slight gradient along the upper survey at the higher velocity settings (higher pressures were recorded near the inside tunnel wall). The static pressure distributions are presented in figure 70. The differential pressure transducers for pitot-static probe 1 on traverse 1 (upper survey) were not operating properly, so the static pressures calculated with the data from that probe are incorrect; the data from pitot-static probe 2 along this survey were not affected. The static pressure instrumentation problem is more readily apparent in the velocity data (fig. 71); the data from probe 1 on traverse 1 are not considered in further discussion of these data.

The velocity data at station 6 still show the effects of the splitter wall and inner cooler area near the inside tunnel wall at all test conditions. The gradient along the outer third of the surveys, as seen at station 5, is also still apparent. The velocity distributions and magnitude from the two surveys were the same for all test conditions (comparing probe 2 from traverse 1 to all traverse 2 data), indicating a symmetric distribution around the tunnel's horizontal centerline. The velocity data from the wind anemometer (fig. 72) also show the similarity between the two survey planes, the effect of the splitter wall, and the gradient near the outside tunnel wall. The wind anemometer data also exhibit a slight deficit region near the center of both surveys (more apparent at the higher velocity settings). This is probably due to the wake of the center vertical support for the spraybar system.

The total temperature data (fig. 73) reveal a significant gradient across the tunnel at the $V_{TS} = 350$ mph setting; this gradient is on the order of 10 °R along both the upper and lower surveys, with the higher temperatures near the inside tunnel wall. This gradient may be a result of less heat being transferred by the secondary heat exchanger since it is most severe in the area of the splitter wall. The gradient decreases with decreasing test section velocity. At $V_{TS} = 250$ mph, there is less than 5 °R variation along the upper survey and a gradient of about 7 °R along the lower survey. At the lower velocity settings, the variation is on the order of 3 °R or less.

Pitch and yaw flow angle distributions are shown in figures 74 and 75, respectively. Because the survey plane was at the inlet of the bellmouth section, the flow was already being influenced by the presence of the bellmouth contours. In the pitch plane, the data along the upper survey (traverse 1) indicate a downward (negative) flow angle, whereas data along the lower survey (traverse 2) show an upward (positive) flow angle trend. These are the expected trends, since the flow from the upper portion of the tunnel would be turned downward (negative flow angle) and flow from the lower portion of the tunnel would be turned upward (positive flow angle) into the bellmouth. The lower survey data also show the effect of the splitter wall, although there is no noticeable effect seen along the upper traverse. The magnitude of the pitch angle is about the same for both surveys over the test range, and it generally varies between 5 to 10° (at $V_{TS} = 350$ mph, the average pitch angles are -7.1° along both the upper and lower traverses).

The yaw flow angle (fig. 75) also clearly shows the effect of the bellmouth contours on the incoming airflow. For all test conditions, the yaw angle varies from 15° near the inside wall to -15° near the outside wall. The positive flow angles measured along the inside portion of the surveys indicate flow from the inside toward the outside wall of the tunnel, which matches the contour of the bellmouth; along the outside portion of the surveys, negative yaw angles were recorded, indicating flow from the outside wall toward the inside wall, which again matches the bellmouth contour. The 0° yaw angles measured near the tunnel centerline (175 in. from the inside tunnel wall) indicate a symmetric flow pattern around the tunnel centerline. In both surveys, the effects of the splitter wall (disturbances between 40 and 100 in. from the inside wall) can be seen.

Hot-wire data are presented in figures 76 through 80. The mean axial velocity data from the hot-wire instrumentation (fig. 76) very closely match the data sets from the pitot-static probes and the wind anemometers in terms of magnitude and distribution. The mean horizontal (crossflow) velocity (fig. 77) and the yaw flow angle (fig. 78) show the influence of the bellmouth contours on the incoming airflow as the air is turned toward the center of the tunnel. The yaw flow angle data match the wind anemometer data in terms of magnitude and trend for all test points. Axial turbulence intensity levels (fig. 79) along traverse 1 (upper survey) vary between 2 and 10 percent, whereas along traverse 2 (lower survey), the variation is between 4 and 12 percent. Neglecting the data near the tunnel walls, the average axial turbulence value from the upper traverse is about 4 to 5 percent; along the lower traverse, the average is between 6 and 7 percent. Similar values were recorded for horizontal turbulence levels (fig. 80).

Flow Visualization

Station 1: Downstream of the fan.—A portable smoke wand system was used to briefly study the characteristics of the flow immediately downstream of the IRT fan. Observations were made with the fan rotating at 50, 100, and 187 rpm (187 rpm corresponds to a test section speed of 150 mph). Flow visualization studies were carried out only at low test sections speeds (150 mph and below) because safety regulations do not allow personnel to be present in the IRT tunnel-loop sections (i.e., settling chamber section, heat exchanger section, and fan section) at high test section speeds. In general, the same results were observed at all three fan speeds. In the area between the downstream half of the fan motor housing and the outer wall, reversed and separated flow was observed along the outer wall and along the fan motor housing. This reversed flow subsided at elevations closer to the floor. Further downstream along the outer wall and near the outer wall vent tower doors, more reversed flow was noted.

Between the fan motor housing and the inner wall, the flow was relatively smooth and appeared to be attached along the fan motor housing and along the inner wall. Generally, flow swirl induced by the fan rotation could be seen at all locations. Such flow phenomena in and around the fan motor housing have been noted in previous flow visualization studies (ref. 1) and generally result from the blockage introduced by the solid fan motor housing supports. As the flow exits the fan, it tends to swirl clockwise (from a downstream viewpoint, the fan spins in a clockwise direction; see fig. 11). With the solid support legs hindering the swirl, flow is drawn from the outer wall side and accumulates on the inner wall side. The drawn flow is more susceptible to separation and reversal, whereas the accumulated flow is more likely to remain attached and be more directionally uniform.

Station 5: Upstream of the spraybars.—The smoke wand system was also used to inject flow visualization smoke into the settling chamber. The smoke was injected immediately downstream of the spraybar plane, at three spanwise locations and at five vertical locations. The spanwise locations were about 2 ft from the inner wall, 2 ft from the centerline, and 2 ft from the outer wall. The five vertical locations corresponded to the vertical locations of the five spraybars closest to the settling chamber floor (vertical heights of 6, 8, 10, 12, and 14 ft, respectively). Smoke trails were observed from three locations: the settling chamber at the point of smoke injection, which gives an eye-level view from the settling chamber; the windows of the main IRT control room, which give a view of the inner test section wall; and the windows of the auxiliary IRT control room, which give a view of the outer test section wall.

The smoke trails were videotaped from the settling chamber. Observers in the control rooms located the smoke trails in the test section by using 1-ft graduation marks on the test section walls. Table 3 summarizes the observations made during the flow visualization tests. These observations should be used only for qualitative purposes and should not be used in any quantitative manner. As a rule, the smoke streams diffused rather quickly after leaving the tip of the smoke wand because of the turbulence of the flow in the settling chamber. In addition, the smoke streams appeared to be unsteady as they moved through the test section. When the smoke was injected at the 14-ft vertical location (centerline spanwise location), the resulting smoke trail appeared to pass through the test section centerline. When the smoke was injected near the inner wall, the smoke trails tended to be on the test section centerline. Smoke injected on the centerline and at the lower vertical heights tended to move toward the outer test section wall.

Follow-On Tests

As a result of the initial series of tunnel-loop flow quality surveys described in this report, several follow-on tests were identified. These tests included the heat exchanger exit guide vane studies mentioned previously and described in appendix D. Two other tests were also conducted: detailed temperature surveys at the heat exchanger inlet (app. E) and flow quality surveys directly downstream of the fan (app. F). Each of these tests addressed specific questions concerning the tunnel flow quality, and the results of the tests were used in the design of facility improvements.

SUMMARY OF RESULTS

The purpose of these studies was to characterize the flow quality throughout the tunnel loop of NASA Glenn Research Center's Icing Research Tunnel. The data reported herein will be used to determine areas in the facility where modifications can be made to improve flow quality and efficiency. These data could also be used to provide boundary or starting conditions for computer simulations of the flow field in the actual facility. Results of these studies follow.

Station 1—Downstream of the Fan

Smoke flow visualization around the drive motor housing (station 1) indicated the presence of a reversed flow area along the outside wall of the tunnel adjacent to the housing.

Station 2—Downstream of the Drive Motor Housing

1. A velocity gradient was found along the vertical surveys downstream of the drive motor housing (station 2), with the higher velocities being near the tunnel floor. The gradient was more severe along the survey made near the inside tunnel wall. Horizontal surveys indicated that there were much higher velocities along the inside portion of the tunnel. Overall, the highest velocities recorded at station 2 were in the lower inside quadrant, and the lowest velocities were in the upper outside quadrant.
2. There were no significant temperature variations recorded at station 2 over the test range.
3. Flow angle measurements at station 2 were consistent with the expected swirl due to rotation of the fan.
4. Axial turbulence intensity at station 2 varied between 10 and 30 percent, with the higher values being recorded near the ceiling and the outside tunnel wall.

Station 3—Upstream of the Heat Exchanger

1. A velocity (total pressure) gradient was measured along the vertical surveys at the heat exchanger inlet, with larger velocities near the tunnel floor (at $V_{TS} = 350$ mph, the velocity near the floor was approximately twice that at the tunnel ceiling).
2. No significant temperature variations were recorded at the heat exchanger inlet.
3. Pitch flow angle data indicated upflow over most of the survey.
4. Axial turbulence intensity levels at the heat exchanger inlet varied between 10 and 18 percent.

Station 4—At the Heat Exchanger Exit

1. The folded configuration of the heat exchanger and the aerodynamic fairings at the corners of the folds caused large disturbances in the flow field downstream of the heat exchanger. The heat exchanger adversely affected the total pressure and velocity distributions at this station by causing a large deficit region near the tunnel centerline and two smaller disturbances at about one-quarter and three-quarters of the tunnel height (these three flow disturbances were caused by the fairings at the corners of the heat exchanger folds).

2. There was a significant total temperature gradient along the vertical surveys downstream of the heat exchanger at $V_{TS} = 350$ mph (10 to 15 °R). The gradient decreased with decreasing velocity.

3. The flow direction (pitch flow angle) was directly affected by the folded configuration of the heat exchanger. The exit guide vanes on the downstream surfaces of the heat exchanger sections overturned the flow such that the flow followed the angle of the heat exchanger sections.

Station 5—Upstream of the Spraybars

1. The effect of the heat exchanger on the flow field (total pressure and velocity profiles) was still apparent in the vertical surveys between the D corner turning vanes and the spraybars. The large centerline deficit region was still very apparent, although the two smaller disturbances had dissipated to some extent. Horizontal surveys showed a low-speed region near the inside wall caused by the inner cooler and a disturbance caused by the splitter wall; there was also a velocity gradient region along the outside portion of the horizontal surveys.

2. The temperature variations recorded downstream of the heat exchanger continued to be apparent at station 5.

3. Axial turbulence intensity levels at station 5 varied between 3 and 12 percent.

Station 6—Downstream of the Spraybars

1. Velocity trends were similar to those seen along the horizontal surveys at station 5 (effect of the splitter wall near the inside wall and the gradient over the outside portion of the survey).

2. There was a 10 °R gradient across the tunnel at $V_{TS} = 350$ mph (higher temperatures were recorded near the outside tunnel wall). The magnitude of the gradient decreased with decreasing velocity.

3. The flow direction at this station was heavily influenced by the bellmouth contours, as demonstrated in both the pitch and yaw flow angle distributions.

4. Axial turbulence intensity at station 6 was between 2 and 12 percent.

CONCLUDING REMARKS

Flow quality in several key areas of the Icing Research Tunnel has been more fully documented in terms of local airspeeds, flow angles, turbulence intensities, and air temperatures. Additional insight has been provided to explain causes of poor flow quality in certain areas of the tunnel. Data are now available to serve as a basis for the design of flow quality improvements and a new facility heat exchanger.

APPENDIX A

SYMBOLS

| | |
|------------|--|
| a | speed of sound, ft/sec |
| M | Mach number |
| N | number of data points |
| P | pressure, psia |
| Pitch | vertical flow angle, positive toward ceiling, deg |
| P_o | total pressure, psia |
| $P_{o,TS}$ | test section total pressure, psia |
| P_s | static pressure, psia |
| $P_{s,TS}$ | test section static pressure, psia |
| R | gas constant, 1716 lb-ft/(slug·°R) |
| T | temperature, °F or °R |
| T_o | total temperature, °R |
| T_s | static temperature, °R |
| TI_u | turbulence intensity in mean flow direction |
| u | velocity component in mean flow direction |
| \bar{u} | average velocity in mean flow direction |
| V | velocity, ft/sec or mph |
| V_{TS} | test section velocity, mph |
| Yaw | horizontal flow angle, positive toward outer wall, deg |
| Z | vertical distance from reference surface, in. |
| γ | ratio of specific heats (constant = 1.4) |
| ΔP | differential pressure ($P_o - P_s$), psid |

Subscripts

| | |
|---------|-------------------------------------|
| A | corner A in the IRT |
| avg | average |
| B | corner B in the IRT |
| C | corner C in the IRT |
| D | corner D in the IRT |
| crawl | crawl space below the tunnel floor |
| outside | outside weather conditions |
| $PS1$ | traverse pitot-static probe 1 |
| $PS2$ | cable traverse pitot-static probe 2 |

T total or stagnation conditions
traverse measurements made by probes on the cable traverse
TS test section
WA cable traverse wind anemometer

APPENDIX B

DATA READING LIST FOR 1995 ICING RESEARCH TUNNEL LOOP FLOW QUALITY STUDIES

Table 4 lists the reading numbers collected during the flow quality surveys for each configuration tested.

APPENDIX C

TABULAR LISTING OF FLOW-FIELD SURVEY DATA

Tables 5 through 36 list the data collected during surveys in the tunnel loop at test section velocities of 250 and 350 mph. Each table contains data from one traverse for one survey station and test configuration. The test section conditions corresponding to the first reading of each survey are also listed on each table. In addition, each table lists the position of the flow-sensing probe from the tunnel reference surface and the measured flow-field parameters.

APPENDIX D

HEAT EXCHANGER EXIT GUIDE VANE STUDIES

Additional measurements were made to quantify the effects of the heat exchanger exit guide vanes on the flow quality downstream of the heat exchanger (station 4). The vane angles of the existing exit guide vanes cannot easily be adjusted with respect to the heat exchanger surface. In order to study the effects of the vane angle on the flow quality, replacement panels of adjustable exit guide vanes were built and installed on the heat exchanger. Because of limited resources, only four panels were constructed. These panels were mounted on the downstream face of the second heat exchanger element such that the portion of that element with the replacement panels was in line with traverse 2 (inside position). In addition to the baseline configuration (described in the text), three other exit guide vane configurations were studied:

Configuration 1—No exit guide vanes (baseline panels removed; no mechanism to turn the flow).

Configuration 2—Replacement panels installed with exit guide vanes stowed (maximum turning of the flow; flow expected to follow contour of the heat exchanger); guide vane exit angle of 0° (parallel to heat exchanger surface).

Configuration 3—Replacement panels installed with exit guide vanes deployed (minimum turning of the flow; flow expected to be more evenly distributed downstream of the heat exchanger); guide vane exit angle of 11° with respect to heat exchanger surface.

Because only a small number of the heat exchanger exit guide vanes were changed, the effects on the flow quality were expected to be localized to just downstream of the new panels; therefore, the length of the surveys was reduced so as to cover only the affected areas. Total and static pressure, velocity from both pitot-static probes and wind anemometers, total temperature, and pitch and yaw flow angle data are included for each configuration (figs. 81 through 87 for configuration 1; figs. 88 through 94 for configuration 2; and figs. 95 through 101 for configuration 3). A summary comparing the data from each configuration to baseline data is given in this appendix.

Configuration 1—No Exit Guide Vanes

Removal of the exit guide vane panels produced a larger than baseline total pressure deficit (both in the magnitude of the deficit and in the size of the affected area; see fig. 81) near the center of the survey directly downstream of the area where the vanes were removed (traverse position 2). There was little difference between the baseline and configuration 1 data at traverse position 1. The effect was more noticeable at the higher velocity conditions. At the $V_{TS} = 350$ mph setting, the total pressure deficit at the tunnel center was about 0.025-psia lower than the peak at 240 in. above the tunnel floor (in comparison to a deficit of about 0.014-psia for the baseline configuration). Static pressure data (fig. 82) show a good deal of scatter for configuration 1, but the distributions indicate increased variation in the static pressure profiles in comparison to the baseline. Velocity data from both the pitot-static probes (fig. 83) and wind anemometers (fig. 84) show a very poor velocity distribution directly downstream of the area where the exit guide vanes were removed (traverse 2). There was a very large velocity deficit in this region (between 70 and 160 in. above the tunnel floor). The data from traverse 1 indicate that the flow from this deficit region was displaced toward the outside wall of the tunnel. Comparison of the baseline and configuration 1 data along traverse 1 shows that the configuration 1 data are much more uniform (the deficit recorded at the baseline was filled in by the displaced flow during the configuration 1 surveys). This trend was recorded at all test conditions by both the pitot-static and wind anemometer instrumentation. These data illustrate not only that the exit guide vanes are required for good flow quality (witness the poor flow quality along traverse 2), but also that the baseline configuration does not provide the optimum velocity distribution (note the improved distribution along traverse 1 for configuration 1, in comparison to the baseline data).

Removing the exit guide vanes actually had a positive effect on the temperature distribution along traverse 2 while degrading the profile along traverse 1 at the $V_{TS} = 350$ mph setting (fig. 85). There is little difference between the baseline and configuration 1 data sets at the other test conditions. Figure 86 shows that much higher pitch flow angles were recorded directly downstream of the area where the exit guide vanes were removed. At traverse position 2, the data indicate large positive angles (upflow), as expected, since there was no mechanism in place to turn the flow in this area. The traverse 1 data indicate little difference in the flow along the portion of the survey below the tunnel centerline; above the tunnel centerline, the pitch angles were smaller than at baseline. With configuration 1, there was a yaw angle gradient over the area directly downstream of where the exit guide vanes were removed.

(fig. 87). The yaw flow angle changed direction, from positive (outflow) at about 80 in. above the tunnel floor to negative (inflow) at about the tunnel centerline. Above the tunnel centerline, the data from traverse 2 are similar to the baseline data. Traverse 1 data are similar to the baseline data except at locations near the tunnel centerline, where the positive yaw angles recorded at the baseline are no longer evident.

Configuration 2—New Exit Guide Vanes With Vanes Stowed

The replacement exit guide vanes with vanes in the stowed position produced nearly identical flow-field distributions as those from the baseline heat exchanger surveys for each flow-field parameter (total and static pressure, velocity, total temperature, and pitch and yaw flow angles; see figs. 88 through 94). There was an increased amount of scatter in the total pressure data at $V_{TS} = 250$ mph and lower settings for configuration 2. The pitot-static velocity results were also affected (the cause of the data scatter is not known).

Configuration 3: New Exit Guide Vanes With Vanes Deployed

Flow-field data collected downstream of the heat exchanger with the replacement exit guide vanes installed and in the deployed (fully extended or open position) are presented in figures 95 through 101. Although the total pressure data (fig. 95) indicate an improvement in the flow quality downstream of the heat exchanger with the new exit guide vanes deployed, the effect on the flow field is more readily apparent in the velocity data (figs. 97 and 98). Even though there was still a deficit area at the tunnel centerline along the traverse 2 survey, the size of the deficit area was greatly reduced by deployment of the new exit guide vanes. At $V_{TS} = 350$ mph, the baseline data indicated a minimum velocity of 23 ft/sec at the tunnel centerline along traverse 2, the height of the affected area being approximately 60 in. (fig. 45); with the new exit guide vanes, the minimum velocity increased to about 31 ft/sec and the height of the deficit area decreased to 20 in. (similar results were seen at the lower velocity conditions). The pitot-static probes also recorded a slight positive effect on the velocity distributions along the traverse 1 surveys (fig. 97), but the wind anemometer data did not vary significantly from the baseline data (figs. 98 and 46, respectively). The effect on the total temperature distribution appeared to be negligible for all except the $V_{TS} = 350$ mph case, where there was a slight improvement in the temperature distribution along traverse 2 (there was no apparent effect on traverse 1 data). The pitch flow angle data along traverse 2 (fig. 100) show that in the region directly downstream of the new exit guide vane panels, the pitch angle became more constant and the flow direction changed from generally downflow to upflow, in comparison to the baseline data (fig. 48 shows the pitch flow angle distribution starting as positive at 200 in. above the tunnel floor and decreasing to a negative value through about 80 in. above the floor; the configuration 3 data shows that over this same survey distance, the pitch angle remained roughly constant). The new exit guide vanes had no effect on the yaw flow angle distribution (fig. 101).

APPENDIX E

ICING RESEARCH TUNNEL HEAT EXCHANGER INLET TEMPERATURE SURVEYS— JANUARY 19, 1996

Introduction

On January 19, 1996, a 1-day test program was executed in the NASA Glenn Icing Research Tunnel (IRT). A vertical cable traverse immediately upstream of the facility heat exchanger was used to monitor the facility temperatures and the crawl space temperatures below corners C and D. These data were used to better understand the heat loading on the heat exchanger and the overall thermodynamics of the facility.

Test Setup

A single vertical cable traverse was installed for this test. This traverse was strung between the tunnel ceiling and floor, about 24 in. upstream of the heat exchanger inlet fairings and 148.5 in. from the outside wall. (The heat exchanger leg is 350-in. wide by 314-in. high.) Installed on the cable traverse carriage were a wind anemometer for measuring airspeed, pitch angle, and yaw angle, and two type-T, aspirated total-temperature probes for measuring total temperature. In the crawl space below corners C and D (the space between the floor and the ground), type-T thermocouple probes were installed.

Test Matrix

Table 37 gives the test matrix for this 1-day program.

Results

Figures 102, 103, and 104 graphically show the important results. Figure 102 shows data versus time for the duration of the test. Figure 102(a) shows the test section velocity and cable traverse vertical position. Figure 102(b) shows the air velocity, pitch flow angle, and yaw flow angle as measured by the wind anemometer on the cable traverse. Figure 102(c) shows all pertinent temperatures: the outside air temperature, the temperature measured by the thermocouple probes on the cable traverse, the temperatures in the crawl spaces beneath corners C and D, and the average air temperatures in corners A, B, C, and D.

If the data in figure 102(c) are closely examined for a test section airspeed of 250 mph, the following data trends can be observed: (1) crawl space C is warmer than crawl space D, and (2) corner C is warmest followed by the traverse, corner D, corner B, and corner A, respectively. The temperatures in corners D, B, and A are within about 3 °F. These results make intuitive sense because crawl space C should be warmer than crawl space D since C is upstream of the heat exchanger and D is downstream. There is also a significant temperature drop (close to 5 °F) between corners C and D due to the cooling of the heat exchanger. The temperatures measured at the traverse are between those measured in corners C and D.

If the data in figure 102(c) are examined for a test section airspeed of 350 mph, the following data trends can be observed: (1) crawl space D is warmer than crawl space C (this is counterintuitive), and corner C is the warmest followed by the traverse, corner B, corner A, and corner D, respectively. Corner D is, of course, the coldest since it is directly downstream of the heat exchanger. The temperatures in corners A and B are close to each other. The traverse temperature approaches the temperature in corner C.

Figures 103 and 104 show the air velocity, flow angle, and air temperature versus distance from the floor as measured by the wind anemometer and thermocouple probes on the cable traverse. Figure 103 is for a test section velocity of 250 mph and a tunnel total temperature of 15 °F. Figure 104 is for a test section velocity of 350 mph and a tunnel total temperature of -17 °F. The air velocity profiles and magnitudes are consistent with previous measurements. Higher air velocities are present near the floor. The flow angles are also consistent with data taken previously. Pitch angles are generally toward the ceiling by 5° to 10° and yaw angles are generally toward the outer

wall by 0° to 5°. The temperature profiles exhibit a temperature gradient with warmer temperatures near the floor. This is counterintuitive because cooler, more dense, air would have a tendency to collect near the floor. In figure 103(c), the gradient range is about 2 °F. In figure 104(c), the gradient range is about 4 °F.

Measurement Uncertainties

During this test, some electronic noise present in the frequency-to-direct-current converter used to measure the wind anemometer airspeed introduced some uncertainty in the measured airspeed. The uncertainty in these measurements was estimated to be ± 2 ft/sec.

In addition, temperature bath calibrations were carried out on the thermocouple probes used on the traverse and in the crawl spaces. Temperature measurements made with these probes were estimated to have an uncertainty of ± 0.5 °F.

APPENDIX F

ICING RESEARCH TUNNEL FAN EXIT FLOW QUALITY SURVEYS—AUGUST 23, 1996

Introduction

On August 23, 1996, a 1-day test program was executed in the NASA Glenn Icing Research Tunnel (IRT). Flow quality data (total pressures, static pressures, total temperatures, airspeeds, pitch angles, and yaw angles) were collected immediately downstream of the IRT fan. These data were needed to aid in the design of fan outlet guide vanes.

Test Setup

A single vertical cable traverse was installed for this test about 50-in. downstream of the fan blade leading edges. This traverse was strung between the tunnel ceiling and fan motor nacelle at the 12 o'clock position (with respect to the fan) as depicted in figure 105. The vertical distance between the nacelle housing and tunnel ceiling where the traverse was installed was 94.25 in. Structural channels were used to reinforce the cable traverse system and to guide the traverse carriage vertically under the air loads. As shown in figure 105, the traverse was rotated "into the wind" or "in the yaw plane" by 30° to compensate for the fan swirl. The traverse carriage was instrumented with two pitot-static probes, a type "K" thermocouple total temperature probe, and a wind anemometer that could resolve airspeed, pitch angle, and yaw angle. On the traverse carriage, the two pitot-static probes were vertically spaced 11.0 in. apart. The wind anemometer was located 5.5 in. above the pitot-static probe closest to the fan motor nacelle. The vertical position of the temperature probe exactly coincided with the pitot-static probe closest to the fan motor nacelle.

The total pressures from the pitot-static probes were measured by 25-psia absolute pressure transducers. The pressure differences between the total and static pressure ports on the pitot-static probes were measured by differential pressure transducers that had 1.0 in. of water range.

In the test section, a flat plate blockage model was used to vary the test section blockage. During this test, the blockage model was installed at a 55° angle of attack or was not used at all. A 90° angle of attack would have corresponded to maximum model blockage.

Test Matrix

Table 38 gives the test matrix for this 1-day test program.

Results

Figure 106 shows measured and computed variables versus time. Figure 106(a) shows the traverse position and the test section velocity for all data acquired. This plot is useful in determining what the test section velocity and traverse position were at any given instant in time during the test. Figure 106(b) shows computed velocities from the wind anemometer and the two pitot-static probes. From Figure 106(b), it is apparent that the wind anemometer and the pitot-static probes worked properly for the first 2.4 hr of the test. Beyond this, the data are questionable. During this test, we noticed that the airspeed sensor failed on the wind anemometer and that the delta-pressure transducers were overranged. Figure 106(c) shows temperatures measured near the traverse, in corner D, and outside. Over the course of the test, the outside air temperature varied between 72 and 84 °F. The traverse and corner D temperatures correlated well and ranged between 59 and 80 °F. The traverse temperature was always higher than the average corner D temperature. The peaks and valleys for the two temperatures were identical. Figure 106(d) shows pitch and yaw flow angles from the wind anemometer. The yaw angles at about 5 hr into the test appear to be questionable since they are around 90°. Figure 106(e) shows the total pressures measured by the two traverse pitot-static probes and the total pressure measured in the test section. The pressures matched at zero flow (at times of 0.0, 1.45, 4.1, and

5.85 hr). Generally speaking, the total pressure downstream of the fan increased with increasing airspeed near the fan blade midspan and tip. Near the root, the total pressure decreased with increasing airspeed. Some of these results are clearer in subsequent figures.

Figure 107(a) shows the wind anemometer air velocity versus test section airspeed for three different elevations ($Z = 23.8, 47.6$, and 73.0 in.) and for two different blockages (no blockage plate and a blockage plate at 55°). Airspeeds as high as 55 and 75 ft/sec were measured for test section speeds of 300 mph. The flat velocity lines indicate that the airspeed sensor on the wind anemometer was not functioning.

Figures 107(b) and (c) show the air velocities computed using the pressures from the two traverse pitot-static probes. Much of the data are near zero and are unusable. This may have resulted from the delta-pressure transducers being overranged. There are a couple of data lines that vary between 30 and 70 ft/sec. These data lines follow the lines seen in figure 107(a).

Figures 108(a) and (b) show the pitch and corrected yaw wind anemometer flow angles, respectively. The pitch angles generally varied between 15° and -10° ; however, the pitch angles near the blade roots ($Z = 23.8$ in.) varied between -15° and -50° . The yaw angles generally varied between 10° and -40° . Two yaw data lines varied between -70° and -95° . However, these data lines are questionable since they are so close to -90° .

Figures 109(a) and (b) show the total pressure recoveries for the two traverse pitot-static probes normalized with respect to the test section total pressure. The data from pitot-static probe 1 (fig. 109(a)) is better behaved and may be of better quality than the data from pitot-static probe 2 (fig. 109(b)). The data generally show increasing total pressure with increasing test section airspeed near the blade tips ($Z = 67.5$ in.), constant total pressure near the blade midspan ($Z = 42.1$ in.), and decreasing total pressure with increasing test section airspeed near the blade roots ($Z = 18.3$ in.). Figure 109(c) shows the total temperature measured by the traverse normalized with respect to the average corner D temperature. The data generally indicate warmer temperatures (by as much as 8°F) with increasing test section airspeed.

Measurement Uncertainties

The measurement uncertainties for the data presented in this appendix are estimated to be ± 3.0 ft/sec for the wind anemometer airspeed, $\pm 2.0^\circ$ for the wind anemometer pitch and yaw flow angles, ± 0.03 psia for the total pressure and ± 0.00005 psid for the delta-pressure (based on accuracy data from the manufacturer), and $\pm 1.0^\circ\text{F}$ for the temperature.

REFERENCES

1. Arrington, E.A.; Pickett, M.T.; and Sheldon, D.W.: Flow Quality Studies of the NASA Lewis Research Center Icing Research Tunnel. NASA TM-106545, 1994.
2. Soeder, R.H.; and Andracchio, C.R.: NASA Lewis Icing Research Tunnel User Manual. NASA TM-102319, 1990.
3. Ames Research Staff: Equations, Tables, and Charts for Compressible Flow. NACA TR-1135, 1953.

TABLE 1.— TEST MATRIX FOR THE 1995 TUNNEL-LOOP FLOW QUALITY STUDIES IN THE NASA GLENN ICING RESEARCH TUNNEL

[For each test configuration, surveys were conducted corresponding to test section velocity settings V_{TS} of 350, 250, 150, and 50 mph]

| Type of survey | Priority | Run number | Comment |
|---|----------|------------|------------------------------------|
| At station 1—downstream of the fan | | | |
| Flow visualization | 4 | n/a | Baseline |
| At station 2—downstream of the drive motor | | | |
| Vertical at 1/3 and 2/3 tunnel width | 2a | 14 | Baseline |
| Horizontal at 1/3 and 2/3 tunnel height | 2a | 15 | Baseline |
| At station 3—upstream of the heat exchanger | | | |
| Vertical at 1/2 and 3/4 tunnel width | 1c | 12 | Baseline |
| At station 4—downstream of the heat exchanger | | | |
| Vertical at 1/2 and 3/4 tunnel width | 1b | 3,4,6 | Baseline heat exchanger |
| Vertical at 1/2 and 3/4 tunnel width | 1b | 4 | Exit guide vanes removed |
| Vertical at 1/2 and 3/4 tunnel width | 1b | 4 | Replacement guide vanes (stowed) |
| Vertical at 1/2 and 3/4 tunnel width | 1b | 5 | Replacement guide vanes (deployed) |
| At station 5—upstream of the spraybars | | | |
| Vertical at 1/4 and 1/2 tunnel width | 1a | 8 | Baseline |
| Vertical at 1/2 and 3/4 tunnel width | 1a | 9 | Baseline |
| Horizontal surveys at 1/4 and 1/2 tunnel height | 1a | 10 | Baseline |
| Horizontal at 1/2 and 3/4 tunnel height | 1a | 11 | Baseline |
| Flow visualization | 4 | 17 | Baseline |
| At station 6—downstream of the spraybars | | | |
| Horizontal at 1/3 and 2/3 tunnel height | 3 | 17 | Baseline |

TABLE 2.—TYPICAL TEST SECTION CONDITIONS FOR THE TUNNEL-LOOP FLOW QUALITY STUDIES

[Conditions were from run 3 (2/13/1995)—empty test section and no icing/spray conditions.]

| Flow parameter | | | | | | |
|---|-------------------------------|----------------|------------------------------|---|-------------------------------|----------------|
| Nominal test section velocity, V_{TS} , mph | Static pressure, P_s , psia | Mach number, M | Total pressure, P_o , psia | Actual test section velocity, V_{TS} , mph (ft/sec) | Total temperature, T_o , °R | Fan speed, rpm |
| 350 | 12.315 | 0.480 | 14.418 | 350.6 (514.2) | 499 | 393 |
| 250 | 13.321 | .339 | 14.424 | 250.6 (367.5) | 500 | 291 |
| 150 | 14.021 | .203 | 14.430 | 150.7(221.0) | 497 | 180 |
| 50 | 14.425 | .068 | 14.472 | 51.0 (74.8) | 503 | 65 |

TABLE 3.—SUMMARY OF OBSERVATIONS DURING SMOKE FLOW VISUALIZATIONS IN SETTLING CHAMBER

| Vertical distance of smoke injection site from settling chamber floor, ft | Test section velocity, V_{TS} , mph | Vertical distance of smoke from floor in test section, ft | Comments |
|---|---------------------------------------|---|--|
| Smoke injected spanwise near inner wall | | | |
| 6 | 200 | 2.0 | Smoke steady in bellmouth |
| 8 | 200 | 2.5 | Smoke steady in bellmouth |
| 8 | 150 | 2.0±0.5 | Smoke steady in bellmouth and unsteady in test section |
| 10 | 150 | 3.0 | Smoke steady in bellmouth |
| 12 | 150 | 4.0±0.5 | Smoke steady in bellmouth |
| 14 | 150 | 4.5±0.5 | Smoke steady in bellmouth |
| Smoke injected spanwise near centerline | | | |
| 6 | 150 | 1.0±1.0 | Spanwise location of smoke was closer to outer wall |
| 8 | 150 | 2.0±1.0 | Spanwise location of smoke was closer to outer wall |
| 10 | 150 | 2.8±0.5 | Spanwise location of smoke was closer to outer wall |
| 12 | 150 | 3.5±1.0 | Spanwise location of smoke was near centerline |
| 14 | 150 | 3.8±1.0 | Spanwise location of smoke was near centerline |
| Smoke injected spanwise near outer wall | | | |
| 6 | 150 | 1.0±1.0 | Smoke followed bellmouth contour smoothly |
| 8 | 150 | 2.0±0.5 | Some smoke unsteadiness in bellmouth |
| 10 | 150 | 2.5±1.0 | Smoke unsteady in test section |
| 12 | 150 | 3.0±1.0 | Smoke unsteadiness reduced |
| 14 | 150 | 4.0±1.0 | Smoke unsteadiness reduced |

TABLE 4.—SUMMARY OF DATA^a RECORDED DURING EACH RUN DAY FOR EACH TEST CONFIGURATION

| Run day | Station | Reading numbers for various test section velocities, V_{TS} | | | |
|---------|---------|---|--------------|------------------------|--------------|
| | | 50 mph | 150 mph | 250 mph | 350 mph |
| 3,4 | 4 | 210 to 260 | 156 to 206 | 105 to 127; 129 to 155 | 54 to 104 |
| 4 | 4 | 348 to 376 | 319 to 347 | 290 to 318 | 261 to 289 |
| 5 | 4 | 465 to 493 | 436 to 464 | 407 to 435 | 378 to 406 |
| 5,6 | 4 | 583 to 611 | 554 to 582 | 525 to 553 | 494 to 523 |
| 6 | 4 | 681 to 700 | 661 to 680 | 641 to 660 | 612 to 640 |
| 8 | 5 | 860 to 908 | 811 to 859 | 761 to 810 | 711 to 760 |
| 9 | 5 | 1168 to 1219 | 1109 to 1159 | 1050 to 1100 | 991 to 1041 |
| 10 | 5 | 1425 to 1469 | 1373 to 1416 | 1317 to 1364 | 1265 to 1308 |
| 11 | 5 | 1588 to 1622 | 1552 to 1587 | 1516 to 1551 | 1480 to 1515 |
| 12 | 3 | 1785 to 1836 | 1732 to 1784 | 1679 to 1731 | 1626 to 1678 |
| 14 | 2 | 2023 to 2065 | 1979 to 2022 | 1934 to 1978 | 1883 to 1933 |
| 15 | 2 | 2244 to 2293 | 2195 to 2243 | 2148 to 2194 | 2098 to 2147 |
| 17 | 6 | 2432 to 2472 | 2391 to 2431 | 2350 to 2390 | 2308 to 2349 |

^aData are stored in data base as part of IRT ESCORT program D033.

TABLE 5.—DATA LISTING FOR TRAVERSE 1 AT STATION 2—VERTICAL SURVEY
 [Test section data for reading 1883; total pressure, 14.312; static pressure, 12.222 psia; total temperature,
 449°R ; velocity, 350.9 mph; fan speed, 387.5 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|---------------------------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, $^{\circ}\text{R}$ | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1883 | 31.3 | 14.335 | 14.326 | 33.7 | 20.8 | 14.360 | 14.324 | 65.8 | 31.1 | 506.8 | 26.1 | 66.0 | 1.9 | 11.8 |
| 1884 | 36.3 | 14.337 | 14.328 | 32.4 | 25.8 | 14.361 | 14.326 | 64.7 | 36.0 | 506.5 | 31.0 | 65.2 | 2.3 | 11.3 |
| 1885 | 38.9 | 14.338 | 14.329 | 33.3 | 28.4 | 14.363 | 14.328 | 65.2 | 38.6 | 506.5 | 33.6 | 64.7 | 1.8 | 11.6 |
| 1886 | 44.8 | 14.338 | 14.330 | 31.8 | 34.3 | 14.363 | 14.329 | 64.5 | 44.5 | 506.1 | 39.5 | 63.9 | 1.9 | 9.6 |
| 1887 | 51.3 | 14.339 | 14.330 | 31.8 | 40.8 | 14.361 | 14.327 | 63.9 | 51.0 | 506.1 | 46.0 | 63.4 | 1.9 | 9.8 |
| 1888 | 60.5 | 14.339 | 14.330 | 34.1 | 50.0 | 14.360 | 14.327 | 62.9 | 60.3 | 506.0 | 55.3 | 64.4 | 4.9 | 8.9 |
| 1889 | 66.3 | 14.340 | 14.330 | 34.8 | 55.8 | 14.358 | 14.326 | 62.5 | 66.0 | 505.8 | 61.0 | 58.4 | 2.7 | 10.1 |
| 1890 | 72.9 | 14.341 | 14.330 | 35.6 | 62.4 | 14.360 | 14.327 | 62.8 | 72.6 | 505.7 | 67.6 | 60.2 | 2.8 | 7.8 |
| 1891 | 78.3 | 14.338 | 14.329 | 32.8 | 67.8 | 14.354 | 14.325 | 58.8 | 78.0 | 505.8 | 73.0 | 54.5 | 2.2 | 10.3 |
| 1892 | 84.3 | 14.338 | 14.330 | 32.5 | 73.8 | 14.352 | 14.325 | 57.4 | 84.1 | 505.6 | 79.1 | 58.6 | 2.4 | 8.1 |
| 1893 | 90.2 | 14.339 | 14.329 | 34.2 | 79.7 | 14.353 | 14.326 | 57.3 | 89.9 | 505.5 | 84.9 | 61.7 | 2.9 | 5.0 |
| 1894 | 96.6 | 14.338 | 14.330 | 31.9 | 86.1 | 14.349 | 14.325 | 53.5 | 96.4 | 505.5 | 91.4 | 50.1 | 2.2 | 9.5 |
| 1895 | 102.3 | 14.337 | 14.329 | 29.5 | 91.8 | 14.346 | 14.325 | 50.2 | 102.1 | 505.4 | 97.1 | 45.5 | 3.2 | 11.1 |
| 1896 | 108.8 | 14.337 | 14.330 | 30.4 | 98.3 | 14.345 | 14.324 | 50.1 | 108.5 | 505.3 | 103.5 | 48.3 | 1.4 | 7.7 |
| 1897 | 114.9 | 14.337 | 14.329 | 30.4 | 104.4 | 14.344 | 14.324 | 48.9 | 114.7 | 505.2 | 109.7 | 45.9 | 3.9 | 7.2 |
| 1898 | 120.8 | 14.337 | 14.329 | 30.0 | 110.3 | 14.344 | 14.325 | 47.9 | 120.5 | 505.1 | 115.5 | 45.3 | 3.6 | 12.0 |
| 1899 | 126.6 | 14.335 | 14.329 | 28.1 | 116.1 | 14.341 | 14.324 | 44.8 | 126.3 | 504.9 | 121.3 | 41.6 | 3.4 | 8.4 |
| 1900 | 132.4 | 14.336 | 14.330 | 25.3 | 121.9 | 14.338 | 14.324 | 41.4 | 132.1 | 505.0 | 127.1 | 38.1 | 5.7 | 8.2 |
| 1901 | 138.2 | 14.336 | 14.330 | 26.5 | 127.7 | 14.339 | 14.324 | 41.7 | 138.0 | 505.0 | 133.0 | 37.2 | 1.1 | 6.0 |
| 1902 | 144.5 | 14.335 | 14.330 | 25.3 | 134.0 | 14.336 | 14.323 | 38.9 | 144.3 | 505.3 | 139.3 | 35.7 | 1.9 | 9.0 |
| 1903 | 150.3 | 14.336 | 14.331 | 26.2 | 139.8 | 14.335 | 14.322 | 38.7 | 150.0 | 505.8 | 145.0 | 35.0 | 8.7 | 4.8 |
| 1904 | 156.5 | 14.336 | 14.331 | 24.5 | 146.0 | 14.334 | 14.323 | 36.6 | 156.3 | 505.6 | 151.3 | 34.7 | 3.4 | -9 |
| 1905 | 162.4 | 14.336 | 14.332 | 20.9 | 151.9 | 14.334 | 14.324 | 33.3 | 162.1 | 505.2 | 157.1 | 29.5 | 1.4 | 4.7 |
| 1906 | 168.3 | 14.336 | 14.332 | 20.0 | 157.8 | 14.335 | 14.325 | 34.2 | 168.0 | 505.2 | 163.0 | 32.1 | 3.2 | 6.3 |
| 1907 | 175.0 | 14.336 | 14.332 | 22.0 | 164.5 | 14.335 | 14.326 | 33.6 | 174.8 | 505.0 | 169.8 | 28.8 | -2.7 | 5.6 |

TABLE 5.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1908 | 181.0 | 14.336 | 14.331 | 22.6 | 170.5 | 14.335 | 14.325 | 34.1 | 180.7 | 504.8 | 175.7 | 28.5 | -1.4 | 4.1 |
| 1909 | 186.4 | 14.337 | 14.333 | 21.8 | 175.9 | 14.336 | 14.327 | 33.2 | 186.2 | 504.6 | 181.2 | 29.7 | 4.3 | 0.0 |
| 1910 | 192.0 | 14.336 | 14.333 | 20.7 | 181.5 | 14.335 | 14.327 | 31.3 | 191.8 | 504.7 | 186.8 | 27.8 | .9 | .4 |
| 1911 | 198.0 | 14.336 | 14.333 | 18.8 | 187.5 | 14.333 | 14.326 | 29.8 | 197.8 | 504.7 | 192.8 | 26.5 | -5.7 | -1.1 |
| 1912 | 204.7 | 14.337 | 14.334 | 17.4 | 194.2 | 14.335 | 14.328 | 28.1 | 204.4 | 504.3 | 199.4 | 25.1 | -1.4 | -4.1 |
| 1913 | 210.1 | 14.337 | 14.334 | 17.2 | 199.6 | 14.334 | 14.328 | 26.7 | 209.9 | 504.3 | 204.9 | 23.4 | -3.1 | 2.5 |
| 1914 | 217.8 | 14.337 | 14.334 | 17.8 | 207.3 | 14.334 | 14.328 | 25.9 | 217.6 | 504.5 | 212.6 | 23.6 | -6.3 | -2.4 |
| 1915 | 221.5 | 14.337 | 14.334 | 18.5 | 211.0 | 14.334 | 14.328 | 27.8 | 221.2 | 504.5 | 216.2 | 25.0 | -.3 | -2.8 |
| 1916 | 228.2 | 14.337 | 14.335 | 16.7 | 217.7 | 14.334 | 14.328 | 27.3 | 227.9 | 504.4 | 222.9 | 24.3 | -3.5 | -5.1 |
| 1917 | 233.6 | 14.336 | 14.335 | 14.9 | 223.1 | 14.333 | 14.327 | 25.9 | 233.4 | 503.8 | 228.4 | 22.8 | -3.7 | -5.4 |
| 1918 | 239.9 | 14.337 | 14.334 | 18.0 | 229.4 | 14.333 | 14.328 | 24.8 | 239.7 | 503.8 | 234.7 | 20.8 | 0.7 | -8.0 |
| 1919 | 247.4 | 14.337 | 14.335 | 17.1 | 236.9 | 14.333 | 14.327 | 26.0 | 247.1 | 503.7 | 242.1 | 22.2 | -2.8 | -9.9 |
| 1920 | 255.1 | 14.337 | 14.334 | 16.3 | 244.6 | 14.333 | 14.328 | 23.8 | 254.9 | 503.6 | 249.9 | 20.1 | 1.7 | -6.9 |
| 1921 | 258.1 | 14.337 | 14.334 | 16.8 | 247.6 | 14.332 | 14.327 | 24.6 | 257.8 | 503.9 | 252.8 | 21.4 | 2.1 | -10.4 |
| 1922 | 265.4 | 14.337 | 14.335 | 16.3 | 254.9 | 14.332 | 14.327 | 24.1 | 265.2 | 503.8 | 260.2 | 20.2 | -1.8 | -2.5 |
| 1923 | 269.8 | 14.337 | 14.334 | 17.5 | 259.3 | 14.333 | 14.328 | 23.8 | 269.5 | 503.6 | 264.5 | 22.3 | 0.7 | -11.0 |
| 1924 | 276.0 | 14.337 | 14.335 | 17.1 | 265.5 | 14.334 | 14.328 | 26.2 | 275.8 | 503.6 | 270.8 | 23.9 | -.4 | -5.7 |
| 1925 | 283.0 | 14.337 | 14.335 | 16.7 | 272.5 | 14.332 | 14.328 | 23.0 | 282.8 | 503.4 | 277.8 | 21.3 | 2.9 | -7.3 |
| 1926 | 288.9 | 14.337 | 14.335 | 17.1 | 278.4 | 14.331 | 14.327 | 21.6 | 288.7 | 503.6 | 283.7 | 19.3 | 2.8 | -9.7 |
| 1927 | 251.9 | 14.337 | 14.335 | 16.1 | 241.4 | 14.333 | 14.327 | 27.0 | 251.6 | 503.7 | 246.6 | 25.0 | -1.8 | -8.0 |
| 1928 | 215.6 | 14.338 | 14.336 | 17.0 | 205.1 | 14.333 | 14.327 | 26.5 | 215.4 | 503.9 | 210.4 | 22.1 | -1.6 | -6.5 |
| 1929 | 180.5 | 14.339 | 14.335 | 20.6 | 170.0 | 14.336 | 14.327 | 32.6 | 180.3 | 504.2 | 175.3 | 29.9 | 1.4 | 5.3 |
| 1930 | 144.3 | 14.340 | 14.335 | 24.8 | 133.8 | 14.341 | 14.327 | 40.1 | 144.1 | 504.4 | 139.1 | 34.4 | 5.3 | 6.8 |
| 1931 | 109.0 | 14.345 | 14.336 | 31.8 | 98.5 | 14.350 | 14.328 | 51.5 | 108.8 | 504.6 | 103.8 | 47.0 | 1.7 | 5.4 |
| 1932 | 73.2 | 14.348 | 14.338 | 34.3 | 62.7 | 14.360 | 14.329 | 61.1 | 73.0 | 504.7 | 68.0 | 57.9 | 4.6 | 8.7 |
| 1933 | 32.0 | 14.349 | 14.339 | 34.4 | 21.5 | 14.366 | 14.331 | 65.1 | 31.7 | 505.2 | 26.7 | 64.4 | 1.4 | 13.3 |

TABLE 6.—DATA LISTING FOR TRAVERSE 2 AT STATION 2—VERTICAL SURVEY
 [Test section data for reading 1883; total pressure, 14.312; static pressure, 12.222 psia; total temperature, 49° R; velocity, 350.9 mph; fan speed, 387.5 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1883 | 30.7 | 14.345 | 14.323 | 51.2 | 20.4 | 14.344 | 14.324 | 49.7 | 28.9 | 503.7 | 22.9 | 51.2 | 3.6 | 7.5 |
| 1884 | 36.5 | 14.348 | 14.327 | 50.1 | 26.3 | 14.348 | 14.328 | 49.0 | 34.8 | 503.9 | 28.8 | 50.8 | 5.3 | 8.8 |
| 1885 | 40.1 | 14.347 | 14.327 | 49.5 | 29.9 | 14.347 | 14.328 | 48.1 | 38.4 | 503.6 | 32.4 | 48.7 | 5.7 | 10.7 |
| 1886 | 45.5 | 14.350 | 14.328 | 50.9 | 35.3 | 14.350 | 14.329 | 49.5 | 43.8 | 503.5 | 37.8 | 46.2 | 5.5 | 9.4 |
| 1887 | 51.7 | 14.349 | 14.329 | 48.7 | 41.5 | 14.348 | 14.329 | 46.7 | 50.0 | 503.6 | 44.0 | 45.8 | 5.8 | 9.4 |
| 1888 | 60.2 | 14.347 | 14.329 | 47.0 | 49.9 | 14.346 | 14.330 | 44.9 | 58.4 | 503.6 | 52.4 | 43.2 | 7.6 | 8.5 |
| 1889 | 66.3 | 14.348 | 14.329 | 47.5 | 56.0 | 14.347 | 14.330 | 44.8 | 64.5 | 503.4 | 58.5 | 44.7 | 6.8 | 7.3 |
| 1890 | 72.6 | 14.346 | 14.329 | 45.2 | 62.3 | 14.345 | 14.330 | 42.4 | 70.8 | 503.4 | 64.8 | 43.4 | 4.2 | 8.4 |
| 1891 | 78.4 | 14.345 | 14.328 | 44.8 | 68.1 | 14.345 | 14.330 | 41.8 | 76.6 | 503.5 | 70.6 | 41.3 | 11.7 | 6.0 |
| 1892 | 84.7 | 14.345 | 14.329 | 43.9 | 74.4 | 14.343 | 14.330 | 39.9 | 82.9 | 503.4 | 76.9 | 38.6 | 4.6 | 7.6 |
| 1893 | 90.2 | 14.344 | 14.330 | 40.9 | 79.9 | 14.342 | 14.330 | 38.0 | 88.4 | 503.4 | 82.4 | 34.8 | 9.1 | 7.3 |
| 1894 | 96.0 | 14.343 | 14.330 | 38.9 | 85.7 | 14.342 | 14.331 | 36.4 | 94.2 | 503.5 | 88.2 | 33.8 | 8.5 | 3.6 |
| 1895 | 102.2 | 14.343 | 14.330 | 39.0 | 92.0 | 14.341 | 14.330 | 35.3 | 100.5 | 503.5 | 94.5 | 34.2 | 6.3 | 4.4 |
| 1896 | 108.2 | 14.341 | 14.330 | 36.1 | 97.9 | 14.340 | 14.331 | 33.1 | 106.4 | 503.3 | 100.4 | 30.1 | 8.0 | 9.5 |
| 1897 | 114.5 | 14.338 | 14.330 | 32.0 | 104.2 | 14.338 | 14.330 | 29.8 | 112.7 | 503.3 | 106.7 | 27.0 | 6.3 | 3.3 |
| 1898 | 120.5 | 14.338 | 14.330 | 32.5 | 110.2 | 14.338 | 14.331 | 30.7 | 118.7 | 503.5 | 112.7 | 27.3 | 3.5 | 9.6 |
| 1899 | 126.6 | 14.338 | 14.329 | 33.1 | 116.4 | 14.339 | 14.330 | 32.0 | 124.9 | 503.4 | 118.9 | 27.3 | 9.3 | -2.3 |
| 1900 | 132.2 | 14.339 | 14.330 | 32.4 | 122.0 | 14.338 | 14.331 | 30.1 | 130.5 | 503.4 | 124.5 | 28.1 | 4.1 | 7.7 |
| 1901 | 138.2 | 14.338 | 14.330 | 30.4 | 128.0 | 14.338 | 14.332 | 28.6 | 136.5 | 503.6 | 130.5 | 25.4 | 8.6 | -1.0 |
| 1902 | 144.2 | 14.338 | 14.331 | 29.5 | 133.9 | 14.339 | 14.332 | 28.1 | 142.4 | 503.9 | 136.4 | 25.3 | 4.7 | 4.9 |
| 1903 | 149.3 | 14.339 | 14.331 | 30.1 | 139.0 | 14.339 | 14.332 | 29.3 | 147.5 | 504.4 | 141.5 | 24.8 | 6.2 | 4.7 |
| 1904 | 156.2 | 14.339 | 14.332 | 28.5 | 145.9 | 14.339 | 14.332 | 28.1 | 154.4 | 504.4 | 148.4 | 21.6 | 5.6 | -3.8 |
| 1905 | 162.1 | 14.339 | 14.332 | 28.8 | 151.9 | 14.339 | 14.332 | 28.4 | 160.4 | 504.2 | 154.4 | 23.0 | 8.4 | .3 |
| 1906 | 167.7 | 14.339 | 14.332 | 28.7 | 157.5 | 14.339 | 14.333 | 28.0 | 166.0 | 504.1 | 160.0 | 26.9 | 8.5 | 5.6 |
| 1907 | 174.6 | 14.338 | 14.332 | 27.0 | 164.4 | 14.338 | 14.333 | 26.2 | 172.9 | 503.9 | 166.9 | 24.9 | 10.8 | 6.0 |

TABLE 6.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1908 | 180.4 | 14.338 | 14.333 | 25.4 | 170.1 | 14.338 | 14.333 | 25.1 | 178.6 | 503.9 | 172.6 | 21.8 | 7.5 | 5.8 |
| 1909 | 187.5 | 14.340 | 14.333 | 29.0 | 177.3 | 14.340 | 14.334 | 28.3 | 185.8 | 503.8 | 179.8 | 26.4 | 8.5 | 6.4 |
| 1910 | 191.8 | 14.340 | 14.334 | 26.9 | 181.6 | 14.340 | 14.335 | 25.7 | 190.1 | 503.9 | 184.1 | 23.3 | 11.7 | -1.2 |
| 1911 | 198.6 | 14.340 | 14.335 | 26.8 | 188.4 | 14.341 | 14.336 | 26.6 | 196.9 | 503.8 | 190.9 | 25.8 | 11.9 | 5.6 |
| 1912 | 205.5 | 14.341 | 14.335 | 26.4 | 195.3 | 14.342 | 14.336 | 25.9 | 203.8 | 503.6 | 197.8 | 22.0 | 4.1 | 3.5 |
| 1913 | 209.9 | 14.340 | 14.335 | 24.6 | 199.6 | 14.342 | 14.337 | 24.1 | 208.1 | 503.6 | 202.1 | 24.2 | 12.4 | 3.3 |
| 1914 | 217.1 | 14.340 | 14.335 | 24.4 | 206.8 | 14.341 | 14.337 | 24.1 | 215.3 | 504.0 | 209.3 | 22.4 | -1.8 | 2.8 |
| 1915 | 220.9 | 14.341 | 14.336 | 24.7 | 210.7 | 14.341 | 14.336 | 24.6 | 219.2 | 504.0 | 213.2 | 21.9 | 5.0 | 4.1 |
| 1916 | 228.4 | 14.341 | 14.336 | 25.3 | 218.1 | 14.342 | 14.337 | 24.4 | 226.6 | 503.8 | 220.6 | 22.5 | 3.3 | 6.4 |
| 1917 | 235.3 | 14.340 | 14.334 | 25.5 | 225.0 | 14.341 | 14.336 | 25.3 | 233.5 | 503.4 | 227.5 | 20.9 | 4.3 | 7.0 |
| 1918 | 239.2 | 14.340 | 14.335 | 23.7 | 228.9 | 14.341 | 14.336 | 23.5 | 237.4 | 503.5 | 231.4 | 21.7 | 5.0 | 2.7 |
| 1919 | 246.8 | 14.340 | 14.335 | 24.3 | 236.6 | 14.341 | 14.336 | 24.2 | 245.1 | 503.3 | 239.1 | 22.2 | 9.7 | -1.1 |
| 1920 | 255.4 | 14.340 | 14.335 | 23.8 | 245.2 | 14.342 | 14.337 | 24.6 | 253.7 | 503.3 | 247.7 | 22.5 | 6.3 | -3 |
| 1921 | 259.6 | 14.340 | 14.335 | 24.1 | 249.4 | 14.341 | 14.336 | 24.8 | 257.9 | 503.6 | 251.9 | 19.3 | 7.6 | -2.4 |
| 1922 | 264.9 | 14.340 | 14.336 | 23.3 | 254.6 | 14.342 | 14.337 | 24.2 | 263.1 | 503.4 | 257.1 | 21.3 | 2.4 | -4.9 |
| 1923 | 270.7 | 14.341 | 14.335 | 25.4 | 260.4 | 14.343 | 14.337 | 26.4 | 268.9 | 503.3 | 262.9 | 23.5 | 2.1 | -9 |
| 1924 | 276.3 | 14.342 | 14.336 | 25.6 | 266.1 | 14.342 | 14.337 | 25.2 | 274.6 | 503.2 | 268.6 | 22.8 | 8.8 | 2.2 |
| 1925 | 283.2 | 14.342 | 14.337 | 24.4 | 272.9 | 14.343 | 14.338 | 24.4 | 281.4 | 503.3 | 275.4 | 22.1 | 2.9 | -4.6 |
| 1926 | 287.1 | 14.341 | 14.336 | 23.7 | 276.9 | 14.342 | 14.338 | 23.6 | 285.4 | 503.2 | 279.4 | 23.8 | 2.0 | -4.0 |
| 1927 | 250.7 | 14.342 | 14.338 | 24.2 | 240.4 | 14.343 | 14.338 | 24.7 | 248.9 | 503.5 | 242.9 | 23.4 | 13.1 | 5.4 |
| 1928 | 215.4 | 14.342 | 14.338 | 24.0 | 205.2 | 14.343 | 14.339 | 24.1 | 213.7 | 503.4 | 207.7 | 21.3 | 3.5 | 0.1 |
| 1929 | 180.2 | 14.343 | 14.338 | 26.2 | 169.9 | 14.345 | 14.339 | 25.9 | 178.4 | 503.4 | 172.4 | 26.9 | 10.1 | 6.9 |
| 1930 | 144.1 | 14.345 | 14.337 | 30.7 | 133.9 | 14.345 | 14.338 | 29.6 | 142.4 | 503.2 | 136.4 | 27.0 | 3.1 | 6.7 |
| 1931 | 108.4 | 14.349 | 14.338 | 36.0 | 98.1 | 14.348 | 14.339 | 32.7 | 106.6 | 502.9 | 100.6 | 32.6 | 7.4 | 8.5 |
| 1932 | 73.5 | 14.357 | 14.340 | 44.6 | 63.3 | 14.354 | 14.340 | 41.6 | 71.8 | 502.9 | 65.8 | 40.8 | 4.1 | 6.7 |
| 1933 | 29.2 | 14.362 | 14.341 | 51.3 | 18.9 | 14.361 | 14.340 | 50.3 | 27.4 | 502.8 | 21.4 | 54.1 | 4.7 | 9.1 |

TABLE 7.—DATA LISTING FOR TRAVERSE 1 AT STATION 2—VERTICAL SURVEY
 [Test section data for reading 1934; total pressure, 14.333; static pressure, 13.234 psia; total temperature, 497° R; velocity, 250.2 mph; fan speed, 287.5 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1934 | 32.0 | 14.340 | 14.336 | 20.9 | 21.5 | 14.356 | 14.341 | 43.1 | 31.7 | 499.6 | 42.0 | 1.0 | 13.1 | |
| 1935 | 40.3 | 14.338 | 14.334 | 21.3 | 29.8 | 14.353 | 14.337 | 44.8 | 40.1 | 499.8 | 43.0 | 1.4 | 11.5 | |
| 1936 | 47.5 | 14.338 | 14.334 | 21.9 | 37.0 | 14.352 | 14.335 | 45.3 | 47.2 | 499.7 | 42.2 | .8 | 9.1 | |
| 1937 | 54.8 | 14.338 | 14.334 | 21.7 | 44.3 | 14.351 | 14.334 | 44.2 | 54.5 | 499.6 | 45.5 | -.4 | 9.7 | |
| 1938 | 61.3 | 14.339 | 14.335 | 21.8 | 50.8 | 14.349 | 14.333 | 44.1 | 61.1 | 499.5 | 56.1 | .7 | 5.8 | |
| 1939 | 69.3 | 14.338 | 14.334 | 22.4 | 58.8 | 14.349 | 14.333 | 43.4 | 69.0 | 499.7 | 64.0 | 0.7 | 7.9 | |
| 1940 | 76.6 | 14.339 | 14.334 | 23.6 | 66.1 | 14.348 | 14.332 | 43.4 | 76.3 | 500.1 | 71.3 | 45.0 | 3.6 | |
| 1941 | 83.2 | 14.339 | 14.334 | 24.5 | 72.7 | 14.346 | 14.330 | 43.5 | 83.0 | 500.7 | 78.0 | 42.6 | 2.2 | |
| 1942 | 90.7 | 14.338 | 14.333 | 24.5 | 80.2 | 14.342 | 14.327 | 41.8 | 90.4 | 501.9 | 85.4 | 41.0 | 1.6 | |
| 1943 | 97.8 | 14.340 | 14.334 | 25.5 | 87.3 | 14.341 | 14.327 | 41.3 | 97.5 | 502.6 | 92.5 | 39.8 | 2.8 | |
| 1944 | 105.0 | 14.340 | 14.335 | 24.4 | 94.5 | 14.341 | 14.328 | 39.6 | 104.8 | 502.7 | 99.8 | 38.4 | 2.9 | |
| 1945 | 112.9 | 14.343 | 14.338 | 23.9 | 102.4 | 14.342 | 14.330 | 37.3 | 112.7 | 501.9 | 107.7 | 34.4 | 4.3 | |
| 1946 | 119.3 | 14.345 | 14.340 | 24.1 | 108.8 | 14.347 | 14.336 | 37.2 | 119.1 | 500.9 | 114.1 | 34.7 | 4.1 | |
| 1947 | 126.1 | 14.343 | 14.339 | 23.3 | 115.6 | 14.345 | 14.334 | 35.1 | 125.8 | 501.5 | 120.8 | 34.0 | 1.5 | |
| 1948 | 134.2 | 14.342 | 14.338 | 22.2 | 123.7 | 14.343 | 14.333 | 33.9 | 133.9 | 501.9 | 128.9 | 30.9 | 3.7 | |
| 1949 | 141.6 | 14.342 | 14.338 | 22.4 | 131.1 | 14.342 | 14.333 | 32.0 | 141.4 | 502.2 | 136.4 | 30.6 | 4.6 | |
| 1950 | 149.6 | 14.341 | 14.337 | 20.9 | 139.1 | 14.340 | 14.332 | 30.7 | 149.4 | 502.5 | 144.4 | 29.8 | 4.0 | |
| 1951 | 155.2 | 14.344 | 14.340 | 20.4 | 144.7 | 14.342 | 14.335 | 29.1 | 154.9 | 502.3 | 149.9 | 26.5 | 3.3 | |
| 1952 | 162.3 | 14.344 | 14.341 | 19.9 | 151.8 | 14.342 | 14.335 | 28.1 | 162.1 | 502.0 | 157.1 | 25.7 | 2.1 | |
| 1953 | 169.0 | 14.343 | 14.341 | 18.7 | 158.5 | 14.342 | 14.336 | 26.7 | 168.7 | 501.8 | 163.7 | 26.1 | 5.9 | |
| 1954 | 176.1 | 14.343 | 14.340 | 20.5 | 165.6 | 14.342 | 14.336 | 27.9 | 175.9 | 502.0 | 170.9 | 25.7 | 3.8 | |
| 1955 | 183.8 | 14.342 | 14.339 | 18.6 | 173.3 | 14.341 | 14.335 | 25.4 | 183.6 | 502.1 | 178.6 | 21.8 | 3.3 | |
| 1956 | 190.2 | 14.342 | 14.339 | 18.8 | 179.7 | 14.340 | 14.335 | 24.7 | 190.0 | 502.3 | 185.0 | 22.9 | 3.1 | |
| 1957 | 197.5 | 14.342 | 14.340 | 17.3 | 187.0 | 14.340 | 14.336 | 23.0 | 197.3 | 502.1 | 192.3 | 20.0 | 5.2 | |
| 1958 | 204.5 | 14.342 | 14.339 | 17.1 | 194.0 | 14.339 | 14.335 | 22.6 | 204.2 | 502.1 | 199.2 | 20.8 | 2.6 | |
| | | | | | | | | | | | | | 2.0 | |

TABLE 7.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1959 | 211.9 | 14.343 | 14.340 | 17.6 | 201.4 | 14.340 | 14.336 | 22.0 | 211.7 | 502.0 | 206.7 | 18.5 | 4.4 | 3.5 |
| 1960 | 217.3 | 14.342 | 14.340 | 15.7 | 206.8 | 14.339 | 14.336 | 20.1 | 217.0 | 501.7 | 212.0 | 17.6 | 4.5 | -5.0 |
| 1961 | 223.8 | 14.343 | 14.341 | 15.2 | 213.3 | 14.340 | 14.336 | 21.0 | 223.6 | 501.6 | 218.6 | 18.7 | 2.5 | -6.0 |
| 1962 | 230.4 | 14.343 | 14.341 | 15.9 | 219.9 | 14.341 | 14.338 | 19.7 | 230.1 | 501.5 | 225.1 | 17.6 | 2.3 | -1.8 |
| 1963 | 237.1 | 14.342 | 14.341 | 14.5 | 226.6 | 14.341 | 14.338 | 19.4 | 236.8 | 501.4 | 231.8 | 18.3 | .2 | -7 |
| 1964 | 243.5 | 14.343 | 14.341 | 14.9 | 233.0 | 14.340 | 14.337 | 19.7 | 243.2 | 501.5 | 238.2 | 17.3 | 1.7 | -5.8 |
| 1965 | 251.3 | 14.343 | 14.341 | 15.6 | 240.8 | 14.339 | 14.336 | 18.2 | 251.0 | 501.6 | 246.0 | 17.1 | 5.2 | -1.2 |
| 1966 | 258.1 | 14.343 | 14.341 | 15.0 | 247.6 | 14.340 | 14.337 | 18.2 | 257.8 | 501.8 | 252.8 | 16.4 | .2 | -5.8 |
| 1967 | 265.6 | 14.343 | 14.341 | 14.9 | 255.1 | 14.338 | 14.336 | 17.6 | 265.3 | 501.8 | 260.3 | 16.0 | 3.1 | -7.1 |
| 1968 | 271.2 | 14.343 | 14.341 | 14.8 | 260.7 | 14.339 | 14.337 | 18.0 | 270.9 | 501.8 | 265.9 | 14.1 | -.7 | -8.8 |
| 1969 | 278.2 | 14.344 | 14.342 | 15.0 | 267.7 | 14.340 | 14.337 | 18.4 | 277.9 | 501.9 | 272.9 | 13.3 | -0.2 | -4.2 |
| 1970 | 284.6 | 14.344 | 14.342 | 15.5 | 274.1 | 14.340 | 14.338 | 17.6 | 284.3 | 501.7 | 279.3 | 12.4 | -1.1 | -8.2 |
| 1971 | 287.7 | 14.345 | 14.343 | 15.5 | 277.2 | 14.341 | 14.339 | 17.9 | 287.5 | 501.7 | 282.5 | 11.9 | 2.5 | -6.3 |
| 1972 | 250.4 | 14.345 | 14.343 | 15.7 | 239.9 | 14.341 | 14.338 | 19.2 | 250.2 | 501.7 | 245.2 | 15.2 | 1.3 | -2.3 |
| 1973 | 212.0 | 14.346 | 14.344 | 16.4 | 201.5 | 14.343 | 14.339 | 21.5 | 211.8 | 501.8 | 206.8 | 17.3 | 4.1 | -4.9 |
| 1974 | 176.3 | 14.347 | 14.344 | 18.3 | 165.8 | 14.345 | 14.339 | 26.0 | 176.0 | 501.6 | 171.0 | 22.4 | 4.0 | -0.1 |
| 1975 | 141.4 | 14.348 | 14.344 | 21.8 | 130.9 | 14.349 | 14.340 | 31.3 | 141.1 | 501.4 | 136.1 | 28.3 | 2.2 | 5.5 |
| 1976 | 110.2 | 14.349 | 14.345 | 23.6 | 99.7 | 14.352 | 14.340 | 37.9 | 110.0 | 501.4 | 105.0 | 35.7 | 2.5 | 11.6 |
| 1977 | 67.4 | 14.350 | 14.345 | 23.9 | 56.9 | 14.358 | 14.341 | 45.3 | 67.1 | 501.0 | 62.1 | 43.8 | 1.0 | 6.5 |
| 1978 | 31.8 | 14.350 | 14.345 | 22.2 | 21.3 | 14.357 | 14.341 | 43.8 | 31.6 | 501.1 | 26.6 | 43.0 | 1.4 | 12.1 |

TABLE 8.—DATA LISTING FOR TRAVERSE 2 AT STATION 2—VERTICAL SURVEY
 [Test section data for reading 1934; total pressure, 14.333; static pressure, 13.234 psia; total temperature, 49° R; velocity, 250.2 mph; fan speed, 287.5 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1934 | 29.2 | 14.347 | 14.336 | 36.7 | 18.9 | 14.347 | 14.336 | 35.8 | 27.4 | 498.4 | 21.4 | 38.1 | 4.3 | 7.8 |
| 1935 | 40.1 | 14.347 | 14.336 | 36.9 | 29.8 | 14.347 | 14.336 | 36.0 | 38.3 | 498.5 | 32.3 | 38.4 | 4.1 | 9.3 |
| 1936 | 47.1 | 14.346 | 14.335 | 36.1 | 36.8 | 14.346 | 14.336 | 35.2 | 45.3 | 498.4 | 39.3 | 37.1 | 2.7 | 9.9 |
| 1937 | 54.3 | 14.346 | 14.336 | 35.9 | 44.0 | 14.346 | 14.336 | 34.6 | 52.5 | 498.3 | 46.5 | 36.7 | 6.8 | 8.2 |
| 1938 | 61.1 | 14.346 | 14.336 | 34.2 | 50.9 | 14.346 | 14.337 | 32.8 | 59.4 | 498.3 | 53.4 | 34.4 | 2.9 | .6 |
| 1939 | 69.1 | 14.346 | 14.336 | 33.8 | 58.9 | 14.346 | 14.337 | 31.8 | 67.4 | 498.6 | 61.4 | 34.6 | 9.3 | 6.8 |
| 1940 | 76.2 | 14.346 | 14.337 | 32.1 | 66.0 | 14.345 | 14.338 | 30.2 | 74.5 | 499.1 | 68.5 | 31.0 | 7.2 | 5.4 |
| 1941 | 83.3 | 14.345 | 14.337 | 30.4 | 73.0 | 14.344 | 14.338 | 28.4 | 81.5 | 499.7 | 75.5 | 31.6 | 5.7 | 6.9 |
| 1942 | 90.3 | 14.345 | 14.338 | 28.9 | 80.1 | 14.345 | 14.339 | 27.0 | 88.6 | 500.9 | 82.6 | 26.7 | 4.0 | 4.1 |
| 1943 | 97.4 | 14.345 | 14.339 | 27.5 | 87.1 | 14.345 | 14.339 | 25.3 | 95.6 | 501.8 | 89.6 | 26.9 | 3.8 | 4.3 |
| 1944 | 104.8 | 14.345 | 14.340 | 24.9 | 94.5 | 14.345 | 14.340 | 23.5 | 103.0 | 501.9 | 97.0 | 25.2 | 4.5 | 3.1 |
| 1945 | 112.2 | 14.345 | 14.341 | 21.1 | 101.9 | 14.345 | 14.341 | 20.4 | 110.4 | 501.0 | 104.4 | 21.2 | 4.6 | 8.8 |
| 1946 | 119.0 | 14.345 | 14.341 | 22.7 | 108.8 | 14.345 | 14.341 | 21.2 | 117.3 | 500.0 | 111.3 | 20.8 | 5.4 | 7.5 |
| 1947 | 126.2 | 14.345 | 14.341 | 22.9 | 115.9 | 14.346 | 14.341 | 22.7 | 124.4 | 500.4 | 118.4 | 22.1 | 5.8 | 5.0 |
| 1948 | 134.3 | 14.345 | 14.341 | 20.7 | 124.1 | 14.346 | 14.342 | 21.0 | 132.6 | 501.0 | 126.6 | 20.4 | 6.8 | 4.9 |
| 1949 | 141.4 | 14.345 | 14.341 | 20.7 | 131.2 | 14.346 | 14.342 | 21.1 | 139.7 | 501.4 | 133.7 | 19.6 | 5.0 | 1.2 |
| 1950 | 149.3 | 14.345 | 14.341 | 20.8 | 139.1 | 14.346 | 14.342 | 21.3 | 147.6 | 501.8 | 141.6 | 20.5 | 5.5 | 5.8 |
| 1951 | 155.0 | 14.346 | 14.342 | 20.4 | 144.7 | 14.346 | 14.342 | 20.5 | 153.2 | 501.4 | 147.2 | 19.0 | 5.0 | 4.3 |
| 1952 | 162.6 | 14.346 | 14.343 | 21.2 | 152.3 | 14.346 | 14.343 | 20.9 | 160.8 | 501.2 | 154.8 | 19.2 | 2.4 | 7.7 |
| 1953 | 167.9 | 14.347 | 14.343 | 21.6 | 157.6 | 14.347 | 14.343 | 21.1 | 166.1 | 501.0 | 160.1 | 19.3 | 5.9 | 6.9 |
| 1954 | 176.1 | 14.345 | 14.342 | 20.2 | 165.9 | 14.346 | 14.343 | 20.5 | 174.4 | 501.3 | 168.4 | 19.2 | 3.3 | 3.7 |
| 1955 | 182.9 | 14.346 | 14.343 | 20.3 | 172.6 | 14.345 | 14.342 | 20.1 | 181.1 | 501.5 | 175.1 | 20.2 | 5.5 | 7.0 |
| 1956 | 189.8 | 14.346 | 14.342 | 20.6 | 179.6 | 14.346 | 14.342 | 19.9 | 188.1 | 501.6 | 182.1 | 19.5 | 2.4 | 4.4 |
| 1957 | 197.0 | 14.346 | 14.343 | 20.4 | 186.7 | 14.346 | 14.343 | 19.9 | 195.2 | 501.6 | 189.2 | 19.6 | 4.0 | 4.0 |
| 1958 | 204.3 | 14.345 | 14.342 | 19.0 | 194.1 | 14.346 | 14.343 | 18.6 | 202.6 | 501.6 | 196.6 | 17.4 | 8.8 | 1.8 |

TABLE 8.—Concluded.

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | | Wind anemometer | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1959 | 211.7 | 14.346 | 14.343 | 18.2 | 201.4 | 14.346 | 14.343 | 18.3 | 209.9 | 501.6 | 203.9 | 17.6 | 8.4 | 3.7 |
| 1960 | 217.4 | 14.347 | 14.343 | 19.8 | 207.2 | 14.346 | 14.343 | 19.9 | 215.7 | 501.4 | 209.7 | 18.1 | 6.9 | 1.2 |
| 1961 | 222.9 | 14.347 | 14.344 | 18.4 | 212.6 | 14.346 | 14.343 | 18.5 | 221.1 | 501.1 | 215.1 | 17.9 | 4.5 | 3.0 |
| 1962 | 230.2 | 14.346 | 14.343 | 17.5 | 220.0 | 14.346 | 14.344 | 18.1 | 228.5 | 501.0 | 222.5 | 17.6 | 5.7 | 3.9 |
| 1963 | 237.2 | 14.347 | 14.344 | 18.8 | 226.9 | 14.347 | 14.344 | 18.6 | 235.4 | 500.9 | 229.4 | 19.6 | 5.9 | 2.4 |
| 1964 | 242.6 | 14.347 | 14.344 | 18.2 | 232.4 | 14.346 | 14.343 | 18.7 | 240.9 | 501.2 | 234.9 | 19.1 | 5.8 | 2.2 |
| 1965 | 252.0 | 14.347 | 14.344 | 17.8 | 241.7 | 14.347 | 14.344 | 18.4 | 250.2 | 501.3 | 244.2 | 16.9 | 5.1 | -1.4 |
| 1966 | 258.3 | 14.347 | 14.345 | 16.8 | 248.1 | 14.347 | 14.344 | 18.0 | 256.6 | 501.6 | 250.6 | 17.0 | 3.0 | -6.1 |
| 1967 | 265.1 | 14.347 | 14.345 | 18.2 | 254.9 | 14.348 | 14.345 | 19.2 | 263.4 | 501.6 | 257.4 | 17.7 | 7.4 | -6.4 |
| 1968 | 271.0 | 14.348 | 14.345 | 18.1 | 260.7 | 14.348 | 14.345 | 18.4 | 269.2 | 501.6 | 263.2 | 16.5 | 4.7 | -4.4 |
| 1969 | 278.1 | 14.347 | 14.345 | 16.2 | 267.8 | 14.348 | 14.346 | 16.3 | 276.3 | 501.5 | 270.3 | 14.6 | 0.6 | -2.1 |
| 1970 | 283.4 | 14.348 | 14.346 | 16.4 | 273.1 | 14.348 | 14.346 | 16.8 | 281.6 | 501.5 | 275.6 | 14.4 | 8.4 | -3.7 |
| 1971 | 288.6 | 14.349 | 14.346 | 17.8 | 278.3 | 14.349 | 14.347 | 18.5 | 286.8 | 501.4 | 280.8 | 16.2 | 4.8 | -2.8 |
| 1972 | 249.1 | 14.349 | 14.346 | 17.9 | 238.8 | 14.349 | 14.346 | 18.2 | 247.3 | 501.5 | 241.3 | 16.2 | 6.4 | 4.0 |
| 1973 | 212.3 | 14.350 | 14.347 | 18.2 | 202.0 | 14.350 | 14.347 | 18.5 | 210.5 | 501.3 | 204.5 | 15.0 | .9 | 2.0 |
| 1974 | 176.4 | 14.351 | 14.348 | 19.5 | 166.1 | 14.351 | 14.348 | 19.5 | 174.6 | 500.9 | 168.6 | 19.2 | 4.1 | 1.9 |
| 1975 | 141.6 | 14.351 | 14.347 | 21.1 | 131.3 | 14.351 | 14.347 | 20.6 | 139.8 | 500.6 | 133.8 | 17.3 | 3.3 | 4.1 |
| 1976 | 110.0 | 14.353 | 14.348 | 24.7 | 99.8 | 14.353 | 14.348 | 22.6 | 108.3 | 500.1 | 102.3 | 21.4 | 8.0 | 1.6 |
| 1977 | 67.4 | 14.358 | 14.349 | 32.8 | 57.1 | 14.354 | 14.346 | 30.9 | 65.6 | 499.9 | 59.6 | 32.9 | 7.2 | 4.1 |
| 1978 | 29.2 | 14.361 | 14.349 | 37.6 | 18.9 | 14.359 | 14.348 | 36.6 | 27.4 | 499.6 | 21.4 | 37.3 | 2.2 | 7.3 |

TABLE 9.—DATA LISTING FOR TRAVERSE 1 AT STATION 2—HORIZONTAL SURVEY
[Test section data for reading 2098: total pressure, 14.297; static pressure, 12.213 psia; total temperature, 499 °R; velocity, 350.6 mph; fan speed, 387.2 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Pitch, deg | Yaw, deg |
| 2098 | 31.7 | 14.315 | 14.313 | 15.0 | 21.2 | 14.315 | 14.308 | 29.0 | 31.5 | 505.3 | 26.5 | -0.3 | -17.4 |
| 2099 | 38.5 | 14.314 | 14.312 | 15.0 | 28.0 | 14.314 | 14.307 | 29.1 | 38.2 | 505.6 | 33.2 | -4.0 | -17.4 |
| 2100 | 44.5 | 14.314 | 14.312 | 15.0 | 34.0 | 14.312 | 14.306 | 27.9 | 44.3 | 505.4 | 39.3 | -4.4 | -13.7 |
| 2101 | 50.9 | 14.314 | 14.313 | 12.3 | 40.4 | 14.313 | 14.307 | 27.9 | 50.6 | 505.3 | 45.6 | -6.0 | -15.6 |
| 2102 | 58.7 | 14.315 | 14.314 | 12.8 | 48.2 | 14.313 | 14.307 | 26.9 | 58.5 | 505.4 | 53.5 | -5.0 | -11.7 |
| 2103 | 66.9 | 14.316 | 14.314 | 12.2 | 56.4 | 14.314 | 14.308 | 27.8 | 66.6 | 505.1 | 61.6 | 26.0 | -7.7 |
| 2104 | 72.9 | 14.313 | 14.312 | 11.3 | 62.4 | 14.314 | 14.308 | 26.8 | 72.6 | 505.4 | 67.6 | 25.1 | -14.0 |
| 2105 | 79.2 | 14.315 | 14.314 | 10.8 | 68.7 | 14.314 | 14.308 | 25.7 | 79.0 | 505.2 | 74.0 | 24.1 | -13.1 |
| 2106 | 86.3 | 14.314 | 14.313 | 9.7 | 75.8 | 14.314 | 14.308 | 26.1 | 86.1 | 505.1 | 81.1 | 25.6 | -13.4 |
| 2107 | 93.7 | 14.312 | 14.311 | 11.3 | 83.2 | 14.313 | 14.308 | 25.6 | 93.4 | 504.9 | 88.4 | 23.1 | -6.6 |
| 2108 | 101.2 | 14.313 | 14.312 | 11.1 | 90.7 | 14.314 | 14.308 | 27.2 | 100.9 | 504.6 | 95.9 | 25.7 | -5.0 |
| 2109 | 108.2 | 14.312 | 14.311 | 8.6 | 97.7 | 14.314 | 14.307 | 28.8 | 108.0 | 504.6 | 103.0 | 26.1 | -5.9 |
| 2110 | 115.8 | 14.312 | 14.311 | 9.0 | 105.3 | 14.315 | 14.307 | 31.6 | 115.6 | 504.5 | 110.6 | 26.9 | -2.0 |
| 2111 | 121.5 | 14.312 | 14.311 | 9.8 | 111.0 | 14.314 | 14.308 | 28.9 | 121.3 | 504.6 | 116.3 | 26.9 | -12.7 |
| 2112 | 127.8 | 14.312 | 14.312 | 7.9 | 117.3 | 14.314 | 14.307 | 30.1 | 127.6 | 504.6 | 122.6 | 26.1 | -7.0 |
| 2113 | 135.2 | 14.312 | 14.311 | 8.9 | 124.7 | 14.315 | 14.307 | 30.5 | 134.9 | 504.5 | 129.9 | 25.0 | -3.1 |
| 2114 | 143.7 | 14.312 | 14.311 | 10.7 | 133.2 | 14.317 | 14.309 | 32.4 | 143.5 | 504.2 | 138.5 | 27.9 | -6.8 |
| 2115 | 150.4 | 14.313 | 14.312 | 12.2 | 139.9 | 14.317 | 14.308 | 34.0 | 150.2 | 504.4 | 145.2 | 30.1 | -3.9 |
| 2116 | 158.4 | 14.312 | 14.311 | 13.7 | 147.9 | 14.317 | 14.308 | 33.7 | 158.2 | 504.2 | 153.2 | 26.9 | 0.0 |
| 2117 | 165.3 | 14.312 | 14.311 | 13.9 | 154.8 | 14.318 | 14.308 | 34.1 | 165.0 | 504.0 | 160.0 | 30.2 | -4.2 |
| 2118 | 174.2 | 14.313 | 14.311 | 15.5 | 163.7 | 14.317 | 14.307 | 34.1 | 173.9 | 503.8 | 168.9 | 29.8 | -0.8 |
| 2119 | 181.2 | 14.313 | 14.310 | 16.3 | 170.7 | 14.317 | 14.307 | 34.2 | 180.9 | 503.7 | 175.9 | 30.4 | 1.1 |
| 2120 | 188.4 | 14.312 | 14.310 | 16.4 | 177.9 | 14.315 | 14.307 | 31.5 | 188.2 | 503.8 | 183.2 | 27.8 | -3.8 |
| 2121 | 196.7 | 14.313 | 14.310 | 19.2 | 186.2 | 14.315 | 14.306 | 32.4 | 196.5 | 503.6 | 191.5 | 28.2 | -1.7 |
| 2122 | 202.8 | 14.313 | 14.310 | 18.9 | 192.3 | 14.314 | 14.307 | 30.6 | 202.5 | 503.8 | 197.5 | 26.2 | -1.2 |

TABLE 9.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Pitch, deg | Yaw, deg |
| 2123 | 209.7 | 14.314 | 14.310 | 20.1 | 199.2 | 14.315 | 14.306 | 31.6 | 209.4 | 503.5 | 204.4 | -0.8 | -1.6 |
| 2124 | 217.2 | 14.313 | 14.310 | 18.0 | 206.7 | 14.312 | 14.305 | 27.8 | 216.9 | 503.5 | 211.9 | 2.9 | 2.8 |
| 2125 | 224.2 | 14.312 | 14.309 | 19.8 | 213.7 | 14.312 | 14.305 | 28.5 | 223.9 | 503.4 | 218.9 | .6 | 1.1 |
| 2126 | 230.5 | 14.313 | 14.311 | 16.7 | 220.0 | 14.312 | 14.306 | 26.3 | 230.3 | 503.4 | 225.3 | 3.4 | 4.3 |
| 2127 | 238.5 | 14.312 | 14.310 | 16.1 | 228.0 | 14.310 | 14.305 | 23.8 | 238.2 | 503.3 | 233.2 | 2.1 | -2.9 |
| 2128 | 244.7 | 14.312 | 14.309 | 17.5 | 234.2 | 14.310 | 14.306 | 23.2 | 244.4 | 503.3 | 239.4 | 20.7 | -0.6 |
| 2129 | 250.8 | 14.312 | 14.310 | 16.7 | 240.3 | 14.310 | 14.305 | 22.8 | 250.5 | 503.0 | 245.5 | 23.3 | -1.1 |
| 2130 | 257.6 | 14.312 | 14.310 | 16.9 | 247.1 | 14.309 | 14.305 | 21.6 | 257.4 | 503.1 | 252.4 | 23.3 | -8.4 |
| 2131 | 264.9 | 14.311 | 14.310 | 14.8 | 254.4 | 14.309 | 14.305 | 22.0 | 264.7 | 503.1 | 259.7 | 19.4 | .7 |
| 2132 | 271.9 | 14.312 | 14.310 | 13.8 | 261.4 | 14.308 | 14.305 | 18.9 | 271.6 | 502.8 | 266.6 | 22.5 | -5.0 |
| 2133 | 277.4 | 14.311 | 14.310 | 11.6 | 266.9 | 14.307 | 14.305 | 16.7 | 277.1 | 503.0 | 272.1 | 23.0 | -3.4 |
| 2134 | 285.3 | 14.311 | 14.309 | 14.5 | 274.8 | 14.309 | 14.306 | 19.4 | 285.0 | 502.9 | 280.0 | 24.1 | .4 |
| 2135 | 292.8 | 14.311 | 14.309 | 14.7 | 282.3 | 14.308 | 14.305 | 19.0 | 292.6 | 502.9 | 287.6 | 23.4 | 2.1 |
| 2136 | 297.4 | 14.311 | 14.310 | 13.8 | 286.9 | 14.308 | 14.305 | 17.3 | 297.1 | 502.9 | 292.1 | 25.1 | -1.9 |
| 2137 | 304.7 | 14.311 | 14.310 | 11.5 | 294.2 | 14.307 | 14.304 | 16.8 | 304.5 | 503.0 | 299.5 | 22.2 | 0.0 |
| 2138 | 312.0 | 14.311 | 14.310 | 11.3 | 301.5 | 14.308 | 14.306 | 15.3 | 311.8 | 503.0 | 306.8 | 33.5 | -0.4 |
| 2139 | 319.6 | 14.311 | 14.311 | 9.9 | 309.1 | 14.308 | 14.306 | 13.1 | 319.3 | 503.0 | 314.3 | 31.6 | -2.7 |
| 2140 | 321.6 | 14.312 | 14.311 | 11.2 | 311.1 | 14.309 | 14.306 | 16.8 | 321.3 | 503.0 | 316.3 | 25.4 | -4.0 |
| 2141 | 282.1 | 14.312 | 14.309 | 16.6 | 271.6 | 14.310 | 14.306 | 21.5 | 281.8 | 503.1 | 276.8 | 19.3 | -3.7 |
| 2142 | 240.3 | 14.312 | 14.310 | 16.1 | 229.8 | 14.310 | 14.306 | 22.8 | 240.1 | 503.1 | 235.1 | 20.8 | 7.0 |
| 2143 | 200.5 | 14.312 | 14.309 | 17.7 | 190.0 | 14.314 | 14.305 | 31.4 | 200.3 | 503.2 | 195.3 | -7.8 | -1.9 |
| 2144 | 160.7 | 14.312 | 14.310 | 13.1 | 150.2 | 14.315 | 14.305 | 34.1 | 160.5 | 503.6 | 155.5 | 27.9 | 5.0 |
| 2145 | 118.7 | 14.311 | 14.310 | 7.3 | 108.2 | 14.312 | 14.305 | 29.1 | 118.5 | 504.0 | 113.5 | 22.0 | -7.5 |
| 2146 | 70.6 | 14.312 | 14.310 | 12.3 | 60.1 | 14.311 | 14.306 | 25.5 | 70.3 | 504.1 | 65.3 | 22.4 | -18.0 |
| 2147 | 31.8 | 14.314 | 14.312 | 16.8 | 21.3 | 14.314 | 14.307 | 29.2 | 31.5 | 504.6 | 26.5 | -3.3 | -13.4 |

TABLE 10.—DATA LISTING FOR TRAVERSE 2 AT STATION 2—HORIZONTAL SURVEY
 [Test section data for reading 2098; total pressure, 14.297; static pressure, 12.213 psia; total temperature, 499 °R; velocity, 350.6 mph; fan speed, 387.2 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 2098 | 30.5 | 14.325 | 14.315 | 34.7 | 20.2 | 14.326 | 14.316 | 35.0 | 28.7 | 506.0 | 22.7 | 35.8 | 0.9 | -10.8 |
| 2099 | 37.5 | 14.325 | 14.315 | 34.8 | 27.2 | 14.326 | 14.316 | 35.3 | 35.7 | 506.1 | 29.7 | 34.6 | 1.4 | -13.8 |
| 2100 | 43.4 | 14.326 | 14.315 | 36.9 | 33.2 | 14.326 | 14.314 | 37.1 | 41.7 | 506.2 | 35.7 | 34.2 | 2.2 | -15.3 |
| 2101 | 49.0 | 14.326 | 14.315 | 36.1 | 38.8 | 14.326 | 14.315 | 36.0 | 47.3 | 506.1 | 41.3 | 34.8 | .8 | -6.3 |
| 2102 | 56.5 | 14.326 | 14.315 | 36.2 | 46.3 | 14.327 | 14.316 | 37.8 | 54.8 | 506.2 | 48.8 | 34.0 | 2.1 | -12.7 |
| 2103 | 63.8 | 14.328 | 14.317 | 37.4 | 53.5 | 14.329 | 14.317 | 38.5 | 62.0 | 506.3 | 56.0 | 34.6 | 6.2 | -12.3 |
| 2104 | 69.5 | 14.329 | 14.317 | 38.0 | 59.2 | 14.330 | 14.317 | 39.4 | 67.7 | 506.2 | 61.7 | 36.7 | 5.4 | -9.3 |
| 2105 | 75.4 | 14.331 | 14.317 | 40.4 | 65.1 | 14.332 | 14.317 | 42.8 | 73.6 | 506.3 | 67.6 | 38.5 | 8.5 | -9.7 |
| 2106 | 82.2 | 14.331 | 14.317 | 41.0 | 71.9 | 14.331 | 14.315 | 43.5 | 80.4 | 506.1 | 74.4 | 41.4 | 3.7 | -12.6 |
| 2107 | 88.6 | 14.331 | 14.316 | 43.2 | 78.3 | 14.332 | 14.315 | 45.7 | 86.8 | 505.9 | 80.8 | 43.7 | 5.6 | -9.0 |
| 2108 | 95.6 | 14.331 | 14.315 | 43.5 | 85.3 | 14.332 | 14.315 | 46.6 | 93.8 | 505.7 | 87.8 | 42.8 | 4.6 | -4.1 |
| 2109 | 102.4 | 14.333 | 14.315 | 46.8 | 92.1 | 14.334 | 14.314 | 49.8 | 100.6 | 505.7 | 94.6 | 47.2 | 7.5 | -3.0 |
| 2110 | 108.9 | 14.334 | 14.315 | 48.7 | 98.6 | 14.337 | 14.315 | 51.5 | 107.1 | 505.6 | 101.1 | 46.3 | .8 | -6.6 |
| 2111 | 114.2 | 14.336 | 14.316 | 49.9 | 103.9 | 14.339 | 14.316 | 53.0 | 112.4 | 505.7 | 106.4 | 47.3 | 8.6 | -3.7 |
| 2112 | 119.8 | 14.337 | 14.315 | 51.7 | 109.6 | 14.342 | 14.317 | 54.8 | 118.1 | 505.5 | 112.1 | 53.2 | 6.8 | -2.4 |
| 2113 | 127.0 | 14.337 | 14.316 | 51.4 | 116.8 | 14.341 | 14.316 | 54.7 | 125.3 | 505.4 | 119.3 | 49.7 | 3.7 | -1.5 |
| 2114 | 134.5 | 14.342 | 14.317 | 55.1 | 124.2 | 14.344 | 14.318 | 56.5 | 132.7 | 505.2 | 126.7 | 51.6 | 4.7 | 1.1 |
| 2115 | 141.0 | 14.343 | 14.317 | 56.3 | 130.7 | 14.345 | 14.318 | 57.6 | 139.2 | 505.0 | 133.2 | 55.9 | .4 | .4 |
| 2116 | 148.2 | 14.344 | 14.317 | 56.9 | 137.9 | 14.345 | 14.317 | 58.0 | 146.4 | 504.7 | 140.4 | 56.2 | 5.0 | -.8 |
| 2117 | 154.3 | 14.344 | 14.317 | 56.3 | 144.1 | 14.344 | 14.318 | 55.4 | 152.6 | 504.4 | 146.6 | 53.9 | 7.9 | -.6 |
| 2118 | 163.0 | 14.343 | 14.316 | 56.3 | 152.7 | 14.342 | 14.317 | 54.4 | 161.2 | 504.3 | 155.2 | 55.0 | 2.6 | 2.2 |
| 2119 | 169.5 | 14.341 | 14.316 | 54.6 | 159.3 | 14.341 | 14.318 | 52.8 | 167.8 | 504.1 | 161.8 | 51.8 | 5.6 | .9 |
| 2120 | 175.9 | 14.338 | 14.316 | 51.6 | 165.6 | 14.337 | 14.317 | 49.0 | 174.1 | 503.7 | 168.1 | 48.1 | 1.3 | 3.7 |
| 2121 | 183.2 | 14.339 | 14.316 | 52.1 | 172.9 | 14.336 | 14.316 | 49.4 | 181.4 | 503.6 | 175.4 | 44.1 | 2.5 | 3.4 |
| 2122 | 188.7 | 14.336 | 14.316 | 48.7 | 178.5 | 14.334 | 14.317 | 45.7 | 187.0 | 503.5 | 181.0 | 44.8 | 5.0 | 1.4 |

TABLE 10.—Concluded.

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|-----------------|----------|--|--|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg | | |
| 2123 | 195.1 | 14.334 | 14.315 | 47.9 | 184.9 | 14.333 | 14.316 | 45.5 | 193.4 | 503.5 | 187.4 | 43.6 | 3.1 | -0.3 | | |
| 2124 | 202.4 | 14.333 | 14.316 | 45.0 | 192.1 | 14.332 | 14.317 | 42.8 | 200.6 | 503.3 | 194.6 | 40.1 | 6.6 | 2.3 | | |
| 2125 | 208.9 | 14.332 | 14.316 | 44.0 | 198.7 | 14.329 | 14.315 | 41.3 | 207.2 | 503.2 | 201.2 | 39.0 | .9 | 1.5 | | |
| 2126 | 214.5 | 14.331 | 14.317 | 42.4 | 204.2 | 14.331 | 14.317 | 40.0 | 212.7 | 503.1 | 206.7 | 37.6 | .8 | 1.4 | | |
| 2127 | 221.8 | 14.330 | 14.316 | 40.9 | 211.5 | 14.328 | 14.316 | 38.5 | 220.0 | 503.0 | 214.0 | 37.0 | .9 | 4.8 | | |
| 2128 | 227.3 | 14.327 | 14.316 | 37.8 | 217.0 | 14.326 | 14.315 | 36.7 | 225.5 | 502.9 | 219.5 | 34.1 | 1.3 | 3.6 | | |
| 2129 | 232.5 | 14.327 | 14.315 | 38.4 | 222.2 | 14.326 | 14.315 | 35.6 | 230.7 | 502.9 | 224.7 | 33.0 | 1.7 | 4.6 | | |
| 2130 | 238.9 | 14.326 | 14.315 | 35.4 | 228.6 | 14.324 | 14.315 | 33.3 | 237.1 | 502.8 | 231.1 | 30.8 | -1.1 | .1 | | |
| 2131 | 245.4 | 14.325 | 14.315 | 34.0 | 235.2 | 14.323 | 14.315 | 31.7 | 243.7 | 502.8 | 237.7 | 32.7 | 1.5 | -1.7 | | |
| 2132 | 252.0 | 14.322 | 14.314 | 30.4 | 241.8 | 14.321 | 14.314 | 28.3 | 250.3 | 502.7 | 244.3 | 27.0 | 7.1 | 4.6 | | |
| 2133 | 257.5 | 14.323 | 14.315 | 31.2 | 247.3 | 14.322 | 14.315 | 29.8 | 255.8 | 502.6 | 249.8 | 29.5 | 1.2 | 0.8 | | |
| 2134 | 265.0 | 14.321 | 14.315 | 27.5 | 254.7 | 14.319 | 14.314 | 24.3 | 263.2 | 502.7 | 257.2 | 23.7 | -2.4 | .1 | | |
| 2135 | 271.5 | 14.320 | 14.315 | 25.9 | 261.3 | 14.320 | 14.315 | 24.6 | 269.8 | 502.7 | 263.8 | 21.9 | .9 | 4.2 | | |
| 2136 | 276.0 | 14.320 | 14.315 | 24.1 | 265.7 | 14.319 | 14.315 | 21.3 | 274.2 | 502.7 | 268.2 | 21.0 | 5.4 | -1.2 | | |
| 2137 | 282.0 | 14.319 | 14.314 | 24.4 | 271.7 | 14.318 | 14.314 | 22.7 | 280.2 | 502.7 | 274.2 | 21.3 | 4.0 | -1.8 | | |
| 2138 | 290.0 | 14.320 | 14.316 | 20.8 | 279.7 | 14.318 | 14.315 | 19.8 | 288.2 | 502.6 | 282.2 | 19.7 | -5.3 | -8.1 | | |
| 2139 | 295.8 | 14.320 | 14.316 | 20.9 | 285.5 | 14.319 | 14.316 | 20.5 | 294.0 | 502.6 | 288.0 | 22.2 | -2.4 | -2 | | |
| 2140 | 323.4 | 14.320 | 14.317 | 19.9 | 313.2 | 14.320 | 14.316 | 21.4 | 321.7 | 502.6 | 315.7 | 20.9 | -6.1 | -6 | | |
| 2141 | 262.2 | 14.323 | 14.316 | 28.5 | 251.9 | 14.321 | 14.315 | 25.9 | 260.4 | 502.9 | 254.4 | 21.9 | -.2 | -1.7 | | |
| 2142 | 223.8 | 14.330 | 14.316 | 40.7 | 213.6 | 14.329 | 14.317 | 38.8 | 222.1 | 503.1 | 216.1 | 36.3 | .7 | 2.6 | | |
| 2143 | 186.6 | 14.337 | 14.316 | 50.4 | 176.4 | 14.334 | 14.316 | 47.5 | 184.9 | 503.1 | 178.9 | 43.9 | 1.2 | 2.7 | | |
| 2144 | 149.8 | 14.343 | 14.315 | 57.5 | 139.5 | 14.344 | 14.317 | 57.0 | 148.0 | 504.2 | 142.0 | 57.0 | 1.9 | 2.3 | | |
| 2145 | 111.3 | 14.334 | 14.315 | 47.8 | 101.0 | 14.336 | 14.315 | 51.0 | 109.5 | 505.1 | 103.5 | 48.3 | 4.7 | -5.8 | | |
| 2146 | 67.4 | 14.328 | 14.316 | 38.3 | 57.1 | 14.329 | 14.316 | 39.4 | 65.6 | 505.3 | 59.6 | 34.1 | 3.3 | -11.2 | | |
| 2147 | 30.0 | 14.327 | 14.317 | 34.5 | 34.5 | 14.328 | 14.317 | 35.3 | 28.3 | 505.5 | 22.3 | 36.3 | 1.2 | -10.1 | | |

TABLE II.—DATA LISTING FOR TRAVERSE 1 AT STATION 2—HORIZONTAL SURVEY
 [Test section data for reading 2148; total pressure, 14,302; static pressure, 13,198; psia; total temperature, 499° R; velocity, 251.6 mph; fan speed, 287.8 rpm.]

| Reading number | Probe one | | | | | | Probe two | | | | | | Thermocouple | | | Wind anemometer | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|--------------|----------|--|-----------------|--|--|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg | | | | |
| 2148 | 32.6 | 14,314 | 14,313 | 13.4 | 22.1 | 14,301 | 14,296 | 23.1 | 32.3 | 502.6 | 27.3 | 22.3 | -1.4 | -13.3 | | | | |
| 2149 | 39.3 | 14,315 | 14,313 | 13.5 | 28.8 | 14,303 | 14,299 | 23.1 | 39.1 | 503.0 | 34.1 | 18.8 | -3.9 | -13.8 | | | | |
| 2150 | 46.8 | 14,314 | 14,313 | 11.7 | 36.3 | 14,303 | 14,299 | 21.8 | 46.6 | 503.1 | 41.6 | 17.8 | -2.8 | -13.0 | | | | |
| 2151 | 54.7 | 14,315 | 14,314 | 11.5 | 44.2 | 14,306 | 14,303 | 21.6 | 54.5 | 503.1 | 49.5 | 18.6 | -5.0 | -8.6 | | | | |
| 2152 | 61.6 | 14,315 | 14,314 | 10.1 | 51.1 | 14,309 | 14,305 | 19.3 | 61.4 | 502.7 | 56.4 | 16.2 | -8.2 | -14.0 | | | | |
| 2153 | 69.3 | 14,315 | 14,314 | 10.7 | 58.8 | 14,310 | 14,307 | 20.3 | 69.1 | 502.1 | 64.1 | 17.7 | -1.5 | -13.0 | | | | |
| 2154 | 76.8 | 14,316 | 14,315 | 10.1 | 66.3 | 14,314 | 14,310 | 21.3 | 76.6 | 501.6 | 71.6 | 18.6 | -3.8 | -10.1 | | | | |
| 2155 | 84.2 | 14,315 | 14,315 | 9.9 | 73.7 | 14,314 | 14,311 | 20.6 | 83.9 | 501.3 | 78.9 | 17.5 | -5.8 | -7.1 | | | | |
| 2156 | 92.6 | 14,314 | 14,314 | 9.9 | 82.1 | 14,314 | 14,311 | 20.7 | 92.3 | 501.1 | 87.3 | 18.5 | -5.0 | -7.4 | | | | |
| 2157 | 98.9 | 14,314 | 14,313 | 10.0 | 88.4 | 14,314 | 14,310 | 20.5 | 98.6 | 500.9 | 93.6 | 18.6 | -7.4 | -12.3 | | | | |
| 2158 | 105.6 | 14,313 | 14,312 | 9.4 | 95.1 | 14,314 | 14,310 | 21.9 | 105.3 | 500.8 | 100.3 | 20.6 | -6.2 | -9.7 | | | | |
| 2159 | 114.4 | 14,313 | 14,312 | 9.9 | 103.9 | 14,314 | 14,310 | 21.2 | 114.1 | 500.8 | 109.1 | 17.4 | -2.7 | -6.7 | | | | |
| 2160 | 121.2 | 14,312 | 14,311 | 8.6 | 110.7 | 14,314 | 14,310 | 22.7 | 121.0 | 500.7 | 116.0 | 19.6 | -5.8 | -4.1 | | | | |
| 2161 | 129.1 | 14,312 | 14,312 | 9.2 | 118.6 | 14,314 | 14,310 | 23.8 | 128.9 | 500.5 | 123.9 | 19.6 | -4.7 | -4.3 | | | | |
| 2162 | 135.9 | 14,312 | 14,311 | 11.0 | 125.4 | 14,314 | 14,309 | 25.5 | 135.6 | 500.7 | 130.6 | 21.1 | -5.9 | 1.0 | | | | |
| 2163 | 143.3 | 14,312 | 14,310 | 12.4 | 132.8 | 14,313 | 14,307 | 25.0 | 143.0 | 500.8 | 138.0 | 20.7 | -6.3 | 4.8 | | | | |
| 2164 | 151.7 | 14,312 | 14,311 | 11.9 | 141.2 | 14,312 | 14,307 | 24.8 | 151.4 | 500.8 | 146.4 | 19.7 | -1.1 | -3.1 | | | | |
| 2165 | 160.2 | 14,312 | 14,311 | 12.8 | 149.7 | 14,314 | 14,308 | 26.8 | 159.9 | 500.9 | 154.9 | 22.0 | -2.6 | 1.1 | | | | |
| 2166 | 167.5 | 14,312 | 14,311 | 14.1 | 157.0 | 14,313 | 14,308 | 26.0 | 167.3 | 501.0 | 162.3 | 20.1 | -1.4 | 4 | | | | |
| 2167 | 175.0 | 14,312 | 14,310 | 13.3 | 164.5 | 14,312 | 14,306 | 26.2 | 174.7 | 500.9 | 169.7 | 21.1 | -1.6 | -7 | | | | |
| 2168 | 184.8 | 14,312 | 14,311 | 12.9 | 171.3 | 14,312 | 14,307 | 24.5 | 181.5 | 501.0 | 176.5 | 20.2 | -0.5 | 2.1 | | | | |
| 2169 | 189.4 | 14,312 | 14,310 | 12.8 | 178.9 | 14,312 | 14,307 | 23.4 | 189.1 | 500.8 | 184.1 | 19.8 | -4 | .7 | | | | |
| 2170 | 198.1 | 14,312 | 14,311 | 14.3 | 187.6 | 14,312 | 14,307 | 23.6 | 197.9 | 500.8 | 192.9 | 19.2 | -1.5 | -1.2 | | | | |
| 2171 | 205.4 | 14,313 | 14,311 | 13.6 | 194.9 | 14,312 | 14,309 | 20.5 | 205.1 | 500.9 | 200.1 | 16.9 | -1 | 1.3 | | | | |
| 2172 | 213.7 | 14,313 | 14,311 | 14.7 | 203.2 | 14,313 | 14,309 | 21.6 | 213.5 | 500.7 | 208.5 | 18.7 | -3 | 1.1 | | | | |

TABLE 11.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg |
| 2173 | 220.7 | 14.312 | 14.311 | 14.4 | 210.2 | 14.312 | 14.308 | 20.7 | 220.5 | 500.8 | 215.5 | 17.0 | 0.7 |
| 2174 | 226.9 | 14.313 | 14.311 | 13.6 | 216.4 | 14.312 | 14.308 | 19.7 | 226.7 | 500.7 | 221.7 | 16.3 | -1.1 |
| 2175 | 233.7 | 14.313 | 14.311 | 13.7 | 223.2 | 14.312 | 14.309 | 18.7 | 233.4 | 500.6 | 228.4 | 16.3 | -2.8 |
| 2176 | 240.6 | 14.312 | 14.311 | 12.9 | 230.1 | 14.312 | 14.309 | 18.4 | 240.4 | 500.7 | 235.4 | 15.7 | -0.8 |
| 2177 | 248.3 | 14.312 | 14.311 | 13.0 | 237.8 | 14.312 | 14.309 | 18.5 | 248.1 | 500.8 | 243.1 | 14.7 | -2.9 |
| 2178 | 255.9 | 14.312 | 14.310 | 13.7 | 245.4 | 14.310 | 14.307 | 17.4 | 255.6 | 500.8 | 250.6 | 13.5 | 2.8 |
| 2179 | 262.2 | 14.312 | 14.311 | 12.3 | 251.7 | 14.311 | 14.309 | 17.1 | 262.0 | 500.9 | 257.0 | 15.6 | -6.1 |
| 2180 | 268.9 | 14.312 | 14.310 | 11.6 | 258.4 | 14.310 | 14.307 | 15.9 | 268.7 | 500.9 | 263.7 | 13.9 | 2.5 |
| 2181 | 275.8 | 14.311 | 14.310 | 11.3 | 265.3 | 14.310 | 14.308 | 15.1 | 275.5 | 501.0 | 270.5 | 14.4 | -4.7 |
| 2182 | 282.3 | 14.312 | 14.310 | 11.3 | 271.8 | 14.310 | 14.308 | 15.7 | 282.1 | 501.1 | 277.1 | 14.4 | -3.9 |
| 2183 | 289.2 | 14.312 | 14.310 | 11.5 | 278.7 | 14.310 | 14.307 | 16.9 | 288.9 | 501.2 | 283.9 | 14.5 | 1.0 |
| 2184 | 296.8 | 14.312 | 14.310 | 11.8 | 286.3 | 14.309 | 14.307 | 16.2 | 296.6 | 501.3 | 291.6 | 14.3 | -5.6 |
| 2185 | 304.2 | 14.311 | 14.310 | 11.2 | 293.7 | 14.310 | 14.308 | 16.5 | 304.0 | 501.1 | 299.0 | 13.5 | -5 |
| 2186 | 311.4 | 14.311 | 14.310 | 10.1 | 300.9 | 14.310 | 14.308 | 14.1 | 311.1 | 501.2 | 306.1 | 14.8 | -6.2 |
| 2187 | 321.9 | 14.312 | 14.311 | 10.7 | 311.4 | 14.309 | 14.307 | 15.2 | 321.7 | 501.3 | 316.7 | 13.7 | -2.3 |
| 2188 | 282.5 | 14.312 | 14.311 | 10.9 | 272.0 | 14.311 | 14.309 | 15.5 | 282.2 | 501.1 | 277.2 | 12.8 | -0.3 |
| 2189 | 243.2 | 14.313 | 14.312 | 13.1 | 232.8 | 14.313 | 14.310 | 19.0 | 243.0 | 500.9 | 238.0 | 14.8 | -1.8 |
| 2190 | 201.0 | 14.313 | 14.311 | 14.5 | 190.5 | 14.314 | 14.310 | 22.7 | 200.7 | 501.0 | 195.7 | 17.8 | -1.0 |
| 2191 | 161.8 | 14.312 | 14.311 | 12.1 | 151.3 | 14.315 | 14.310 | 25.1 | 161.5 | 501.3 | 156.5 | 21.6 | -3.7 |
| 2192 | 121.3 | 14.312 | 14.311 | 9.9 | 110.8 | 14.313 | 14.309 | 21.7 | 121.1 | 501.9 | 116.1 | 18.3 | -6.4 |
| 2193 | 74.8 | 14.313 | 14.312 | 10.3 | 64.3 | 14.314 | 14.310 | 21.3 | 74.5 | 502.2 | 69.5 | 19.1 | -5.0 |
| 2194 | 31.8 | 14.314 | 14.312 | 13.3 | 21.3 | 14.316 | 14.311 | 22.9 | 31.5 | 502.2 | 26.5 | 19.7 | -12.6 |

TABLE 12.—DATA LISTING FOR TRAVERSE 2 AT STATION 2—HORIZONTAL SURVEY
 [Test section data for reading 2148: total pressure, 14.302; static pressure, 13.198 psia; total temperature, 499°R; velocity, 251.6 mph; fan speed, 287.8 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg |
| 2148 | 30.5 | 14.332 | 14.326 | 27.2 | 20.3 | 14.334 | 14.327 | 29.0 | 28.8 | 502.4 | 22.8 | 28.8 | -8.0 |
| 2149 | 39.1 | 14.332 | 14.326 | 28.7 | 28.9 | 14.333 | 14.326 | 29.6 | 37.4 | 502.9 | 31.4 | 30.4 | -12.1 |
| 2150 | 46.5 | 14.332 | 14.325 | 29.1 | 36.3 | 14.334 | 14.326 | 30.1 | 44.8 | 503.1 | 38.8 | 33.0 | .8 |
| 2151 | 54.5 | 14.332 | 14.325 | 29.6 | 44.2 | 14.333 | 14.325 | 31.3 | 52.7 | 502.9 | 46.7 | 32.1 | -4.5 |
| 2152 | 61.2 | 14.332 | 14.324 | 30.7 | 50.9 | 14.333 | 14.324 | 32.3 | 59.4 | 502.6 | 53.4 | 34.4 | -6.6 |
| 2153 | 69.6 | 14.331 | 14.323 | 30.7 | 59.3 | 14.331 | 14.323 | 31.9 | 67.8 | 501.9 | 61.8 | 32.9 | -10.4 |
| 2154 | 76.5 | 14.331 | 14.323 | 32.4 | 66.3 | 14.333 | 14.323 | 34.3 | 74.8 | 501.4 | 68.8 | 34.4 | 4.0 |
| 2155 | 84.2 | 14.331 | 14.322 | 33.4 | 73.9 | 14.333 | 14.323 | 35.1 | 82.4 | 501.1 | 76.4 | 35.7 | 5.0 |
| 2156 | 92.0 | 14.332 | 14.322 | 34.7 | 81.8 | 14.333 | 14.321 | 36.9 | 90.3 | 500.9 | 84.3 | 37.9 | -3.7 |
| 2157 | 98.3 | 14.332 | 14.321 | 36.5 | 88.1 | 14.334 | 14.321 | 38.6 | 96.6 | 500.6 | 90.6 | 39.4 | 3.7 |
| 2158 | 105.4 | 14.333 | 14.322 | 36.9 | 95.2 | 14.334 | 14.322 | 38.9 | 103.7 | 500.6 | 97.7 | 39.9 | 6.6 |
| 2159 | 114.5 | 14.332 | 14.320 | 38.3 | 104.2 | 14.335 | 14.321 | 40.2 | 112.7 | 500.4 | 106.7 | 41.2 | 6.0 |
| 2160 | 121.6 | 14.333 | 14.320 | 39.5 | 111.4 | 14.335 | 14.321 | 40.8 | 119.9 | 500.2 | 113.9 | 40.3 | -1.6 |
| 2161 | 129.3 | 14.334 | 14.320 | 41.0 | 119.1 | 14.336 | 14.321 | 41.5 | 127.6 | 500.0 | 121.6 | 42.5 | -2.6 |
| 2162 | 135.6 | 14.334 | 14.320 | 41.0 | 125.4 | 14.335 | 14.321 | 41.3 | 133.9 | 500.3 | 127.9 | 42.1 | -1.0 |
| 2163 | 143.7 | 14.334 | 14.320 | 41.9 | 133.4 | 14.334 | 14.319 | 41.5 | 141.9 | 500.2 | 135.9 | 42.6 | -6 |
| 2164 | 151.7 | 14.334 | 14.320 | 41.0 | 141.4 | 14.333 | 14.320 | 40.3 | 149.9 | 500.1 | 143.9 | 40.6 | 4.4 |
| 2165 | 160.0 | 14.332 | 14.320 | 38.4 | 149.7 | 14.333 | 14.321 | 37.3 | 158.2 | 500.1 | 152.2 | 40.1 | -1.2 |
| 2166 | 167.5 | 14.332 | 14.320 | 37.9 | 157.2 | 14.331 | 14.320 | 35.9 | 165.7 | 500.1 | 159.7 | 36.2 | 1.4 |
| 2167 | 174.8 | 14.331 | 14.320 | 36.9 | 164.6 | 14.329 | 14.319 | 34.6 | 173.1 | 500.0 | 167.1 | 36.6 | -4 |
| 2168 | 181.5 | 14.331 | 14.320 | 35.6 | 171.3 | 14.329 | 14.320 | 33.6 | 179.8 | 500.1 | 173.8 | 34.4 | 2.0 |
| 2169 | 189.3 | 14.328 | 14.319 | 32.4 | 179.0 | 14.327 | 14.319 | 30.3 | 187.5 | 500.0 | 181.5 | 31.8 | 0.0 |
| 2170 | 198.5 | 14.328 | 14.320 | 31.1 | 188.3 | 14.326 | 14.319 | 29.1 | 196.8 | 499.8 | 190.8 | 31.6 | -1.4 |
| 2171 | 205.6 | 14.326 | 14.320 | 27.6 | 195.4 | 14.325 | 14.320 | 26.1 | 203.9 | 499.9 | 197.9 | 27.3 | 2.2 |
| 2172 | 213.5 | 14.326 | 14.320 | 27.4 | 203.3 | 14.325 | 14.319 | 26.3 | 211.8 | 499.7 | 205.8 | 28.3 | 1.9 |

TABLE 12.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 2173 | 220.4 | 14.325 | 14.319 | 25.0 | 210.2 | 14.324 | 14.319 | 24.3 | 218.7 | 499.8 | 212.7 | 25.1 | 2.4 | 0.2 |
| 2174 | 226.4 | 14.325 | 14.319 | 25.8 | 216.2 | 14.324 | 14.319 | 25.6 | 224.7 | 499.7 | 218.7 | 26.1 | -.8 | 1.5 |
| 2175 | 233.4 | 14.324 | 14.319 | 25.1 | 223.1 | 14.324 | 14.319 | 24.0 | 231.6 | 499.8 | 225.6 | 24.5 | .7 | 1.4 |
| 2176 | 240.6 | 14.324 | 14.320 | 22.9 | 230.3 | 14.324 | 14.320 | 22.6 | 238.8 | 499.9 | 232.8 | 24.3 | 3.6 | 1.7 |
| 2177 | 248.4 | 14.323 | 14.319 | 22.2 | 238.1 | 14.324 | 14.320 | 21.5 | 246.6 | 500.0 | 240.6 | 22.3 | -1.7 | -.1 |
| 2178 | 254.9 | 14.323 | 14.319 | 21.4 | 244.7 | 14.323 | 14.319 | 21.4 | 253.2 | 500.1 | 247.2 | 21.4 | -3.8 | -1.5 |
| 2179 | 262.0 | 14.323 | 14.319 | 22.5 | 251.7 | 14.323 | 14.319 | 22.0 | 260.2 | 500.1 | 254.2 | 22.6 | 1.5 | -1.0 |
| 2180 | 268.5 | 14.322 | 14.318 | 19.8 | 258.2 | 14.322 | 14.319 | 20.0 | 266.7 | 500.4 | 260.7 | 19.4 | -1.2 | 1.6 |
| 2181 | 275.0 | 14.323 | 14.319 | 20.2 | 264.7 | 14.321 | 14.318 | 19.4 | 273.2 | 500.5 | 267.2 | 19.8 | .1 | -1.6 |
| 2182 | 282.0 | 14.322 | 14.318 | 19.2 | 271.7 | 14.320 | 14.317 | 19.1 | 280.2 | 500.5 | 274.2 | 19.6 | 2.9 | -.4 |
| 2183 | 288.9 | 14.322 | 14.318 | 19.9 | 278.6 | 14.322 | 14.318 | 19.6 | 287.1 | 500.4 | 281.1 | 18.8 | -1.3 | 0.4 |
| 2184 | 296.5 | 14.321 | 14.319 | 16.3 | 286.3 | 14.320 | 14.318 | 17.1 | 294.8 | 500.6 | 288.8 | 17.2 | 1.0 | -3.4 |
| 2185 | 304.4 | 14.321 | 14.318 | 18.8 | 294.2 | 14.322 | 14.318 | 19.8 | 302.7 | 500.7 | 296.7 | 19.0 | .1 | 2.4 |
| 2186 | 311.9 | 14.321 | 14.318 | 18.6 | 301.6 | 14.321 | 14.318 | 20.1 | 310.1 | 500.7 | 304.1 | 19.2 | 2.8 | 1.3 |
| 2187 | 323.5 | 14.322 | 14.319 | 19.6 | 313.3 | 14.322 | 14.318 | 20.9 | 321.8 | 500.6 | 315.8 | 21.5 | -2.7 | 3.0 |
| 2188 | 282.5 | 14.322 | 14.319 | 18.6 | 272.3 | 14.322 | 14.319 | 19.4 | 280.8 | 500.6 | 274.8 | 19.2 | 1.8 | 2.6 |
| 2189 | 243.6 | 14.324 | 14.319 | 22.9 | 233.3 | 14.324 | 14.320 | 21.6 | 241.8 | 500.2 | 235.8 | 21.0 | 1.1 | 3.5 |
| 2190 | 200.5 | 14.327 | 14.320 | 30.5 | 190.2 | 14.327 | 14.320 | 29.0 | 198.7 | 500.2 | 192.7 | 28.4 | 2.0 | 0.0 |
| 2191 | 161.3 | 14.332 | 14.319 | 39.8 | 151.0 | 14.333 | 14.321 | 38.2 | 159.5 | 500.6 | 153.5 | 36.7 | 5.0 | 2.1 |
| 2192 | 121.0 | 14.334 | 14.320 | 40.9 | 110.7 | 14.335 | 14.320 | 42.2 | 119.2 | 501.6 | 113.2 | 40.5 | 3.7 | -1.0 |
| 2193 | 74.6 | 14.330 | 14.321 | 32.5 | 64.3 | 14.331 | 14.321 | 34.4 | 72.8 | 502.2 | 66.8 | 35.1 | 3.0 | -8.2 |
| 2194 | 30.0 | 14.326 | 14.320 | 26.7 | 19.7 | 14.326 | 14.319 | 28.2 | 28.2 | 502.3 | 22.2 | 28.6 | 2.5 | -9.1 |

TABLE 13.—DATA LISTING FOR TRAVERSE 1 AT STATION 3—VERTICAL SURVEY
 [Test section data for reading 1629; total pressure, 14.254; static pressure, 12.179 psia; total temperature, 498 °R; velocity, 349.8 mph; fan speed, 384.7 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1626 | 32.2 | 14.331 | 14.321 | 35.1 | 21.7 | 14.333 | 14.320 | 38.8 | 32.0 | 500.6 | 27.0 | 39.6 | 28.6 | 2.8 |
| 1627 | 38.6 | 14.331 | 14.319 | 38.4 | 28.1 | 14.334 | 14.320 | 41.2 | 38.3 | 504.1 | 33.3 | 42.9 | 27.0 | 2.5 |
| 1628 | 44.7 | 14.331 | 14.318 | 39.7 | 34.2 | 14.333 | 14.319 | 41.5 | 44.4 | 503.3 | 39.4 | 43.0 | 22.7 | 2.7 |
| 1629 | 50.4 | 14.331 | 14.318 | 39.3 | 39.9 | 14.332 | 14.318 | 41.0 | 50.1 | 501.5 | 45.1 | 42.6 | 24.6 | 3.0 |
| 1630 | 56.1 | 14.331 | 14.317 | 41.4 | 45.6 | 14.333 | 14.318 | 41.8 | 55.8 | 501.6 | 50.8 | 47.0 | 21.2 | 2.9 |
| 1631 | 62.6 | 14.332 | 14.318 | 41.6 | 52.1 | 14.334 | 14.320 | 42.1 | 62.3 | 502.2 | 57.3 | 45.7 | 22.3 | 2.4 |
| 1632 | 68.5 | 14.333 | 14.319 | 41.4 | 58.0 | 14.333 | 14.319 | 41.1 | 68.2 | 502.7 | 63.2 | 46.3 | 24.4 | 3.1 |
| 1633 | 74.1 | 14.334 | 14.319 | 42.5 | 63.6 | 14.334 | 14.319 | 42.3 | 73.9 | 502.6 | 68.9 | 46.0 | 23.3 | 2.6 |
| 1634 | 80.5 | 14.334 | 14.320 | 40.8 | 70.0 | 14.334 | 14.321 | 39.9 | 80.2 | 502.6 | 75.2 | 45.9 | 24.1 | 3.0 |
| 1635 | 86.8 | 14.333 | 14.320 | 39.9 | 76.3 | 14.334 | 14.322 | 38.1 | 86.5 | 502.5 | 81.5 | 43.0 | 22.3 | 3.2 |
| 1636 | 92.5 | 14.333 | 14.321 | 39.4 | 82.0 | 14.333 | 14.322 | 36.0 | 92.3 | 502.6 | 87.3 | 42.7 | 23.3 | 3.2 |
| 1637 | 98.8 | 14.334 | 14.321 | 38.7 | 88.3 | 14.333 | 14.322 | 36.5 | 98.6 | 502.7 | 93.6 | 40.5 | 22.0 | 2.3 |
| 1638 | 104.4 | 14.332 | 14.322 | 35.4 | 93.9 | 14.333 | 14.323 | 34.8 | 104.1 | 502.8 | 99.1 | 39.2 | 22.8 | 2.5 |
| 1639 | 110.3 | 14.331 | 14.322 | 34.5 | 99.8 | 14.332 | 14.322 | 34.2 | 110.1 | 502.8 | 105.1 | 39.8 | 21.7 | 3.1 |
| 1640 | 116.6 | 14.331 | 14.322 | 33.7 | 106.1 | 14.332 | 14.322 | 33.5 | 116.3 | 502.8 | 111.3 | 37.0 | 21.5 | 2.2 |
| 1641 | 122.6 | 14.331 | 14.322 | 32.5 | 112.1 | 14.331 | 14.322 | 32.0 | 122.3 | 502.6 | 117.3 | 36.6 | 20.9 | 3.6 |
| 1642 | 128.4 | 14.331 | 14.321 | 34.1 | 117.9 | 14.332 | 14.323 | 33.6 | 128.1 | 502.6 | 123.1 | 37.8 | 17.8 | 3.0 |
| 1643 | 134.3 | 14.330 | 14.321 | 33.4 | 123.8 | 14.331 | 14.322 | 33.0 | 134.0 | 502.6 | 129.0 | 36.0 | 17.3 | 3.4 |
| 1644 | 140.8 | 14.329 | 14.321 | 32.2 | 130.3 | 14.329 | 14.321 | 31.7 | 140.6 | 502.6 | 135.6 | 37.5 | 17.9 | 4.0 |
| 1645 | 146.6 | 14.329 | 14.321 | 31.8 | 136.1 | 14.329 | 14.321 | 31.4 | 146.4 | 502.5 | 141.4 | 35.9 | 22.5 | 5.1 |
| 1646 | 152.2 | 14.328 | 14.320 | 30.0 | 141.7 | 14.328 | 14.320 | 29.8 | 151.9 | 502.7 | 146.9 | 34.9 | 19.7 | 4.2 |
| 1647 | 158.4 | 14.328 | 14.320 | 31.3 | 147.9 | 14.327 | 14.319 | 31.2 | 158.2 | 503.0 | 153.2 | 37.2 | 19.7 | 4.5 |
| 1648 | 164.7 | 14.327 | 14.320 | 30.3 | 154.2 | 14.327 | 14.320 | 30.1 | 164.4 | 503.2 | 159.4 | 34.9 | 23.1 | 4.3 |
| 1649 | 170.3 | 14.326 | 14.319 | 29.8 | 159.8 | 14.326 | 14.319 | 29.2 | 170.0 | 503.1 | 165.0 | 34.5 | 16.7 | 4.8 |
| 1650 | 176.5 | 14.324 | 14.317 | 29.4 | 166.0 | 14.325 | 14.318 | 28.2 | 176.3 | 503.1 | 171.3 | 33.7 | 18.4 | 4.5 |

TABLE 13.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1651 | 182.6 | 14.324 | 14.318 | 28.1 | 172.1 | 14.324 | 14.318 | 27.3 | 182.3 | 503.0 | 177.3 | 30.9 | 17.4 | 4.4 |
| 1652 | 188.6 | 14.325 | 14.318 | 28.9 | 178.1 | 14.324 | 14.317 | 28.9 | 188.4 | 503.0 | 183.4 | 35.2 | 15.1 | 3.9 |
| 1653 | 194.3 | 14.325 | 14.319 | 26.8 | 183.8 | 14.324 | 14.318 | 27.2 | 194.0 | 502.8 | 189.0 | 31.2 | 14.2 | 4.6 |
| 1654 | 200.2 | 14.324 | 14.318 | 27.1 | 189.7 | 14.324 | 14.318 | 27.7 | 199.9 | 502.8 | 194.9 | 32.0 | 11.1 | 3.8 |
| 1655 | 206.4 | 14.325 | 14.318 | 27.3 | 195.9 | 14.325 | 14.318 | 28.0 | 206.1 | 502.8 | 201.1 | 33.2 | 13.3 | 2.5 |
| 1656 | 212.2 | 14.324 | 14.318 | 26.5 | 201.7 | 14.324 | 14.318 | 26.8 | 211.9 | 502.8 | 206.9 | 30.2 | 14.5 | 2.1 |
| 1657 | 218.3 | 14.323 | 14.317 | 26.4 | 207.8 | 14.324 | 14.318 | 26.8 | 218.0 | 503.1 | 213.0 | 30.4 | 9.3 | 1.7 |
| 1658 | 224.6 | 14.324 | 14.318 | 26.9 | 214.1 | 14.325 | 14.319 | 27.0 | 224.3 | 503.2 | 219.3 | 32.2 | 10.8 | 1.8 |
| 1659 | 230.1 | 14.323 | 14.318 | 26.5 | 219.6 | 14.323 | 14.318 | 26.7 | 229.9 | 503.1 | 224.9 | 30.7 | 13.3 | 1.2 |
| 1660 | 236.7 | 14.324 | 14.318 | 25.6 | 226.2 | 14.324 | 14.318 | 25.8 | 236.4 | 503.0 | 231.4 | 29.4 | 11.0 | .2 |
| 1661 | 242.5 | 14.323 | 14.317 | 26.5 | 232.0 | 14.323 | 14.318 | 25.7 | 242.3 | 503.0 | 237.3 | 29.0 | 15.1 | 0.6 |
| 1662 | 248.2 | 14.321 | 14.316 | 25.8 | 237.7 | 14.323 | 14.317 | 25.3 | 248.0 | 503.0 | 243.0 | 28.7 | 12.8 | 0.0 |
| 1663 | 254.2 | 14.321 | 14.316 | 25.3 | 243.7 | 14.322 | 14.317 | 24.2 | 254.0 | 503.2 | 249.0 | 27.4 | 17.9 | -.5 |
| 1664 | 260.4 | 14.319 | 14.314 | 23.3 | 249.9 | 14.322 | 14.317 | 23.5 | 260.2 | 503.2 | 255.2 | 25.2 | 12.8 | -.8 |
| 1665 | 266.3 | 14.320 | 14.315 | 24.2 | 255.8 | 14.321 | 14.316 | 24.3 | 266.0 | 503.3 | 261.0 | 27.2 | 9.9 | -1.5 |
| 1666 | 272.2 | 14.319 | 14.315 | 23.0 | 261.7 | 14.321 | 14.317 | 23.1 | 271.9 | 503.2 | 266.9 | 24.6 | 11.5 | -1.6 |
| 1667 | 278.7 | 14.320 | 14.316 | 22.2 | 268.2 | 14.322 | 14.318 | 21.7 | 278.4 | 503.2 | 273.4 | 25.1 | 15.3 | -2.3 |
| 1668 | 284.8 | 14.321 | 14.317 | 22.2 | 274.3 | 14.322 | 14.318 | 22.0 | 284.6 | 503.0 | 279.6 | 24.5 | 14.5 | -2.0 |
| 1669 | 290.3 | 14.321 | 14.317 | 22.6 | 279.8 | 14.322 | 14.318 | 21.8 | 290.1 | 503.1 | 285.1 | 24.5 | 11.0 | -2.6 |
| 1670 | 292.2 | 14.321 | 14.317 | 20.8 | 281.7 | 14.322 | 14.319 | 19.9 | 292.0 | 503.2 | 287.0 | 22.7 | 15.4 | -2.7 |
| 1671 | 254.4 | 14.324 | 14.318 | 25.3 | 243.9 | 14.324 | 14.319 | 24.6 | 254.1 | 503.2 | 249.1 | 27.9 | 14.0 | -0.4 |
| 1672 | 218.9 | 14.324 | 14.318 | 27.3 | 208.4 | 14.324 | 14.318 | 27.9 | 218.6 | 502.9 | 213.6 | 32.8 | 10.7 | 2.3 |
| 1673 | 182.6 | 14.325 | 14.318 | 27.9 | 172.1 | 14.325 | 14.318 | 27.6 | 182.4 | 502.8 | 177.4 | 31.8 | 14.0 | 4.5 |
| 1674 | 146.8 | 14.329 | 14.319 | 33.4 | 136.3 | 14.328 | 14.319 | 32.9 | 146.5 | 502.5 | 141.5 | 37.0 | 19.9 | 4.5 |
| 1675 | 110.6 | 14.330 | 14.320 | 35.3 | 100.1 | 14.331 | 14.320 | 35.8 | 110.4 | 502.6 | 105.4 | 40.7 | 19.7 | 2.5 |
| 1676 | 74.4 | 14.335 | 14.320 | 42.1 | 63.9 | 14.335 | 14.321 | 41.9 | 74.2 | 502.6 | 69.2 | 47.6 | 25.5 | 2.7 |
| 1677 | 38.8 | 14.334 | 14.322 | 38.2 | 28.3 | 14.336 | 14.322 | 40.9 | 38.5 | 502.9 | 33.5 | 45.1 | 25.2 | 2.6 |
| 1678 | 32.3 | 14.333 | 14.322 | 36.1 | 21.8 | 14.336 | 14.323 | 39.3 | 32.0 | 502.9 | 27.0 | 40.5 | 30.0 | 2.4 |

TABLE 14.—DATA LISTING FOR TRAVERSE 2 AT STATION 3—VERTICAL SURVEY
 [Test section data for reading 1629; total pressure, 14.254; static pressure, 12.179 psia; total temperature, 498 °R; velocity, 349.8 mph; fan speed, 384.7 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1626 | 32.5 | 14.350 | 14.326 | 53.0 | 22.3 | 14.345 | 14.327 | 45.3 | 30.8 | 502.5 | 24.8 | 53.3 | -26.4 | -4.5 |
| 1627 | 38.1 | 14.345 | 14.322 | 52.8 | 27.8 | 14.342 | 14.321 | 50.9 | 36.3 | 505.9 | 30.3 | 53.1 | -27.8 | -4.8 |
| 1628 | 44.4 | 14.341 | 14.317 | 52.9 | 34.1 | 14.342 | 14.319 | 52.1 | 42.6 | 505.3 | 36.6 | 56.1 | -25.8 | -4.8 |
| 1629 | 50.5 | 14.347 | 14.323 | 54.4 | 40.2 | 14.342 | 14.320 | 52.7 | 48.7 | 503.1 | 42.7 | 56.7 | -25.6 | -4.8 |
| 1630 | 56.1 | 14.348 | 14.325 | 53.1 | 45.9 | 14.343 | 14.320 | 52.2 | 54.4 | 503.1 | 48.4 | 54.6 | -27.4 | -4.7 |
| | | | | | | | | | | | | | | |
| 1631 | 62.5 | 14.345 | 14.323 | 51.9 | 52.2 | 14.343 | 14.319 | 53.1 | 60.7 | 503.9 | 54.7 | 55.4 | -26.1 | -4.9 |
| 1632 | 68.4 | 14.346 | 14.323 | 52.9 | 58.2 | 14.343 | 14.319 | 53.4 | 66.7 | 504.3 | 60.7 | 54.0 | -26.1 | -4.4 |
| 1633 | 73.9 | 14.343 | 14.322 | 50.5 | 63.7 | 14.342 | 14.321 | 51.4 | 72.2 | 504.1 | 66.2 | 52.8 | -23.9 | -4.6 |
| 1634 | 80.6 | 14.343 | 14.323 | 48.8 | 70.3 | 14.343 | 14.322 | 51.3 | 78.8 | 503.9 | 72.8 | 53.1 | -24.8 | -4.6 |
| 1635 | 86.1 | 14.343 | 14.324 | 48.1 | 75.8 | 14.342 | 14.323 | 48.7 | 84.3 | 503.8 | 78.3 | 52.5 | -22.4 | -4.4 |
| | | | | | | | | | | | | | | |
| 1636 | 92.2 | 14.344 | 14.325 | 48.5 | 81.9 | 14.342 | 14.325 | 44.9 | 90.4 | 504.0 | 84.4 | 50.0 | -27.4 | -4.4 |
| 1637 | 98.5 | 14.344 | 14.325 | 47.4 | 88.2 | 14.341 | 14.324 | 45.3 | 96.7 | 503.9 | 90.7 | 50.3 | -23.1 | -4.7 |
| 1638 | 104.5 | 14.342 | 14.325 | 45.5 | 94.2 | 14.342 | 14.325 | 45.3 | 102.7 | 503.8 | 96.7 | 47.8 | -19.5 | -4.8 |
| 1639 | 110.5 | 14.342 | 14.325 | 44.9 | 100.2 | 14.341 | 14.325 | 45.1 | 108.7 | 504.0 | 102.7 | 47.5 | -20.8 | -4.2 |
| 1640 | 116.6 | 14.341 | 14.325 | 44.0 | 106.4 | 14.340 | 14.325 | 43.7 | 114.9 | 503.8 | 108.9 | 46.9 | -21.3 | -4.5 |
| | | | | | | | | | | | | | | |
| 1641 | 122.1 | 14.341 | 14.326 | 43.0 | 111.9 | 14.341 | 14.326 | 42.6 | 120.4 | 503.8 | 114.4 | 45.1 | -19.5 | -4.4 |
| 1642 | 128.1 | 14.340 | 14.325 | 42.4 | 117.8 | 14.340 | 14.326 | 41.0 | 126.3 | 503.9 | 120.3 | 44.8 | -23.3 | -4.2 |
| 1643 | 134.1 | 14.341 | 14.326 | 42.2 | 123.9 | 14.340 | 14.326 | 42.0 | 132.4 | 503.9 | 126.4 | 42.6 | -23.8 | -4.1 |
| 1644 | 140.4 | 14.338 | 14.324 | 40.4 | 130.2 | 14.340 | 14.325 | 41.7 | 138.7 | 503.6 | 132.7 | 40.3 | -24.7 | -5.1 |
| 1645 | 146.0 | 14.338 | 14.325 | 39.7 | 135.8 | 14.339 | 14.325 | 41.1 | 144.3 | 503.6 | 138.3 | 41.1 | -27.6 | -5.5 |
| | | | | | | | | | | | | | | |
| 1646 | 152.1 | 14.339 | 14.324 | 41.5 | 141.8 | 14.340 | 14.325 | 43.0 | 150.3 | 503.6 | 144.3 | 43.3 | -27.4 | -5.3 |
| 1647 | 158.4 | 14.336 | 14.323 | 39.4 | 148.2 | 14.337 | 14.323 | 41.4 | 156.7 | 503.8 | 150.7 | 43.1 | -25.5 | -5.2 |
| 1648 | 164.0 | 14.332 | 14.322 | 34.4 | 153.8 | 14.338 | 14.325 | 39.8 | 162.3 | 504.0 | 156.3 | 39.0 | -20.3 | -5.6 |
| 1649 | 170.1 | 14.333 | 14.322 | 36.0 | 159.8 | 14.337 | 14.323 | 41.3 | 168.3 | 504.1 | 162.3 | 35.9 | -16.2 | -5.0 |
| 1650 | 176.6 | 14.332 | 14.321 | 36.4 | 166.4 | 14.335 | 14.324 | 36.1 | 174.9 | 504.1 | 168.9 | 35.5 | -17.8 | -4.9 |

TABLE 14.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | Wind anemometer | | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|-----------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1651 | 182.5 | 14.334 | 14.322 | 37.5 | 172.3 | 14.336 | 14.324 | 37.7 | 180.8 | 503.8 | 174.8 | 38.2 | -16.6 | -5.6 |
| 1652 | 188.4 | 14.333 | 14.322 | 37.4 | 178.2 | 14.335 | 14.323 | 37.6 | 186.7 | 503.9 | 180.7 | 38.2 | -15.6 | -4.9 |
| 1653 | 194.3 | 14.333 | 14.322 | 36.4 | 184.0 | 14.336 | 14.324 | 38.3 | 192.5 | 503.7 | 186.5 | 37.4 | -14.7 | -5.1 |
| 1654 | 199.9 | 14.333 | 14.322 | 35.8 | 189.6 | 14.336 | 14.324 | 37.7 | 198.1 | 503.6 | 192.1 | 36.0 | -14.7 | -4.8 |
| 1655 | 206.2 | 14.333 | 14.323 | 35.6 | 196.0 | 14.336 | 14.324 | 38.4 | 204.5 | 503.6 | 198.5 | 37.1 | -13.1 | -5.0 |
| 1656 | 211.8 | 14.332 | 14.322 | 34.9 | 201.6 | 14.336 | 14.323 | 38.5 | 210.1 | 503.8 | 204.1 | 36.8 | -15.9 | -5.2 |
| 1657 | 218.5 | 14.330 | 14.321 | 32.4 | 208.2 | 14.334 | 14.324 | 34.5 | 216.7 | 503.7 | 210.7 | 34.7 | -18.7 | -4.7 |
| 1658 | 224.4 | 14.331 | 14.321 | 33.0 | 214.1 | 14.335 | 14.324 | 35.8 | 222.6 | 503.8 | 216.6 | 35.3 | -18.8 | -4.6 |
| 1659 | 230.0 | 14.331 | 14.321 | 33.2 | 219.8 | 14.334 | 14.323 | 35.2 | 228.3 | 503.9 | 222.3 | 34.0 | -18.3 | -4.1 |
| 1660 | 236.4 | 14.329 | 14.321 | 31.2 | 226.1 | 14.333 | 14.324 | 32.1 | 234.6 | 503.7 | 228.6 | 32.8 | -22.7 | -3.4 |
| 1661 | 242.1 | 14.329 | 14.322 | 29.4 | 231.8 | 14.332 | 14.325 | 30.6 | 240.3 | 503.6 | 234.3 | 32.4 | -20.4 | -3.5 |
| 1662 | 248.5 | 14.328 | 14.321 | 28.8 | 238.2 | 14.330 | 14.324 | 25.6 | 246.7 | 503.5 | 240.7 | 28.9 | -15.2 | -2.2 |
| 1663 | 254.3 | 14.327 | 14.320 | 29.9 | 244.0 | 14.329 | 14.324 | 23.8 | 252.5 | 503.7 | 246.5 | 29.9 | -17.3 | -2.0 |
| 1664 | 260.5 | 14.326 | 14.319 | 28.8 | 250.2 | 14.328 | 14.324 | 20.6 | 258.7 | 503.7 | 252.7 | 28.8 | -17.0 | -1.0 |
| 1665 | 266.2 | 14.326 | 14.320 | 27.7 | 255.9 | 14.328 | 14.324 | 21.1 | 264.4 | 503.8 | 258.4 | 29.9 | -18.2 | -1.1 |
| 1666 | 272.3 | 14.325 | 14.320 | 26.6 | 262.1 | 14.328 | 14.324 | 20.8 | 270.6 | 503.8 | 264.6 | 27.5 | -18.3 | -1.4 |
| 1667 | 278.2 | 14.326 | 14.321 | 25.0 | 267.9 | 14.328 | 14.325 | 20.6 | 276.4 | 503.6 | 270.4 | 24.9 | -21.5 | -1.2 |
| 1668 | 284.1 | 14.326 | 14.321 | 24.3 | 273.8 | 14.330 | 14.327 | 19.5 | 282.3 | 503.6 | 276.3 | 25.6 | -18.9 | -1.2 |
| 1669 | 290.5 | 14.327 | 14.322 | 23.8 | 280.3 | 14.331 | 14.327 | 20.8 | 288.8 | 503.5 | 282.8 | 23.6 | -19.4 | -1.3 |
| 1670 | 292.5 | 14.328 | 14.323 | 23.0 | 282.2 | 14.330 | 14.327 | 19.0 | 290.7 | 503.6 | 284.7 | 24.5 | -23.1 | -1.0 |
| 1671 | 254.3 | 14.329 | 14.321 | 30.0 | 244.0 | 14.332 | 14.327 | 23.8 | 252.5 | 503.8 | 246.5 | 31.4 | -18.5 | -1.7 |
| 1672 | 218.3 | 14.330 | 14.321 | 34.1 | 208.1 | 14.335 | 14.323 | 37.5 | 216.6 | 503.7 | 210.6 | 36.0 | -20.0 | -4.3 |
| 1673 | 182.4 | 14.333 | 14.322 | 36.3 | 172.2 | 14.335 | 14.324 | 35.8 | 180.7 | 503.7 | 174.7 | 37.0 | -14.7 | -5.4 |
| 1674 | 146.5 | 14.338 | 14.324 | 41.6 | 156.2 | 14.339 | 14.323 | 43.1 | 144.7 | 503.7 | 138.7 | 45.0 | -26.5 | -5.1 |
| 1675 | 110.1 | 14.342 | 14.325 | 45.4 | 99.9 | 14.340 | 14.323 | 45.4 | 108.4 | 503.7 | 102.4 | 47.6 | -19.9 | -4.2 |
| 1676 | 74.1 | 14.349 | 14.326 | 52.5 | 63.9 | 14.344 | 14.321 | 52.7 | 72.4 | 504.2 | 66.4 | 56.6 | -26.0 | -4.8 |
| 1677 | 37.9 | 14.350 | 14.328 | 52.3 | 27.6 | 14.345 | 14.326 | 48.2 | 36.1 | 504.7 | 30.1 | 53.3 | -27.1 | -4.6 |
| 1678 | 32.7 | 14.351 | 14.328 | 52.3 | 22.5 | 14.344 | 14.327 | 46.0 | 31.0 | 504.9 | 25.0 | 52.6 | -30.4 | -4.4 |

TABLE 15.—DATA LISTING FOR TRAVERSE 1 AT STATION 3—VERTICAL SURVEY
 [Test section data for reading 1679; total pressure, 14.269; static pressure, 13.172 psia; total temperature, 499°R; velocity, 251.0 mph; fan speed, 287.1 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1679 | 32.2 | 14.324 | 14.318 | 26.7 | 21.7 | 14.325 | 14.318 | 29.6 | 32.0 | 499.5 | 27.0 | 31.9 | 22.6 | 2.4 |
| 1680 | 38.2 | 14.327 | 14.320 | 29.3 | 27.7 | 14.326 | 14.319 | 30.6 | 37.9 | 499.3 | 32.9 | 32.8 | 23.9 | 2.2 |
| 1681 | 44.3 | 14.328 | 14.319 | 31.2 | 33.8 | 14.327 | 14.319 | 31.8 | 44.1 | 499.3 | 39.1 | 35.4 | 21.0 | 2.8 |
| 1682 | 50.5 | 14.327 | 14.319 | 30.5 | 40.0 | 14.326 | 14.318 | 30.9 | 50.3 | 499.4 | 45.3 | 34.5 | 21.2 | 2.6 |
| 1683 | 56.9 | 14.326 | 14.318 | 30.5 | 46.4 | 14.325 | 14.318 | 30.5 | 56.6 | 499.4 | 51.6 | 33.0 | 20.6 | 2.7 |
| 1684 | 62.7 | 14.325 | 14.318 | 29.9 | 52.2 | 14.325 | 14.318 | 30.1 | 62.5 | 499.9 | 57.5 | 33.4 | 20.9 | 2.3 |
| 1685 | 68.9 | 14.325 | 14.318 | 30.2 | 58.4 | 14.325 | 14.318 | 30.3 | 68.6 | 499.9 | 63.6 | 33.0 | 20.9 | 2.8 |
| 1686 | 74.5 | 14.326 | 14.318 | 30.8 | 64.0 | 14.326 | 14.318 | 30.5 | 74.3 | 500.2 | 69.3 | 33.6 | 19.2 | 3.0 |
| 1687 | 80.9 | 14.325 | 14.317 | 29.8 | 70.4 | 14.325 | 14.317 | 29.4 | 80.6 | 500.6 | 75.6 | 32.8 | 19.7 | 2.9 |
| 1688 | 86.7 | 14.324 | 14.316 | 29.3 | 76.2 | 14.323 | 14.317 | 28.1 | 86.4 | 501.3 | 81.4 | 32.6 | 25.1 | 2.8 |
| 1689 | 92.6 | 14.324 | 14.316 | 29.4 | 82.1 | 14.321 | 14.315 | 26.5 | 92.4 | 501.5 | 87.4 | 31.2 | 23.6 | 2.9 |
| 1690 | 98.6 | 14.322 | 14.315 | 27.4 | 88.1 | 14.321 | 14.315 | 26.1 | 98.4 | 501.7 | 93.4 | 29.2 | 21.8 | 2.7 |
| 1691 | 104.4 | 14.320 | 14.315 | 25.4 | 93.9 | 14.319 | 14.314 | 25.5 | 104.1 | 501.8 | 99.1 | 27.7 | 23.0 | 2.6 |
| 1692 | 110.8 | 14.320 | 14.314 | 26.3 | 100.3 | 14.319 | 14.313 | 26.6 | 110.5 | 501.8 | 105.5 | 28.5 | 25.3 | 2.4 |
| 1693 | 116.2 | 14.319 | 14.314 | 25.0 | 105.7 | 14.319 | 14.313 | 24.8 | 116.0 | 501.2 | 111.0 | 26.9 | 24.4 | 3.0 |
| 1694 | 122.7 | 14.318 | 14.313 | 25.1 | 112.2 | 14.319 | 14.313 | 25.1 | 122.5 | 500.3 | 117.5 | 26.7 | 17.2 | 3.5 |
| 1695 | 128.5 | 14.317 | 14.313 | 22.5 | 118.0 | 14.318 | 14.314 | 22.5 | 128.3 | 499.5 | 123.3 | 25.3 | 19.7 | 3.5 |
| 1696 | 134.3 | 14.318 | 14.313 | 24.4 | 123.8 | 14.318 | 14.313 | 24.1 | 134.0 | 499.4 | 129.0 | 26.1 | 20.5 | 3.5 |
| 1697 | 140.8 | 14.316 | 14.312 | 22.4 | 130.3 | 14.316 | 14.312 | 22.5 | 140.5 | 500.1 | 135.5 | 24.5 | 17.3 | 4.3 |
| 1698 | 146.6 | 14.316 | 14.312 | 22.8 | 136.1 | 14.317 | 14.312 | 23.3 | 146.4 | 500.0 | 141.4 | 25.1 | 19.9 | 4.7 |
| 1699 | 152.5 | 14.317 | 14.313 | 22.1 | 142.0 | 14.317 | 14.313 | 22.3 | 152.2 | 499.4 | 147.2 | 23.4 | 23.9 | 4.3 |
| 1700 | 158.5 | 14.318 | 14.313 | 22.3 | 148.0 | 14.318 | 14.313 | 22.4 | 158.3 | 499.1 | 153.3 | 24.4 | 22.2 | 5.5 |
| 1701 | 164.4 | 14.319 | 14.314 | 22.8 | 153.9 | 14.318 | 14.314 | 22.9 | 164.2 | 499.0 | 159.2 | 25.0 | 21.3 | 4.7 |
| 1702 | 170.5 | 14.318 | 14.314 | 21.6 | 160.0 | 14.319 | 14.315 | 21.4 | 170.2 | 499.3 | 165.2 | 23.6 | 19.9 | 5.0 |
| 1703 | 176.9 | 14.318 | 14.315 | 21.4 | 166.4 | 14.319 | 14.315 | 21.3 | 176.6 | 499.8 | 171.6 | 23.2 | 18.2 | 4.8 |

TABLE 15.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1704 | 182.4 | 14.318 | 14.314 | 20.3 | 171.9 | 14.319 | 14.315 | 20.4 | 182.2 | 500.2 | 177.2 | 21.8 | 16.2 | 4.5 |
| 1705 | 188.7 | 14.318 | 14.314 | 20.7 | 178.2 | 14.318 | 14.314 | 21.5 | 188.4 | 500.6 | 183.4 | 23.4 | 16.0 | 4.1 |
| 1706 | 194.3 | 14.317 | 14.314 | 20.2 | 183.8 | 14.319 | 14.315 | 20.9 | 194.0 | 500.8 | 189.0 | 21.4 | 13.3 | 4.2 |
| 1707 | 200.5 | 14.319 | 14.315 | 20.1 | 190.0 | 14.319 | 14.316 | 21.1 | 200.3 | 501.1 | 195.3 | 22.1 | 11.8 | 3.3 |
| 1708 | 206.2 | 14.320 | 14.316 | 21.0 | 195.7 | 14.319 | 14.316 | 21.8 | 205.9 | 501.3 | 200.9 | 23.2 | 12.0 | 3.1 |
| 1709 | 212.3 | 14.320 | 14.316 | 21.0 | 201.8 | 14.319 | 14.315 | 21.9 | 212.0 | 501.4 | 207.0 | 22.8 | 10.8 | 2.5 |
| 1710 | 218.5 | 14.319 | 14.316 | 20.5 | 208.0 | 14.320 | 14.316 | 21.2 | 218.2 | 501.5 | 213.2 | 22.9 | 12.2 | 2.9 |
| 1711 | 224.4 | 14.320 | 14.316 | 20.5 | 213.9 | 14.319 | 14.316 | 21.1 | 224.2 | 501.4 | 219.2 | 22.8 | 14.9 | 1.6 |
| 1712 | 230.3 | 14.319 | 14.315 | 19.6 | 219.8 | 14.319 | 14.316 | 19.9 | 230.0 | 501.0 | 225.0 | 20.6 | 13.3 | 1.4 |
| 1713 | 236.7 | 14.319 | 14.315 | 20.7 | 226.2 | 14.319 | 14.315 | 21.2 | 236.4 | 500.4 | 231.4 | 21.8 | 14.5 | .8 |
| 1714 | 242.7 | 14.319 | 14.315 | 20.5 | 232.2 | 14.319 | 14.315 | 20.4 | 242.4 | 500.3 | 237.4 | 21.8 | 16.8 | 0.4 |
| 1715 | 248.6 | 14.318 | 14.315 | 19.6 | 238.1 | 14.318 | 14.315 | 19.6 | 248.4 | 500.4 | 243.4 | 20.2 | 16.8 | 0.0 |
| 1716 | 254.2 | 14.317 | 14.314 | 19.6 | 243.7 | 14.318 | 14.315 | 19.8 | 253.9 | 501.2 | 248.9 | 20.0 | 14.9 | -.3 |
| 1717 | 260.3 | 14.318 | 14.315 | 18.8 | 249.8 | 14.318 | 14.315 | 19.5 | 260.1 | 501.8 | 255.1 | 19.6 | 11.6 | -.5 |
| 1718 | 266.6 | 14.318 | 14.315 | 19.1 | 256.1 | 14.318 | 14.314 | 19.7 | 266.4 | 502.2 | 261.4 | 20.7 | 16.2 | -.2 |
| 1719 | 272.2 | 14.318 | 14.315 | 18.4 | 261.7 | 14.318 | 14.315 | 18.4 | 271.9 | 502.1 | 266.9 | 18.4 | 13.0 | -1.7 |
| 1720 | 278.2 | 14.319 | 14.316 | 18.4 | 267.7 | 14.319 | 14.316 | 18.6 | 277.9 | 502.3 | 272.9 | 18.8 | 13.7 | -2.2 |
| 1721 | 284.3 | 14.319 | 14.316 | 17.9 | 273.8 | 14.319 | 14.316 | 17.8 | 284.0 | 502.4 | 279.0 | 17.6 | 14.1 | -2.6 |
| 1722 | 290.1 | 14.319 | 14.316 | 17.5 | 279.6 | 14.319 | 14.316 | 17.4 | 289.9 | 502.6 | 284.9 | 14.6 | 13.8 | -2.3 |
| 1723 | 292.3 | 14.320 | 14.317 | 17.3 | 281.8 | 14.319 | 14.317 | 16.9 | 292.1 | 502.4 | 287.1 | 13.2 | 19.7 | -2.7 |
| 1724 | 294.8 | 14.321 | 14.318 | 18.7 | 244.3 | 14.319 | 14.316 | 19.2 | 254.6 | 502.0 | 249.6 | 17.1 | 16.3 | -0.8 |
| 1725 | 218.6 | 14.322 | 14.318 | 20.6 | 208.1 | 14.320 | 14.316 | 21.4 | 218.4 | 501.5 | 213.4 | 22.0 | 10.6 | 2.6 |
| 1726 | 182.6 | 14.321 | 14.318 | 20.6 | 172.1 | 14.319 | 14.316 | 20.8 | 182.4 | 501.0 | 177.4 | 20.8 | 16.4 | 4.9 |
| 1727 | 146.4 | 14.324 | 14.320 | 22.1 | 135.9 | 14.322 | 14.318 | 22.3 | 146.1 | 500.5 | 141.1 | 23.8 | 22.4 | 4.3 |
| 1728 | 110.7 | 14.326 | 14.321 | 25.2 | 100.2 | 14.325 | 14.320 | 25.1 | 110.5 | 499.9 | 105.5 | 27.1 | 23.5 | 2.5 |
| 1729 | 74.5 | 14.331 | 14.323 | 30.4 | 64.0 | 14.330 | 14.323 | 30.1 | 74.2 | 499.7 | 69.2 | 33.2 | 19.8 | 3.1 |
| 1730 | 38.4 | 14.331 | 14.324 | 29.0 | 27.9 | 14.332 | 14.325 | 30.5 | 38.2 | 500.1 | 33.2 | 33.0 | 23.3 | 2.3 |
| 1731 | 32.2 | 14.331 | 14.325 | 27.8 | 21.7 | 14.333 | 14.325 | 30.2 | 32.0 | 500.3 | 27.0 | 31.1 | 23.8 | 2.1 |

TABLE 16.—DATA LISTING FOR TRAVERSE 2 AT STATION 3—VERTICAL SURVEY
 [Test section data for reading 1679; total pressure, 14.269; static pressure, 13.172 psia; total temperature, 499 °R; velocity, 251.0 mph; fan speed, 287.1 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Pitch, deg | Yaw, deg |
| 1679 | 32.7 | 14.341 | 14.329 | 37.3 | 22.4 | 14.335 | 14.327 | 32.7 | 30.9 | 500.8 | 24.9 | -29.6 | -4.5 |
| 1680 | 37.9 | 14.341 | 14.330 | 35.7 | 27.6 | 14.337 | 14.326 | 35.8 | 36.1 | 500.5 | 30.1 | -28.2 | -5.0 |
| 1681 | 44.1 | 14.340 | 14.329 | 36.2 | 33.8 | 14.337 | 14.325 | 37.4 | 42.3 | 500.6 | 36.3 | -24.6 | -4.9 |
| 1682 | 50.3 | 14.339 | 14.328 | 35.7 | 40.0 | 14.336 | 14.325 | 36.4 | 48.5 | 500.4 | 42.5 | -24.8 | -5.0 |
| 1683 | 56.3 | 14.339 | 14.327 | 36.9 | 46.0 | 14.335 | 14.324 | 37.1 | 54.5 | 500.5 | 48.5 | -27.7 | -5.0 |
| 1684 | 62.1 | 14.337 | 14.326 | 36.6 | 51.9 | 14.335 | 14.323 | 37.5 | 60.4 | 500.7 | 54.4 | -26.6 | -4.9 |
| 1685 | 68.5 | 14.336 | 14.325 | 36.3 | 58.2 | 14.334 | 14.323 | 36.8 | 66.7 | 500.8 | 60.7 | -24.5 | -4.7 |
| 1686 | 74.4 | 14.335 | 14.324 | 36.2 | 64.2 | 14.335 | 14.323 | 36.9 | 72.7 | 501.0 | 66.7 | -24.0 | -4.7 |
| 1687 | 80.4 | 14.333 | 14.324 | 34.0 | 70.2 | 14.334 | 14.323 | 36.0 | 78.7 | 501.1 | 72.7 | -27.7 | -4.9 |
| 1688 | 86.6 | 14.331 | 14.322 | 33.0 | 76.3 | 14.332 | 14.322 | 34.9 | 84.8 | 501.8 | 78.8 | -22.1 | -4.8 |
| 1689 | 92.3 | 14.330 | 14.321 | 33.1 | 82.0 | 14.330 | 14.322 | 31.0 | 90.5 | 502.2 | 84.5 | -23.9 | -4.5 |
| 1690 | 98.7 | 14.329 | 14.320 | 33.2 | 88.4 | 14.330 | 14.322 | 32.2 | 96.9 | 502.3 | 90.9 | -22.5 | -4.4 |
| 1691 | 104.0 | 14.328 | 14.319 | 32.3 | 93.7 | 14.330 | 14.321 | 32.3 | 102.2 | 502.4 | 96.2 | -21.7 | -4.3 |
| 1692 | 110.6 | 14.328 | 14.320 | 31.1 | 100.3 | 14.330 | 14.321 | 32.1 | 108.8 | 502.2 | 102.8 | -20.7 | -4.9 |
| 1693 | 116.5 | 14.328 | 14.320 | 32.0 | 106.3 | 14.329 | 14.321 | 31.9 | 114.8 | 501.8 | 108.8 | -22.1 | -4.3 |
| 1694 | 122.5 | 14.329 | 14.321 | 31.3 | 112.2 | 14.329 | 14.321 | 31.4 | 120.7 | 500.9 | 114.7 | -24.2 | -4.0 |
| 1695 | 128.7 | 14.330 | 14.322 | 30.7 | 118.4 | 14.329 | 14.321 | 30.6 | 126.9 | 500.1 | 120.9 | -20.4 | -4.3 |
| 1696 | 134.5 | 14.330 | 14.322 | 30.2 | 124.2 | 14.329 | 14.321 | 31.2 | 132.7 | 500.1 | 126.7 | -22.7 | -5.0 |
| 1697 | 140.1 | 14.328 | 14.321 | 29.2 | 129.8 | 14.328 | 14.321 | 29.3 | 138.3 | 500.8 | 132.3 | -24.2 | -5.0 |
| 1698 | 146.5 | 14.327 | 14.320 | 28.9 | 136.2 | 14.327 | 14.320 | 30.0 | 144.7 | 500.6 | 138.7 | -28.7 | -5.0 |
| 1699 | 152.2 | 14.328 | 14.322 | 28.2 | 142.0 | 14.327 | 14.320 | 29.3 | 150.5 | 500.0 | 144.5 | -28.0 | -5.5 |
| 1700 | 158.2 | 14.329 | 14.322 | 29.6 | 147.9 | 14.329 | 14.321 | 31.0 | 156.4 | 499.6 | 150.4 | -26.1 | -5.4 |
| 1701 | 164.4 | 14.329 | 14.323 | 26.1 | 154.1 | 14.329 | 14.322 | 30.3 | 162.6 | 499.5 | 156.6 | -19.5 | -5.7 |
| 1702 | 170.1 | 14.328 | 14.322 | 26.5 | 159.9 | 14.329 | 14.322 | 29.8 | 168.4 | 499.9 | 162.4 | -18.6 | -5.0 |
| 1703 | 176.2 | 14.328 | 14.322 | 28.1 | 165.9 | 14.328 | 14.322 | 28.8 | 174.4 | 500.5 | 168.4 | -17.9 | -5.3 |

TABLE 16.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | Wind anemometer | | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|-----------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1704 | 182.2 | 14.327 | 14.321 | 28.1 | 172.0 | 14.328 | 14.321 | 28.4 | 180.5 | 500.7 | 174.5 | 27.4 | -17.2 | -5.2 |
| 1705 | 188.1 | 14.328 | 14.321 | 27.6 | 177.8 | 14.328 | 14.321 | 29.1 | 186.3 | 500.9 | 180.3 | 26.9 | -15.5 | -5.3 |
| 1706 | 194.0 | 14.327 | 14.321 | 28.3 | 183.8 | 14.328 | 14.320 | 29.7 | 192.3 | 501.3 | 186.3 | 28.6 | -16.7 | -5.2 |
| 1707 | 200.1 | 14.327 | 14.321 | 27.2 | 189.8 | 14.329 | 14.322 | 28.7 | 198.3 | 501.6 | 192.3 | 26.5 | -16.3 | -4.8 |
| 1708 | 206.1 | 14.328 | 14.322 | 27.1 | 195.8 | 14.329 | 14.322 | 29.8 | 204.3 | 501.8 | 198.3 | 27.3 | -16.2 | -5.3 |
| 1709 | 212.0 | 14.327 | 14.321 | 27.0 | 201.7 | 14.330 | 14.323 | 28.7 | 210.2 | 502.0 | 204.2 | 27.5 | -14.7 | -4.9 |
| 1710 | 218.2 | 14.327 | 14.322 | 25.0 | 207.9 | 14.329 | 14.323 | 27.5 | 216.4 | 501.9 | 210.4 | 26.6 | -16.9 | -5.2 |
| 1711 | 224.3 | 14.328 | 14.322 | 26.6 | 214.0 | 14.330 | 14.323 | 28.2 | 222.5 | 501.7 | 216.5 | 27.0 | -19.2 | -4.6 |
| 1712 | 230.1 | 14.328 | 14.323 | 25.4 | 219.8 | 14.329 | 14.323 | 27.1 | 228.3 | 501.4 | 222.3 | 25.5 | -20.2 | -4.4 |
| 1713 | 236.2 | 14.328 | 14.323 | 22.7 | 226.0 | 14.328 | 14.324 | 23.8 | 234.5 | 500.8 | 228.5 | 24.0 | -19.9 | -4.5 |
| 1714 | 242.7 | 14.328 | 14.323 | 23.3 | 232.5 | 14.329 | 14.324 | 24.4 | 241.0 | 500.6 | 235.0 | 24.3 | -18.9 | -3.4 |
| 1715 | 248.2 | 14.328 | 14.323 | 23.8 | 238.0 | 14.327 | 14.323 | 21.4 | 246.5 | 500.8 | 240.5 | 23.3 | -19.1 | -2.4 |
| 1716 | 254.3 | 14.327 | 14.323 | 23.1 | 244.0 | 14.325 | 14.322 | 19.0 | 252.5 | 501.7 | 246.5 | 22.6 | -17.7 | -2.1 |
| 1717 | 260.3 | 14.325 | 14.320 | 22.3 | 250.0 | 14.326 | 14.323 | 18.2 | 258.5 | 502.1 | 252.5 | 21.7 | -17.7 | -2.1 |
| 1718 | 266.3 | 14.323 | 14.320 | 21.5 | 256.1 | 14.325 | 14.322 | 16.2 | 264.6 | 502.5 | 258.6 | 22.0 | -17.9 | -1.4 |
| 1719 | 272.2 | 14.324 | 14.321 | 20.3 | 261.9 | 14.325 | 14.323 | 16.8 | 270.4 | 502.5 | 264.4 | 18.9 | -18.9 | -2.1 |
| 1720 | 278.2 | 14.325 | 14.321 | 20.2 | 267.9 | 14.325 | 14.323 | 16.4 | 276.4 | 502.6 | 270.4 | 19.5 | -17.1 | -1.6 |
| 1721 | 284.4 | 14.325 | 14.322 | 20.5 | 274.2 | 14.327 | 14.325 | 17.2 | 282.7 | 502.7 | 276.7 | 19.8 | -18.6 | -1.8 |
| 1722 | 289.9 | 14.327 | 14.324 | 19.0 | 279.7 | 14.328 | 14.326 | 15.6 | 288.2 | 502.7 | 282.2 | 17.6 | -22.6 | -1.9 |
| 1723 | 293.5 | 14.327 | 14.324 | 18.3 | 283.2 | 14.329 | 14.327 | 16.0 | 291.7 | 502.6 | 285.7 | 11.1 | -23.9 | -1.7 |
| 1724 | 254.2 | 14.329 | 14.324 | 24.0 | 243.9 | 14.329 | 14.326 | 19.3 | 252.4 | 502.4 | 246.4 | 24.3 | -19.3 | -2.0 |
| 1725 | 218.0 | 14.330 | 14.325 | 25.7 | 207.8 | 14.331 | 14.325 | 27.2 | 216.3 | 502.0 | 210.3 | 27.3 | -17.7 | -4.6 |
| 1726 | 182.2 | 14.331 | 14.324 | 27.4 | 172.0 | 14.331 | 14.325 | 28.2 | 180.5 | 501.5 | 174.5 | 28.1 | -19.2 | -5.2 |
| 1727 | 146.6 | 14.334 | 14.327 | 29.5 | 136.4 | 14.334 | 14.326 | 29.9 | 144.9 | 501.0 | 138.9 | 31.1 | -28.9 | -5.3 |
| 1728 | 110.6 | 14.337 | 14.329 | 31.4 | 100.3 | 14.336 | 14.328 | 31.6 | 108.8 | 500.6 | 102.8 | 34.0 | -21.0 | -4.5 |
| 1729 | 74.5 | 14.342 | 14.331 | 35.7 | 64.2 | 14.340 | 14.328 | 36.7 | 72.7 | 500.7 | 66.7 | 37.5 | -26.2 | -4.8 |
| 1730 | 38.4 | 14.343 | 14.333 | 35.8 | 28.2 | 14.341 | 14.330 | 35.8 | 36.7 | 501.4 | 30.7 | 36.4 | -30.4 | -5.0 |
| 1731 | 32.5 | 14.344 | 14.333 | 36.0 | 22.3 | 14.339 | 14.332 | 29.7 | 30.8 | 501.5 | 24.8 | 33.6 | -28.8 | -3.9 |

TABLE 17.—DATA LISTING FOR TRAVERSE 1 AT STATION 4—VERTICAL SURVEY
[Test section data for reading 54; total pressure, 14.412; static pressure, 12.319 psia; total temperature, 500° R; velocity, 352.0 mph; fan speed, 394.2 rpm.]

| Reading number | Position, in. | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Total pressure, in. | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 54 | 4.9 | 14.403 | 14.400 | 17.2 | 51.9 | 14.419 | 14.403 | 43.5 | 33.6 | 492.5 | 28.8 | 11.1 | 9.3 |
| 55 | 11.0 | 14.400 | 14.397 | 17.4 | 58.0 | 14.419 | 14.403 | 44.0 | 39.7 | 491.4 | 34.9 | 25.6 | 7.2 |
| 56 | 17.3 | 14.403 | 14.399 | 22.5 | 64.3 | 14.426 | 14.405 | 48.8 | 46.0 | 490.5 | 41.1 | 34.6 | 19.8 |
| 57 | 22.7 | 14.403 | 14.398 | 24.2 | 69.7 | 14.426 | 14.407 | 46.3 | 51.5 | 490.5 | 46.6 | 15.1 | 24.6 |
| 58 | 28.9 | 14.406 | 14.399 | 28.5 | 75.9 | 14.413 | 14.405 | 30.9 | 57.6 | 489.1 | 52.8 | 43.9 | 3.6 |
| 59 | 35.1 | 14.409 | 14.400 | 32.7 | 82.1 | 14.419 | 14.411 | 30.8 | 63.8 | 487.1 | 59.0 | 37.7 | 10.4 |
| 60 | 41.1 | 14.412 | 14.399 | 39.3 | 88.1 | 14.429 | 14.408 | 48.7 | 69.9 | 486.7 | 65.0 | 46.0 | 7.0 |
| 61 | 46.8 | 14.418 | 14.404 | 41.2 | 93.8 | 14.422 | 14.407 | 42.1 | 75.6 | 489.1 | 70.7 | 44.2 | 8.1 |
| 62 | 53.0 | 14.422 | 14.405 | 43.6 | 100.0 | 14.422 | 14.409 | 40.0 | 81.7 | 490.0 | 76.9 | 30.0 | -1.0 |
| 63 | 58.9 | 14.425 | 14.408 | 45.0 | 105.9 | 14.419 | 14.404 | 42.9 | 87.6 | 494.9 | 82.7 | 28.8 | -5.1 |
| 64 | 64.9 | 14.428 | 14.408 | 48.7 | 111.9 | 14.422 | 14.406 | 44.2 | 93.7 | 497.8 | 88.8 | 44.6 | -1.4 |
| 65 | 71.1 | 14.428 | 14.411 | 45.2 | 118.1 | 14.422 | 14.407 | 42.3 | 99.9 | 497.7 | 95.0 | 37.8 | -3.3 |
| 66 | 77.1 | 14.418 | 14.411 | 30.0 | 124.1 | 14.419 | 14.408 | 36.6 | 105.8 | 498.5 | 101.0 | 35.1 | -1.0 |
| 67 | 83.2 | 14.425 | 14.415 | 34.0 | 130.2 | 14.422 | 14.412 | 35.0 | 111.9 | 498.7 | 107.0 | 35.1 | -5.1 |
| 68 | 94.9 | 14.425 | 14.410 | 42.5 | 141.9 | 14.419 | 14.410 | 32.5 | 123.7 | 497.6 | 118.8 | 33.6 | -2.2 |
| 69 | 107.0 | 14.425 | 14.409 | 43.4 | 154.0 | 14.413 | 14.405 | 30.5 | 135.7 | 495.7 | 130.8 | 26.1 | -1.5 |
| 70 | 118.9 | 14.422 | 14.407 | 41.6 | 165.9 | 14.416 | 14.411 | 25.4 | 147.7 | 494.6 | 142.8 | 23.5 | 4.2 |
| 71 | 131.3 | 14.415 | 14.405 | 34.2 | 178.3 | 14.413 | 14.408 | 25.0 | 160.0 | 493.9 | 155.1 | 23.7 | 3.5 |
| 72 | 143.2 | 14.415 | 14.407 | 31.6 | 190.2 | 14.419 | 14.411 | 31.5 | 172.0 | 492.9 | 167.1 | 17.5 | -6.2 |
| 73 | 155.0 | 14.415 | 14.408 | 29.0 | 202.0 | 14.429 | 14.412 | 44.3 | 183.7 | 492.9 | 178.8 | 21.3 | 8.8 |
| 74 | 167.1 | 14.412 | 14.407 | 24.0 | 214.1 | 14.426 | 14.410 | 43.5 | 195.9 | 493.0 | 191.0 | 22.5 | -0.9 |
| 75 | 178.8 | 14.415 | 14.409 | 26.7 | 225.8 | 14.422 | 14.416 | 26.9 | 207.6 | 499.8 | 202.7 | 39.9 | -3.3 |
| 76 | 185.0 | 14.413 | 14.407 | 28.3 | 232.0 | 14.416 | 14.414 | 16.4 | 213.7 | 500.8 | 208.9 | 40.9 | -9.2 |
| 77 | 191.0 | 14.417 | 14.408 | 33.1 | 238.0 | 14.429 | 14.414 | 43.0 | 219.8 | 497.6 | 214.9 | 39.8 | -2.2 |
| 78 | 196.7 | 14.422 | 14.409 | 39.8 | 243.7 | 14.429 | 14.413 | 43.2 | 225.4 | 497.9 | 220.5 | 37.2 | 1.3 |

TABLE 17.—Concluded.

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | | Wind anemometer | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 79 | 202.8 | 14.427 | 14.410 | 44.7 | 249.8 | 14.428 | 14.412 | 43.0 | 231.6 | 500.0 | 226.7 | 17.7 | 4.8 | -8.6 |
| 80 | 208.5 | 14.426 | 14.410 | 43.4 | 255.5 | 14.426 | 14.412 | 41.0 | 237.3 | 501.0 | 232.4 | 15.3 | 3.0 | -2.8 |
| 81 | 214.9 | 14.427 | 14.411 | 43.5 | 261.9 | 14.426 | 14.412 | 40.0 | 243.6 | 501.2 | 238.8 | 38.9 | 2.2 | 1.5 |
| 82 | 221.2 | 14.419 | 14.412 | 30.2 | 268.2 | 14.423 | 14.410 | 38.8 | 249.9 | 501.4 | 245.0 | 38.6 | 1.3 | -7 |
| 83 | 226.7 | 14.416 | 14.411 | 23.8 | 273.7 | 14.422 | 14.410 | 37.6 | 255.4 | 501.5 | 250.6 | 38.2 | 1.3 | .2 |
| 84 | 233.4 | 14.418 | 14.412 | 26.0 | 280.4 | 14.421 | 14.410 | 35.8 | 262.2 | 501.4 | 257.3 | 35.0 | 2.3 | -0.5 |
| 85 | 239.1 | 14.427 | 14.412 | 43.0 | 286.1 | 14.419 | 14.410 | 32.5 | 267.9 | 501.3 | 263.0 | 33.2 | 4.6 | .2 |
| 86 | 244.9 | 14.426 | 14.411 | 42.0 | 291.9 | 14.417 | 14.410 | 29.3 | 273.6 | 501.3 | 268.7 | 29.3 | 5.2 | -7 |
| 87 | 251.0 | 14.423 | 14.409 | 41.2 | 298.0 | 14.416 | 14.410 | 25.0 | 279.8 | 501.2 | 274.9 | 25.6 | 5.1 | -1.0 |
| 88 | 256.9 | 14.422 | 14.408 | 40.1 | 303.9 | 14.414 | 14.410 | 21.5 | 285.6 | 501.5 | 280.7 | 25.0 | 6.3 | -1.7 |
| 89 | 261.2 | 14.421 | 14.408 | 39.4 | 308.2 | 14.413 | 14.410 | 18.9 | 289.9 | 501.5 | 285.1 | 23.4 | 6.8 | -3.7 |
| 90 | 242.7 | 14.426 | 14.411 | 42.3 | 289.7 | 14.419 | 14.411 | 30.6 | 271.5 | 501.2 | 266.6 | 31.1 | 5.5 | .2 |
| 91 | 224.6 | 14.417 | 14.411 | 27.3 | 271.6 | 14.424 | 14.412 | 38.2 | 253.4 | 501.1 | 248.5 | 38.6 | 1.0 | -7 |
| 92 | 207.2 | 14.427 | 14.410 | 43.9 | 254.2 | 14.427 | 14.413 | 41.1 | 235.9 | 501.3 | 231.0 | 13.0 | 4.4 | -8.0 |
| 93 | 189.0 | 14.416 | 14.408 | 30.8 | 236.0 | 14.428 | 14.417 | 37.7 | 217.7 | 501.4 | 212.8 | 40.3 | 8.8 | -4 |
| 94 | 171.3 | 14.413 | 14.408 | 24.4 | 218.3 | 14.430 | 14.416 | 41.8 | 200.0 | 494.6 | 195.1 | 30.8 | 9.1 | -0.2 |
| 95 | 153.1 | 14.416 | 14.408 | 29.8 | 200.1 | 14.429 | 14.413 | 43.3 | 181.9 | 492.3 | 177.0 | 17.6 | 11.3 | -4.9 |
| 96 | 135.0 | 14.418 | 14.409 | 33.3 | 182.0 | 14.419 | 14.413 | 26.7 | 163.8 | 493.5 | 158.9 | 22.0 | 10.1 | -1.8 |
| 97 | 117.1 | 14.426 | 14.411 | 42.7 | 164.1 | 14.419 | 14.413 | 25.7 | 145.8 | 494.6 | 141.0 | 23.3 | 3.4 | 6.4 |
| 98 | 99.4 | 14.424 | 14.411 | 39.2 | 146.4 | 14.422 | 14.414 | 30.8 | 128.1 | 496.2 | 123.2 | 28.3 | -2.8 | -5 |
| 99 | 81.1 | 14.420 | 14.417 | 20.1 | 128.1 | 14.426 | 14.415 | 36.0 | 109.9 | 498.8 | 105.0 | 37.5 | -2.3 | -2.4 |
| 100 | 63.0 | 14.432 | 14.413 | 46.6 | 110.0 | 14.432 | 14.416 | 44.0 | 91.7 | 497.4 | 86.9 | 44.6 | 1.7 | 1.0 |
| 101 | 45.2 | 14.426 | 14.412 | 40.9 | 92.2 | 14.435 | 14.417 | 44.7 | 74.0 | 488.4 | 69.1 | 44.7 | 7.3 | 0.0 |
| 102 | 27.1 | 14.418 | 14.411 | 28.3 | 74.1 | 14.431 | 14.420 | 34.8 | 55.9 | 489.5 | 51.0 | 38.1 | 8.7 | 4 |
| 103 | 9.3 | 14.413 | 14.410 | 18.6 | 56.3 | 14.434 | 14.416 | 45.3 | 38.1 | 490.3 | 33.2 | 22.1 | 5.7 | -1.5 |
| 104 | 5.0 | 14.415 | 14.412 | 17.2 | 52.0 | 14.432 | 14.415 | 44.1 | 33.7 | 490.5 | 28.8 | 16.2 | 6.6 | 0.7 |

TABLE 18.—DATA LISTING FOR TRAVERSE 2 AT STATION 4—VERTICAL SURVEY
 [Test section data for reading 54; total pressure, 14.412; static pressure, 12.319 psia; total temperature, 500 °R; velocity, 352.0 mph; fan speed, 394.2 rpm.]

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|-----------------|----------|--|--|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg | | |
| 54 | 5.0 | 14.406 | 14.404 | 16.7 | 51.1 | 14.428 | 14.410 | 45.9 | 31.6 | 496.0 | 28.1 | 23.4 | 6.9 | 0 | | |
| 55 | 11.5 | 14.403 | 14.399 | 21.5 | 57.6 | 14.428 | 14.410 | 45.6 | 38.1 | 495.1 | 34.6 | 33.1 | 2.8 | -2.4 | | |
| 56 | 17.5 | 14.406 | 14.400 | 26.6 | 63.6 | 14.425 | 14.406 | 47.7 | 44.1 | 494.8 | 40.6 | 35.3 | 5.5 | -4.3 | | |
| 57 | 23.1 | 14.406 | 14.399 | 30.1 | 69.2 | 14.425 | 14.406 | 46.7 | 49.7 | 494.9 | 46.2 | 35.6 | 5.4 | -3.7 | | |
| 58 | 28.7 | 14.406 | 14.397 | 32.8 | 74.8 | 14.422 | 14.408 | 40.7 | 55.3 | 494.6 | 51.8 | 45.1 | 6.0 | -1.5 | | |
| 59 | 34.9 | 14.413 | 14.399 | 39.4 | 81.1 | 14.422 | 14.407 | 41.9 | 61.6 | 494.4 | 58.1 | 39.6 | 6.9 | -4.3 | | |
| 60 | 41.1 | 14.413 | 14.397 | 42.3 | 87.2 | 14.422 | 14.404 | 45.7 | 67.7 | 494.3 | 64.2 | 45.9 | 4.9 | -5.2 | | |
| 61 | 47.2 | 14.416 | 14.399 | 43.9 | 93.3 | 14.422 | 14.405 | 44.3 | 73.8 | 492.7 | 70.3 | 44.0 | 6.3 | -6.1 | | |
| 62 | 52.8 | 14.419 | 14.401 | 46.0 | 98.9 | 14.422 | 14.406 | 43.4 | 79.4 | 492.8 | 75.9 | 39.0 | 5.0 | -5.8 | | |
| 63 | 58.7 | 14.419 | 14.401 | 46.5 | 104.8 | 14.419 | 14.403 | 42.9 | 85.3 | 496.5 | 81.8 | 46.1 | -3.5 | -3.3 | | |
| 64 | 64.8 | 14.425 | 14.405 | 48.8 | 110.9 | 14.419 | 14.403 | 43.3 | 91.4 | 496.7 | 87.9 | 39.8 | -3.3 | -0.9 | | |
| 65 | 70.9 | 14.425 | 14.406 | 47.2 | 117.0 | 14.419 | 14.403 | 42.6 | 97.5 | 496.0 | 94.0 | 39.0 | -4.9 | -5.1 | | |
| 66 | 76.5 | 14.419 | 14.405 | 41.1 | 122.6 | 14.415 | 14.403 | 38.2 | 103.1 | 496.0 | 99.6 | 38.7 | -3.7 | -5.8 | | |
| 67 | 82.8 | 14.425 | 14.411 | 41.4 | 129.0 | 14.412 | 14.402 | 35.6 | 109.5 | 495.8 | 106.0 | 39.5 | -4.6 | -8.3 | | |
| 68 | 95.0 | 14.422 | 14.405 | 44.5 | 141.1 | 14.406 | 14.401 | 25.3 | 121.6 | 494.7 | 118.1 | 35.4 | -1.3 | -8.0 | | |
| 69 | 106.6 | 14.419 | 14.403 | 43.5 | 152.7 | 14.406 | 14.402 | 22.4 | 133.2 | 493.9 | 129.7 | 23.5 | -1.1 | -9.3 | | |
| 70 | 119.6 | 14.416 | 14.401 | 41.2 | 165.8 | 14.409 | 14.402 | 29.2 | 146.3 | 492.5 | 142.8 | 10.1 | -7 | -10.8 | | |
| 71 | 130.9 | 14.413 | 14.403 | 34.1 | 177.1 | 14.412 | 14.402 | 34.8 | 157.6 | 492.0 | 154.1 | 11.6 | -2 | -4.5 | | |
| 72 | 143.2 | 14.403 | 14.399 | 23.3 | 189.3 | 14.415 | 14.403 | 37.8 | 169.8 | 492.5 | 166.3 | 21.0 | 2.1 | -8.7 | | |
| 73 | 155.0 | 14.406 | 14.402 | 23.3 | 201.1 | 14.415 | 14.403 | 38.5 | 181.6 | 493.7 | 178.1 | 26.3 | 3.1 | -7.4 | | |
| 74 | 166.2 | 14.410 | 14.402 | 29.2 | 212.3 | 14.412 | 14.399 | 39.6 | 192.8 | 495.9 | 189.3 | 32.5 | 4.9 | -5.2 | | |
| 75 | 178.3 | 14.413 | 14.402 | 34.9 | 224.5 | 14.422 | 14.408 | 40.9 | 205.0 | 498.5 | 201.5 | 35.2 | 5.7 | -4.6 | | |
| 76 | 185.9 | 14.414 | 14.403 | 37.3 | 232.0 | 14.408 | 14.406 | 12.3 | 212.5 | 499.3 | 209.0 | 35.2 | 7.9 | -4.4 | | |
| 77 | 190.9 | 14.415 | 14.402 | 38.3 | 237.0 | 14.422 | 14.407 | 41.3 | 217.5 | 498.7 | 214.0 | 37.7 | 8.1 | -4.2 | | |
| 78 | 197.2 | 14.415 | 14.403 | 38.5 | 243.3 | 14.419 | 14.405 | 41.0 | 223.8 | 498.3 | 220.3 | 39.2 | 7.4 | -3.8 | | |

TABLE 18.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 79 | 203.2 | 14.416 | 14.403 | 39.3 | 249.3 | 14.415 | 14.403 | 36.6 | 229.8 | 499.5 | 226.3 | 33.8 | 7.8 | -6.0 |
| 80 | 208.4 | 14.417 | 14.404 | 39.5 | 254.5 | 14.413 | 14.403 | 36.1 | 235.0 | 501.8 | 231.5 | 20.8 | 6.7 | -11.8 |
| 81 | 215.2 | 14.418 | 14.404 | 41.1 | 261.3 | 14.411 | 14.401 | 34.3 | 241.8 | 502.0 | 238.3 | 38.3 | .1 | -4.4 |
| 82 | 221.8 | 14.419 | 14.404 | 42.2 | 267.9 | 14.407 | 14.399 | 30.9 | 248.4 | 502.2 | 244.9 | 30.9 | -1.9 | -6.2 |
| 83 | 226.5 | 14.419 | 14.405 | 40.6 | 272.6 | 14.406 | 14.400 | 27.8 | 253.1 | 502.3 | 249.6 | 29.3 | -2.8 | -6.2 |
| 84 | 233.1 | 14.411 | 14.409 | 16.7 | 279.2 | 14.405 | 14.400 | 23.6 | 259.7 | 502.4 | 256.2 | 27.4 | -3.3 | -5.6 |
| 85 | 239.0 | 14.419 | 14.404 | 42.9 | 285.2 | 14.403 | 14.400 | 18.9 | 265.7 | 502.3 | 262.2 | 25.8 | -2.8 | -5.4 |
| 86 | 245.5 | 14.417 | 14.404 | 39.6 | 291.6 | 14.402 | 14.399 | 16.2 | 272.1 | 502.3 | 268.6 | 18.6 | -2.7 | -3.0 |
| 87 | 251.0 | 14.415 | 14.403 | 36.9 | 297.1 | 14.401 | 14.400 | 12.4 | 277.6 | 502.2 | 274.1 | 14.5 | -1.5 | -3.7 |
| 88 | 256.4 | 14.413 | 14.402 | 35.9 | 302.5 | 14.401 | 14.400 | 10.0 | 283.0 | 502.5 | 279.5 | 10.1 | -1.5 | -5.5 |
| 89 | 260.2 | 14.411 | 14.401 | 35.0 | 306.3 | 14.400 | 14.399 | 8.4 | 286.8 | 502.5 | 283.3 | 5.8 | -2.3 | -5.6 |
| 90 | 242.6 | 14.419 | 14.404 | 42.4 | 288.7 | 14.402 | 14.400 | 18.5 | 269.2 | 502.2 | 265.7 | 22.2 | -2.3 | -5.5 |
| 91 | 224.5 | 14.419 | 14.405 | 40.7 | 270.6 | 14.407 | 14.400 | 28.8 | 251.1 | 501.9 | 247.6 | 28.9 | -2.8 | -6.8 |
| 92 | 207.7 | 14.417 | 14.404 | 39.6 | 253.8 | 14.413 | 14.402 | 36.0 | 234.3 | 502.1 | 230.8 | 26.4 | 6.8 | -11.4 |
| 93 | 189.2 | 14.415 | 14.402 | 38.3 | 235.3 | 14.418 | 14.406 | 36.6 | 215.8 | 502.0 | 212.3 | 36.2 | 8.2 | -4.3 |
| 94 | 171.1 | 14.410 | 14.401 | 32.0 | 217.3 | 14.418 | 14.404 | 40.8 | 197.8 | 497.3 | 194.3 | 33.0 | 5.8 | -5.7 |
| 95 | 152.7 | 14.405 | 14.401 | 22.3 | 198.8 | 14.415 | 14.403 | 38.5 | 179.3 | 493.1 | 175.8 | 27.4 | 2.5 | -5.4 |
| 96 | 135.5 | 14.410 | 14.402 | 29.4 | 181.6 | 14.414 | 14.403 | 35.9 | 162.1 | 491.9 | 158.6 | 15.3 | -1.3 | -8.1 |
| 97 | 117.4 | 14.419 | 14.404 | 42.0 | 163.6 | 14.408 | 14.401 | 27.2 | 144.1 | 492.1 | 140.6 | 14.6 | -4 | -7.9 |
| 98 | 99.2 | 14.421 | 14.404 | 44.3 | 145.3 | 14.406 | 14.402 | 22.1 | 125.8 | 494.1 | 122.3 | 30.1 | -1.6 | -6.3 |
| 99 | 81.1 | 14.413 | 14.411 | 15.7 | 127.2 | 14.414 | 14.403 | 36.2 | 107.7 | 496.3 | 104.2 | 39.2 | -4.1 | -5.2 |
| 100 | 63.2 | 14.425 | 14.406 | 47.8 | 109.4 | 14.420 | 14.404 | 43.7 | 89.9 | 496.9 | 86.4 | 41.0 | -3.6 | -4 |
| 101 | 45.0 | 14.420 | 14.404 | 43.7 | 91.1 | 14.425 | 14.408 | 44.3 | 71.6 | 491.7 | 68.1 | 44.5 | 5.9 | -4.8 |
| 102 | 27.6 | 14.413 | 14.404 | 31.9 | 73.7 | 14.427 | 14.411 | 43.2 | 54.2 | 493.5 | 50.7 | 41.6 | 5.9 | -3.5 |
| 103 | 9.4 | 14.407 | 14.403 | 20.6 | 55.5 | 14.424 | 14.406 | 46.2 | 36.0 | 493.5 | 32.5 | 23.0 | 6.0 | -4.3 |
| 104 | 4.9 | 14.406 | 14.403 | 18.8 | 51.1 | 14.423 | 14.405 | 45.8 | 31.6 | 493.1 | 28.1 | 21.8 | 2.5 | -3.3 |

TABLE 19.—DATA LISTING FOR TRAVERSE 1 AT STATION 4—VERTICAL SURVEY
[Test section data for reading 105; total pressure, 14.427; static pressure, 13.320 psia; total temperature, 498 °R; velocity, 250.6 mph; fan speed 290.6 rpm.]

| Reading number | Probe one | | | | | Probe two | | | | | Thermocouple | | | Wind anemometer | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|-----------------|--|--|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg | | |
| 105 | 4.9 | 14.422 | 14.421 | 12.1 | 51.9 | 14.430 | 14.420 | 33.4 | 33.6 | 489.5 | 28.8 | 10.4 | 5.7 | 1.8 | | |
| 106 | 11.1 | 14.421 | 14.420 | 14.1 | 58.1 | 14.430 | 14.420 | 35.2 | 39.8 | 493.0 | 34.9 | 15.8 | 5.6 | -2.0 | | |
| 107 | 17.0 | 14.422 | 14.420 | 16.3 | 64.0 | 14.433 | 14.422 | 36.7 | 45.8 | 494.9 | 40.9 | 20.3 | 7.9 | -1.0 | | |
| 108 | 22.9 | 14.425 | 14.421 | 19.7 | 69.9 | 14.433 | 14.423 | 34.0 | 51.6 | 495.9 | 46.8 | 22.9 | 9.7 | 1.2 | | |
| 109 | 29.2 | 14.427 | 14.422 | 22.9 | 76.2 | 14.427 | 14.423 | 22.7 | 58.0 | 492.4 | 53.1 | 28.8 | 7.7 | -9 | | |
| 110 | 35.2 | 14.427 | 14.421 | 26.4 | 82.2 | 14.427 | 14.423 | 21.6 | 63.9 | 496.4 | 59.0 | 29.6 | 9.3 | -1.2 | | |
| 111 | 40.8 | 14.428 | 14.421 | 29.2 | 87.8 | 14.434 | 14.423 | 36.8 | 69.5 | 490.7 | 64.7 | 31.3 | 8.1 | -.5 | | |
| 112 | 47.0 | 14.430 | 14.422 | 31.5 | 94.0 | 14.430 | 14.421 | 32.1 | 75.8 | 485.4 | 70.9 | 30.9 | 6.9 | 0.1 | | |
| 113 | 53.1 | 14.429 | 14.420 | 32.8 | 100.1 | 14.428 | 14.420 | 30.2 | 81.8 | 486.3 | 77.0 | 19.5 | 6.7 | -3.8 | | |
| 114 | 59.0 | 14.431 | 14.421 | 33.9 | 106.0 | 14.431 | 14.422 | 32.2 | 87.7 | 494.8 | 82.9 | 15.8 | 4.0 | -1.2 | | |
| 115 | 65.0 | 14.433 | 14.421 | 36.6 | 112.0 | 14.430 | 14.421 | 32.5 | 93.7 | 499.1 | 88.8 | 31.5 | 1.7 | 1.5 | | |
| 116 | 71.2 | 14.431 | 14.422 | 32.6 | 118.2 | 14.429 | 14.421 | 31.2 | 100.0 | 499.2 | 95.1 | 27.0 | 0.1 | -1.0 | | |
| 117 | 77.2 | 14.427 | 14.423 | 22.1 | 124.2 | 14.427 | 14.420 | 28.1 | 105.9 | 500.2 | 101.1 | 25.6 | -1.3 | -2.0 | | |
| 118 | 83.1 | 14.428 | 14.424 | 23.4 | 130.1 | 14.426 | 14.420 | 25.5 | 111.9 | 497.6 | 107.0 | 26.0 | -2.3 | -2.1 | | |
| 119 | 94.9 | 14.429 | 14.420 | 32.1 | 141.9 | 14.426 | 14.421 | 23.6 | 123.6 | 498.8 | 118.8 | 21.2 | -2.1 | -9 | | |
| 120 | 106.9 | 14.430 | 14.421 | 32.3 | 153.9 | 14.426 | 14.421 | 22.4 | 135.7 | 497.9 | 130.8 | 16.1 | -2.6 | 3.9 | | |
| 121 | 119.0 | 14.428 | 14.420 | 31.3 | 166.0 | 14.424 | 14.421 | 18.6 | 147.7 | 498.1 | 142.9 | 15.5 | 3.7 | 7.4 | | |
| 122 | 130.8 | 14.426 | 14.420 | 25.7 | 177.8 | 14.423 | 14.420 | 19.3 | 159.6 | 496.6 | 154.7 | 13.5 | 10.2 | 1.4 | | |
| 123 | 143.0 | 14.424 | 14.420 | 23.2 | 190.0 | 14.424 | 14.420 | 24.0 | 171.7 | 497.8 | 166.9 | 10.9 | 10.6 | -3.5 | | |
| 124 | 154.7 | 14.424 | 14.420 | 21.8 | 201.7 | 14.430 | 14.421 | 33.6 | 183.5 | 497.3 | 178.6 | 9.9 | 11.8 | -3.6 | | |
| 125 | 166.8 | 14.422 | 14.419 | 17.9 | 213.8 | 14.430 | 14.420 | 33.8 | 195.5 | 499.2 | 190.6 | 15.8 | 10.5 | -0.6 | | |
| 126 | 179.4 | 14.423 | 14.419 | 19.9 | 226.4 | 14.425 | 14.421 | 20.0 | 208.1 | 500.1 | 203.2 | 28.2 | 10.4 | .3 | | |
| 127 | 184.9 | 14.422 | 14.418 | 21.3 | 231.9 | 14.423 | 14.422 | 11.6 | 213.7 | 499.5 | 208.8 | 29.5 | 9.7 | -.7 | | |
| 128 | 175.5 | 14.421 | 14.418 | 19.3 | 222.5 | 14.425 | 14.421 | 23.1 | 204.2 | 499.7 | 199.3 | 25.7 | 9.2 | .8 | | |
| 129 | 196.7 | 14.427 | 14.419 | 30.7 | 243.7 | 14.427 | 14.418 | 32.5 | 225.5 | 500.9 | 220.6 | 26.4 | 5.9 | 1.5 | | |

TABLE 19.—Concluded.

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|-----------------|----------|--|--|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg | | |
| 130 | 202.9 | 14.429 | 14.419 | 33.7 | 249.9 | 14.427 | 14.419 | 32.3 | 231.7 | 501.2 | 226.8 | 11.0 | 5.7 | -9.4 | | |
| 131 | 208.9 | 14.428 | 14.419 | 32.9 | 255.9 | 14.427 | 14.419 | 31.3 | 237.6 | 500.9 | 232.7 | 9.7 | 3.3 | -1.8 | | |
| 132 | 215.1 | 14.429 | 14.420 | 33.2 | 262.1 | 14.427 | 14.419 | 30.7 | 243.8 | 501.3 | 238.9 | 27.6 | 2.0 | 1.6 | | |
| 133 | 221.1 | 14.427 | 14.422 | 24.0 | 268.1 | 14.426 | 14.419 | 29.6 | 249.8 | 500.4 | 244.9 | 27.7 | 1.1 | -1.3 | | |
| 134 | 227.2 | 14.422 | 14.420 | 16.3 | 274.2 | 14.425 | 14.418 | 28.2 | 256.0 | 501.9 | 251.1 | 26.3 | 1.5 | -8 | | |
| 135 | 232.9 | 14.424 | 14.421 | 17.2 | 279.9 | 14.424 | 14.418 | 25.8 | 261.7 | 500.4 | 256.8 | 25.2 | 2.8 | -0.8 | | |
| 136 | 239.1 | 14.429 | 14.420 | 32.9 | 286.1 | 14.423 | 14.418 | 24.1 | 267.8 | 501.1 | 263.0 | 21.4 | 2.5 | -3.0 | | |
| 137 | 245.0 | 14.427 | 14.419 | 31.9 | 292.0 | 14.422 | 14.418 | 21.2 | 273.8 | 500.6 | 268.9 | 20.9 | 4.3 | -1.0 | | |
| 138 | 251.3 | 14.427 | 14.419 | 31.5 | 298.3 | 14.422 | 14.419 | 18.3 | 280.0 | 500.5 | 275.2 | 17.6 | 4.4 | -1.3 | | |
| 139 | 257.2 | 14.426 | 14.418 | 30.8 | 304.2 | 14.420 | 14.418 | 15.6 | 285.9 | 500.6 | 281.0 | 17.3 | 6.7 | -1.7 | | |
| 140 | 261.4 | 14.426 | 14.418 | 30.4 | 308.4 | 14.420 | 14.418 | 14.5 | 290.1 | 501.0 | 285.2 | 14.5 | 7.8 | -0.5 | | |
| 141 | 243.3 | 14.427 | 14.419 | 31.5 | 290.3 | 14.423 | 14.419 | 21.9 | 272.1 | 499.8 | 267.2 | 18.6 | 2.7 | -1.0 | | |
| 142 | 224.8 | 14.424 | 14.421 | 20.6 | 271.8 | 14.427 | 14.420 | 28.9 | 253.5 | 500.4 | 248.7 | 27.5 | 1.4 | -9 | | |
| 143 | 207.4 | 14.428 | 14.418 | 33.6 | 254.4 | 14.427 | 14.418 | 31.6 | 236.2 | 499.8 | 231.3 | 5.7 | 3.9 | -7.1 | | |
| 144 | 189.0 | 14.422 | 14.418 | 23.8 | 236.0 | 14.427 | 14.420 | 29.3 | 217.7 | 500.8 | 212.9 | 28.9 | 8.9 | -3 | | |
| 145 | 171.2 | 14.421 | 14.418 | 18.2 | 218.2 | 14.428 | 14.419 | 32.3 | 199.9 | 498.6 | 195.0 | 19.9 | 9.4 | 0.1 | | |
| 146 | 153.2 | 14.422 | 14.418 | 22.1 | 200.2 | 14.427 | 14.418 | 33.2 | 182.0 | 498.3 | 177.1 | 9.6 | 11.2 | -4.9 | | |
| 147 | 134.9 | 14.423 | 14.418 | 24.5 | 181.9 | 14.422 | 14.419 | 20.3 | 163.7 | 498.1 | 158.8 | 13.2 | 10.8 | -5 | | |
| 148 | 117.2 | 14.427 | 14.418 | 31.8 | 164.2 | 14.420 | 14.417 | 19.2 | 145.9 | 499.0 | 141.1 | 15.5 | 2.0 | 7.0 | | |
| 149 | 99.2 | 14.426 | 14.418 | 30.1 | 146.2 | 14.423 | 14.419 | 23.4 | 128.0 | 495.5 | 123.1 | 19.3 | -3.0 | -3 | | |
| 150 | 81.0 | 14.422 | 14.420 | 13.3 | 128.0 | 14.424 | 14.418 | 26.3 | 109.8 | 497.1 | 104.9 | 25.7 | -2.3 | -2.1 | | |
| 151 | 63.1 | 14.428 | 14.417 | 35.6 | 110.1 | 14.427 | 14.418 | 33.2 | 91.9 | 498.5 | 87.0 | 30.4 | 1.9 | .8 | | |
| 152 | 45.3 | 14.427 | 14.419 | 31.1 | 92.3 | 14.429 | 14.419 | 34.3 | 74.0 | 492.1 | 69.2 | 32.0 | 8.7 | .3 | | |
| 153 | 27.1 | 14.421 | 14.417 | 20.9 | 74.1 | 14.427 | 14.422 | 24.6 | 55.9 | 490.4 | 51.0 | 27.7 | 7.4 | .2 | | |
| 154 | 9.2 | 14.419 | 14.417 | 13.4 | 56.2 | 14.430 | 14.420 | 34.2 | 37.9 | 491.7 | 33.0 | 12.3 | 5.7 | -.3 | | |
| 155 | 4.9 | 14.420 | 14.419 | 11.1 | 51.9 | 14.428 | 14.419 | 33.8 | 33.7 | 490.8 | 28.8 | 10.6 | 6.5 | 1.5 | | |

TABLE 20.—DATA LISTING FOR TRAVERSE 2 AT STATION 4—VERTICAL SURVEY
 [Test section data for reading 105; total pressure, 14.427; static pressure, 13.320 psia; total temperature, 498 °R; velocity, 250.6 mph; fan speed, 290.6 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 105 | 4.9 | 14.412 | 14.411 | 12.8 | 51.0 | 14.422 | 14.413 | 33.8 | 31.5 | 489.7 | 28.0 | 12.3 | 3.2 | -3.2 |
| 106 | 11.4 | 14.412 | 14.410 | 14.3 | 57.5 | 14.420 | 14.410 | 33.4 | 38.0 | 493.5 | 34.5 | 17.8 | 4.2 | -3.8 |
| 107 | 17.0 | 14.412 | 14.410 | 17.7 | 63.1 | 14.422 | 14.412 | 35.1 | 43.6 | 496.9 | 40.1 | 21.2 | 6.7 | -3.5 |
| 108 | 23.2 | 14.414 | 14.410 | 21.6 | 69.4 | 14.422 | 14.413 | 33.3 | 49.9 | 497.2 | 46.4 | 25.0 | 6.0 | -4.3 |
| 109 | 29.0 | 14.417 | 14.412 | 24.7 | 75.2 | 14.421 | 14.416 | 24.7 | 55.7 | 492.0 | 52.2 | 28.8 | 6.0 | -2.7 |
| | | | | | | | | | | | | | | |
| 110 | 35.6 | 14.418 | 14.411 | 28.6 | 81.7 | 14.425 | 14.416 | 32.7 | 62.2 | 495.3 | 58.7 | 27.9 | 5.7 | -3.6 |
| 111 | 41.0 | 14.418 | 14.410 | 31.5 | 87.1 | 14.422 | 14.412 | 33.1 | 67.6 | 489.7 | 64.1 | 29.0 | 5.5 | -4.3 |
| 112 | 47.2 | 14.421 | 14.412 | 32.8 | 93.3 | 14.424 | 14.415 | 33.0 | 73.8 | 485.2 | 70.3 | 30.2 | 5.9 | -5.2 |
| 113 | 53.1 | 14.421 | 14.411 | 34.0 | 99.2 | 14.423 | 14.414 | 32.3 | 79.7 | 489.1 | 76.2 | 23.6 | 4.0 | -5.0 |
| 114 | 59.0 | 14.422 | 14.412 | 34.2 | 105.1 | 14.421 | 14.413 | 32.1 | 85.6 | 497.0 | 82.1 | 29.8 | -3.9 | 1.5 |
| | | | | | | | | | | | | | | |
| 115 | 65.2 | 14.422 | 14.411 | 35.7 | 111.3 | 14.418 | 14.410 | 32.1 | 91.8 | 499.1 | 88.3 | 25.1 | -4.7 | -1.8 |
| 116 | 71.1 | 14.422 | 14.413 | 33.9 | 117.2 | 14.417 | 14.409 | 31.1 | 97.7 | 499.4 | 94.2 | 25.7 | -5.2 | -4.9 |
| 117 | 76.8 | 14.417 | 14.413 | 21.5 | 123.0 | 14.417 | 14.410 | 28.8 | 103.5 | 501.0 | 100.0 | 26.4 | -4.9 | -5.7 |
| 118 | 83.0 | 14.422 | 14.414 | 30.5 | 129.1 | 14.418 | 14.412 | 25.6 | 109.6 | 498.2 | 106.1 | 27.1 | -4.8 | -4.7 |
| 119 | 94.7 | 14.419 | 14.410 | 33.4 | 140.9 | 14.413 | 14.410 | 18.2 | 121.4 | 499.6 | 117.9 | 23.8 | -2.6 | -5.8 |
| | | | | | | | | | | | | | | |
| 120 | 107.0 | 14.419 | 14.410 | 32.8 | 153.1 | 14.411 | 14.409 | 15.9 | 133.6 | 496.1 | 130.1 | 15.3 | -0.9 | -7.1 |
| 121 | 119.3 | 14.418 | 14.410 | 30.8 | 165.4 | 14.414 | 14.410 | 20.7 | 145.9 | 495.9 | 142.4 | 3.0 | 1.2 | -7.4 |
| 122 | 130.8 | 14.415 | 14.410 | 25.5 | 177.0 | 14.416 | 14.411 | 25.7 | 157.5 | 495.3 | 154.0 | 3.0 | -6 | -7.5 |
| 123 | 143.2 | 14.411 | 14.408 | 17.5 | 189.3 | 14.416 | 14.409 | 28.4 | 169.8 | 497.4 | 166.3 | 12.8 | .3 | -6.6 |
| 124 | 154.7 | 14.412 | 14.410 | 16.8 | 200.9 | 14.418 | 14.411 | 28.9 | 181.4 | 498.4 | 177.9 | 18.7 | 3.4 | -6.1 |
| | | | | | | | | | | | | | | |
| 125 | 166.8 | 14.413 | 14.409 | 22.2 | 213.0 | 14.418 | 14.410 | 30.5 | 193.5 | 500.3 | 190.0 | 22.5 | 5.4 | -5.9 |
| 126 | 179.1 | 14.415 | 14.409 | 26.8 | 225.2 | 14.419 | 14.411 | 30.9 | 205.7 | 500.7 | 202.2 | 24.9 | 6.7 | -4.5 |
| 127 | 184.9 | 14.415 | 14.408 | 28.2 | 231.1 | 14.413 | 14.412 | 10.1 | 211.6 | 500.1 | 208.1 | 25.5 | 7.7 | -4.0 |
| 128 | 176.4 | 14.414 | 14.408 | 25.9 | 222.5 | 14.418 | 14.410 | 31.4 | 203.0 | 500.4 | 199.5 | 24.2 | 6.4 | -5.0 |
| 129 | 197.1 | 14.415 | 14.408 | 29.3 | 243.2 | 14.414 | 14.406 | 30.8 | 223.7 | 501.6 | 220.2 | 28.1 | 7.0 | -3.8 |

TABLE 20.—Concluded.

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | | Wind anemometer | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 130 | 203.0 | 14.416 | 14.409 | 29.6 | 249.1 | 14.412 | 14.406 | 27.1 | 229.6 | 501.8 | 226.1 | 23.2 | -5.8 | |
| 131 | 209.0 | 14.418 | 14.410 | 30.3 | 255.1 | 14.414 | 14.408 | 27.5 | 235.6 | 501.5 | 232.1 | 11.8 | -11.7 | |
| 132 | 215.2 | 14.419 | 14.410 | 31.4 | 261.4 | 14.412 | 14.407 | 24.7 | 241.9 | 501.9 | 238.4 | .4 | -4.6 | |
| 133 | 221.0 | 14.419 | 14.411 | 32.1 | 267.2 | 14.413 | 14.409 | 22.9 | 247.7 | 501.0 | 244.2 | 21.7 | -1.9 | |
| 134 | 227.1 | 14.419 | 14.411 | 30.4 | 273.3 | 14.407 | 14.404 | 19.7 | 253.8 | 502.4 | 250.3 | 19.1 | -4.1 | |
| 135 | 233.0 | 14.413 | 14.412 | 9.2 | 279.1 | 14.411 | 14.409 | 18.2 | 259.6 | 501.1 | 256.1 | 18.6 | -4.0 | |
| 136 | 239.0 | 14.419 | 14.410 | 32.9 | 285.1 | 14.407 | 14.406 | 12.6 | 265.6 | 501.7 | 262.1 | 16.6 | -4.1 | |
| 137 | 245.2 | 14.417 | 14.410 | 30.1 | 291.4 | 14.408 | 14.407 | 11.7 | 271.9 | 501.3 | 268.4 | 11.6 | -3.6 | |
| 138 | 251.2 | 14.417 | 14.410 | 27.7 | 297.3 | 14.408 | 14.408 | 8.4 | 277.8 | 501.1 | 274.3 | 7.7 | -1.7 | |
| 139 | 257.0 | 14.414 | 14.408 | 27.4 | 303.1 | 14.408 | 14.407 | 4.9 | 283.6 | 501.3 | 280.1 | 4.8 | -5 | |
| 140 | 260.4 | 14.414 | 14.408 | 26.9 | 306.5 | 14.407 | 14.407 | 0.0 | 287.0 | 501.6 | 283.5 | 3.2 | 1.1 | |
| 141 | 243.1 | 14.419 | 14.411 | 31.3 | 289.3 | 14.409 | 14.408 | 12.5 | 269.8 | 500.6 | 266.3 | 13.6 | -3.4 | |
| 142 | 224.9 | 14.419 | 14.411 | 30.8 | 271.0 | 14.411 | 14.407 | 21.2 | 251.5 | 500.9 | 248.0 | 19.3 | -3.5 | |
| 143 | 207.4 | 14.416 | 14.409 | 29.7 | 253.5 | 14.414 | 14.408 | 27.2 | 234.0 | 500.6 | 230.5 | 20.9 | -10.5 | |
| 144 | 189.1 | 14.412 | 14.405 | 29.0 | 235.3 | 14.414 | 14.408 | 27.5 | 215.8 | 501.4 | 212.3 | 25.1 | -4.1 | |
| 145 | 171.2 | 14.412 | 14.407 | 24.1 | 217.3 | 14.417 | 14.409 | 31.2 | 197.8 | 499.5 | 194.3 | 22.7 | 5.8 | |
| 146 | 153.3 | 14.409 | 14.407 | 16.7 | 199.4 | 14.415 | 14.408 | 28.9 | 179.9 | 499.5 | 176.4 | 18.5 | -5.8 | |
| 147 | 135.1 | 14.412 | 14.407 | 22.7 | 181.2 | 14.413 | 14.407 | 26.9 | 161.7 | 497.8 | 158.2 | 8.8 | -1.2 | |
| 148 | 117.0 | 14.415 | 14.407 | 31.5 | 163.2 | 14.409 | 14.405 | 19.9 | 143.7 | 497.8 | 140.2 | 7.3 | 0.0 | |
| 149 | 99.5 | 14.418 | 14.409 | 33.0 | 145.6 | 14.407 | 14.405 | 15.6 | 126.1 | 493.5 | 122.6 | 20.0 | -8.1 | |
| 150 | 81.0 | 14.412 | 14.411 | 8.2 | 127.1 | 14.415 | 14.409 | 27.2 | 107.6 | 497.9 | 104.1 | 26.4 | -5.1 | |
| 151 | 63.1 | 14.418 | 14.408 | 35.5 | 109.2 | 14.417 | 14.408 | 32.6 | 89.7 | 498.6 | 86.2 | 27.8 | -4.5 | |
| 152 | 45.5 | 14.415 | 14.406 | 32.9 | 91.6 | 14.414 | 14.405 | 32.6 | 72.1 | 490.4 | 68.6 | 30.8 | -4.8 | |
| 153 | 27.0 | 14.412 | 14.407 | 23.6 | 73.2 | 14.417 | 14.410 | 29.9 | 53.7 | 491.3 | 50.2 | 27.3 | -4.4 | |
| 154 | 9.2 | 14.408 | 14.407 | 13.1 | 55.3 | 14.418 | 14.408 | 33.7 | 35.8 | 492.9 | 32.3 | 14.9 | -4.1 | |
| 155 | 5.7 | 14.407 | 14.406 | 11.7 | 51.8 | 14.415 | 14.405 | 33.5 | 32.3 | 491.7 | 28.8 | 13.7 | -5.0 | |

TABLE 21.—DATA LISTING FOR TRAVERSE 1 AT STATION 5—VERTICAL SURVEY AT INSIDE WALL
 [Test section data for reading 711; total pressure, 14.362; static pressure, 12.256 psia; total temperature, 499°R; velocity, 351.6 mph; fan speed, 395.9 rpm.]

| Reading number | Position, in. | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|-----------------|------------------|------------|----------|
| | | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 711 | 6.5 | 14.326 | 14.324 | 15.7 | 53.5 | 14.336 | 14.323 | 39.8 | 35.2 | 496.5 | 30.4 | 21.8 | 9.1 | -6.3 |
| 712 | 10.9 | 14.326 | 14.323 | 19.7 | 57.9 | 14.342 | 14.327 | 42.1 | 39.7 | 496.3 | 34.8 | 22.2 | 10.3 | -1.1 |
| 713 | 17.2 | 14.333 | 14.329 | 21.0 | 64.2 | 14.345 | 14.330 | 43.1 | 45.9 | 496.4 | 41.0 | 29.6 | 9.0 | 3.0 |
| 714 | 23.0 | 14.329 | 14.324 | 25.2 | 70.0 | 14.342 | 14.327 | 43.2 | 51.7 | 496.5 | 46.9 | 28.2 | 7.2 | -2.6 |
| 715 | 29.0 | 14.333 | 14.326 | 28.7 | 76.0 | 14.342 | 14.326 | 43.6 | 57.8 | 496.5 | 52.9 | 34.4 | .8 | -3.2 |
| 716 | 35.0 | 14.333 | 14.325 | 30.4 | 82.0 | 14.339 | 14.326 | 40.3 | 63.7 | 496.3 | 58.9 | 34.7 | 1.2 | 1.8 |
| 717 | 41.1 | 14.336 | 14.326 | 34.0 | 88.1 | 14.336 | 14.323 | 39.8 | 69.9 | 497.0 | 65.0 | 36.5 | 1.2 | .7 |
| 718 | 47.1 | 14.336 | 14.325 | 36.1 | 94.1 | 14.342 | 14.327 | 43.3 | 75.8 | 497.6 | 70.9 | 39.9 | -3.2 | 5.1 |
| 719 | 53.1 | 14.339 | 14.327 | 38.3 | 100.1 | 14.339 | 14.324 | 43.1 | 81.8 | 496.0 | 77.0 | 38.9 | -1.4 | 9.2 |
| 720 | 59.0 | 14.339 | 14.324 | 41.4 | 106.0 | 14.339 | 14.324 | 42.5 | 87.8 | 494.5 | 82.9 | 36.9 | -1.8 | 8.3 |
| 721 | 65.1 | 14.342 | 14.327 | 42.6 | 112.1 | 14.342 | 14.328 | 40.8 | 93.8 | 496.5 | 88.9 | 34.8 | -5.2 | -0.3 |
| 722 | 70.9 | 14.342 | 14.327 | 42.8 | 117.9 | 14.339 | 14.325 | 41.7 | 99.7 | 499.1 | 94.8 | 39.2 | 1.2 | -2.6 |
| 723 | 76.8 | 14.342 | 14.327 | 42.2 | 123.8 | 14.342 | 14.329 | 40.5 | 105.6 | 499.5 | 100.7 | 35.8 | 4.8 | -1.1 |
| 724 | 83.0 | 14.339 | 14.326 | 39.6 | 130.0 | 14.342 | 14.329 | 39.3 | 111.7 | 500.2 | 106.9 | 40.0 | 5.6 | -1.4 |
| 725 | 95.0 | 14.345 | 14.329 | 43.4 | 142.0 | 14.336 | 14.329 | 29.5 | 123.7 | 502.2 | 118.8 | 37.1 | 6.4 | -.7 |
| 726 | 107.0 | 14.342 | 14.327 | 42.1 | 154.0 | 14.330 | 14.324 | 25.5 | 135.8 | 500.9 | 130.9 | 36.0 | 6.7 | -1.6 |
| 727 | 119.0 | 14.345 | 14.330 | 42.1 | 166.0 | 14.333 | 14.327 | 27.5 | 147.8 | 500.7 | 142.9 | 24.0 | 7.6 | -2.1 |
| 728 | 131.0 | 14.339 | 14.327 | 38.1 | 178.0 | 14.336 | 14.326 | 34.7 | 159.7 | 499.6 | 154.9 | 18.1 | 4.8 | -5.3 |
| 729 | 142.9 | 14.333 | 14.326 | 29.1 | 189.9 | 14.339 | 14.328 | 37.3 | 171.6 | 497.8 | 166.8 | 19.8 | 3.4 | -2.7 |
| 730 | 154.9 | 14.333 | 14.328 | 24.6 | 201.9 | 14.339 | 14.327 | 38.0 | 183.7 | 498.4 | 178.8 | 29.8 | 4.8 | -6.0 |
| 731 | 166.9 | 14.333 | 14.326 | 28.1 | 213.9 | 14.342 | 14.327 | 42.7 | 195.7 | 498.9 | 190.8 | 31.9 | 4.7 | -1.4 |
| 732 | 178.9 | 14.336 | 14.326 | 34.6 | 225.9 | 14.339 | 14.328 | 37.1 | 207.7 | 498.9 | 202.8 | 34.8 | 3.5 | .1 |
| 733 | 185.0 | 14.339 | 14.327 | 37.1 | 232.0 | 14.342 | 14.331 | 36.8 | 213.8 | 498.9 | 208.9 | 34.3 | 2.8 | 4.2 |
| 734 | 191.5 | 14.339 | 14.327 | 38.4 | 238.5 | 14.342 | 14.329 | 39.7 | 220.2 | 499.2 | 215.4 | 35.2 | 3.8 | 6.9 |
| 735 | 196.9 | 14.339 | 14.327 | 37.4 | 243.9 | 14.342 | 14.331 | 37.0 | 225.7 | 499.8 | 220.8 | 34.4 | 2.7 | 5.6 |

TABLE 21.—Concluded.

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | | Wind anemometer | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 736 | 203.1 | 14.339 | 14.327 | 37.9 | 250.1 | 14.342 | 14.331 | 36.3 | 231.8 | 500.5 | 226.9 | 33.7 | -4.6 | 3.7 |
| 737 | 208.9 | 14.342 | 14.328 | 40.6 | 255.9 | 14.336 | 14.327 | 32.4 | 237.6 | 501.1 | 232.8 | 32.0 | -2.9 | -1.2 |
| 738 | 215.0 | 14.342 | 14.328 | 41.0 | 262.0 | 14.336 | 14.328 | 30.5 | 243.8 | 501.9 | 238.9 | 35.5 | .9 | -2.7 |
| 739 | 221.0 | 14.342 | 14.329 | 39.6 | 268.0 | 14.336 | 14.330 | 28.2 | 249.7 | 502.0 | 244.9 | 30.3 | .2 | -1.9 |
| 740 | 227.0 | 14.342 | 14.331 | 36.7 | 274.0 | 14.336 | 14.331 | 24.3 | 255.8 | 502.0 | 250.9 | 26.5 | 8.2 | 4.5 |
| 741 | 233.1 | 14.342 | 14.331 | 36.9 | 280.1 | 14.333 | 14.330 | 20.4 | 261.8 | 502.0 | 256.9 | 30.3 | 6.8 | 0.0 |
| 742 | 238.9 | 14.342 | 14.329 | 39.1 | 285.9 | 14.333 | 14.330 | 18.1 | 267.6 | 502.2 | 262.8 | 28.5 | .2 | -2.8 |
| 743 | 244.8 | 14.342 | 14.330 | 37.9 | 291.8 | 14.330 | 14.327 | 18.1 | 273.6 | 502.5 | 268.7 | 17.1 | 5.2 | -9.3 |
| 744 | 251.1 | 14.342 | 14.333 | 33.7 | 298.1 | 14.336 | 14.333 | 19.5 | 279.8 | 502.2 | 274.9 | 17.6 | 6.2 | -2.3 |
| 745 | 256.9 | 14.342 | 14.334 | 30.9 | 303.9 | 14.336 | 14.333 | 19.7 | 285.7 | 503.1 | 280.8 | 11.7 | 8.0 | -4 |
| 746 | 243.1 | 14.345 | 14.332 | 39.7 | 290.1 | 14.336 | 14.333 | 18.8 | 271.9 | 502.9 | 267.0 | 24.9 | 3.7 | -1.1 |
| 747 | 225.5 | 14.345 | 14.334 | 37.1 | 272.5 | 14.339 | 14.333 | 27.4 | 254.3 | 503.0 | 249.4 | 30.2 | 3.7 | -1 |
| 748 | 207.3 | 14.348 | 14.335 | 39.9 | 254.3 | 14.339 | 14.330 | 33.0 | 236.0 | 503.0 | 231.2 | 33.3 | 4.1 | -1 |
| 749 | 189.4 | 14.342 | 14.330 | 37.4 | 236.4 | 14.345 | 14.333 | 38.6 | 218.1 | 503.3 | 213.3 | 35.2 | 4.0 | 6.9 |
| 750 | 170.8 | 14.342 | 14.334 | 30.1 | 217.8 | 14.349 | 14.335 | 41.0 | 199.5 | 502.7 | 194.6 | 33.1 | 4.1 | 1.0 |
| 751 | 153.4 | 14.339 | 14.333 | 25.4 | 200.4 | 14.345 | 14.334 | 36.7 | 182.2 | 499.1 | 177.3 | 30.0 | 3.2 | -1.8 |
| 752 | 135.1 | 14.342 | 14.332 | 34.6 | 182.1 | 14.345 | 14.334 | 36.4 | 163.9 | 499.1 | 159.0 | 19.0 | 5.3 | -8.8 |
| 753 | 117.4 | 14.348 | 14.334 | 41.1 | 164.4 | 14.339 | 14.333 | 26.8 | 146.2 | 500.8 | 141.3 | 21.2 | 5.1 | -4.8 |
| 754 | 99.1 | 14.351 | 14.335 | 44.2 | 146.1 | 14.336 | 14.329 | 28.4 | 127.8 | 502.0 | 123.0 | 37.5 | 8.8 | -1.5 |
| 755 | 81.0 | 14.348 | 14.334 | 40.7 | 128.0 | 14.349 | 14.336 | 39.5 | 109.7 | 500.6 | 104.9 | 36.2 | 7.0 | -1.5 |
| 756 | 63.0 | 14.351 | 14.335 | 43.7 | 110.0 | 14.349 | 14.334 | 42.0 | 91.7 | 497.1 | 86.8 | 36.6 | -6.2 | 3.1 |
| 757 | 45.4 | 14.345 | 14.335 | 35.6 | 92.4 | 14.352 | 14.337 | 41.7 | 74.2 | 498.5 | 69.3 | 39.8 | 1.0 | 2.5 |
| 758 | 27.1 | 14.342 | 14.336 | 27.4 | 74.1 | 14.349 | 14.333 | 42.5 | 55.9 | 497.6 | 51.0 | 30.2 | 6.6 | .5 |
| 759 | 8.9 | 14.339 | 14.337 | 16.7 | 55.9 | 14.352 | 14.337 | 41.8 | 37.7 | 496.9 | 32.8 | 24.3 | 6.5 | -5.8 |
| 760 | 6.5 | 14.339 | 14.336 | 16.9 | 53.5 | 14.349 | 14.336 | 39.4 | 35.2 | 496.7 | 30.4 | 24.8 | 4.4 | -7.1 |

TABLE 22.—DATA LISTING FOR TRAVERSE 2 AT STATION 5—VERTICAL SURVEY AT CENTERLINE
[Test section data for reading 711: total pressure, 14.362; static pressure, 12.256 psia; total temperature, 499 °R; velocity, 351.6 mph; fan speed, 395.9 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 711 | 4.6 | 14.340 | 14.338 | 16.8 | 50.7 | 14.352 | 14.343 | 38.7 | 31.2 | 494.7 | 27.7 | 25.0 | 2.3 | 1.2 |
| 712 | 11.2 | 14.346 | 14.342 | 22.0 | 57.3 | 14.358 | 14.341 | 42.0 | 37.8 | 493.8 | 34.3 | 29.1 | 4.0 | .4 |
| 713 | 17.6 | 14.343 | 14.338 | 24.4 | 63.7 | 14.358 | 14.341 | 45.2 | 44.2 | 494.5 | 40.7 | 30.4 | 5.0 | -8.2 |
| 714 | 23.1 | 14.346 | 14.340 | 26.4 | 69.2 | 14.358 | 14.341 | 45.0 | 49.7 | 494.5 | 46.2 | 27.4 | 7.9 | -9.1 |
| 715 | 29.0 | 14.353 | 14.344 | 31.6 | 75.2 | 14.361 | 14.342 | 46.9 | 55.7 | 494.6 | 52.2 | 33.0 | 8.1 | -2.1 |
| 716 | 34.9 | 14.349 | 14.339 | 36.0 | 81.0 | 14.361 | 14.342 | 47.6 | 61.5 | 494.7 | 58.0 | 38.6 | 5.1 | -1.7 |
| 717 | 41.3 | 14.349 | 14.337 | 38.3 | 87.4 | 14.361 | 14.342 | 47.2 | 67.9 | 494.7 | 64.4 | 36.9 | 9.0 | -4.0 |
| 718 | 47.1 | 14.356 | 14.343 | 39.5 | 93.3 | 14.358 | 14.339 | 47.0 | 73.8 | 494.8 | 70.3 | 42.4 | 6.7 | -3.8 |
| 719 | 53.4 | 14.356 | 14.341 | 41.5 | 99.5 | 14.358 | 14.341 | 44.4 | 80.0 | 495.5 | 76.5 | 45.9 | 6.7 | -1.9 |
| 720 | 59.1 | 14.356 | 14.339 | 44.3 | 105.2 | 14.355 | 14.339 | 42.7 | 85.7 | 495.7 | 82.2 | 42.9 | 6.4 | -1.6 |
| 721 | 65.1 | 14.359 | 14.342 | 45.1 | 111.3 | 14.355 | 14.341 | 40.2 | 91.8 | 496.3 | 88.3 | 44.2 | 5.8 | -0.6 |
| 722 | 71.2 | 14.359 | 14.341 | 46.6 | 117.3 | 14.352 | 14.339 | 38.1 | 97.8 | 496.5 | 94.3 | 46.2 | 6.3 | -.8 |
| 723 | 77.3 | 14.359 | 14.340 | 47.6 | 123.4 | 14.345 | 14.336 | 33.2 | 103.9 | 496.8 | 100.4 | 41.7 | 5.9 | -1.7 |
| 724 | 83.3 | 14.362 | 14.342 | 48.2 | 129.4 | 14.345 | 14.338 | 29.3 | 109.9 | 496.0 | 106.4 | 39.5 | 5.8 | -2.5 |
| 725 | 95.0 | 14.359 | 14.341 | 46.6 | 141.1 | 14.345 | 14.340 | 25.8 | 121.6 | 494.9 | 118.1 | 31.4 | 5.9 | .1 |
| 726 | 107.1 | 14.356 | 14.341 | 42.0 | 153.3 | 14.345 | 14.340 | 25.7 | 133.8 | 493.8 | 130.3 | 22.5 | 4.9 | 0.6 |
| 727 | 118.9 | 14.353 | 14.341 | 36.8 | 165.0 | 14.345 | 14.338 | 29.1 | 145.5 | 493.0 | 142.0 | 21.0 | 6.6 | -3.7 |
| 728 | 131.3 | 14.346 | 14.340 | 28.4 | 177.4 | 14.352 | 14.342 | 33.3 | 157.9 | 492.7 | 154.4 | 21.2 | 2.4 | 1.6 |
| 729 | 143.0 | 14.343 | 14.338 | 25.4 | 189.1 | 14.352 | 14.340 | 36.5 | 169.6 | 492.5 | 166.1 | 21.1 | 2.4 | 1.1 |
| 730 | 154.8 | 14.346 | 14.340 | 26.4 | 200.9 | 14.355 | 14.341 | 40.1 | 181.4 | 493.4 | 177.9 | 31.6 | 1.6 | -1.1 |
| 731 | 166.9 | 14.346 | 14.338 | 31.5 | 213.1 | 14.358 | 14.342 | 43.5 | 193.6 | 494.8 | 190.1 | 33.8 | 2.9 | -1.9 |
| 732 | 178.9 | 14.349 | 14.339 | 34.6 | 225.0 | 14.358 | 14.343 | 41.5 | 205.5 | 496.0 | 202.0 | 39.1 | 2.7 | -.1 |
| 733 | 184.9 | 14.353 | 14.341 | 36.6 | 231.0 | 14.358 | 14.343 | 42.2 | 211.5 | 496.3 | 208.0 | 38.5 | 2.0 | -1.0 |
| 734 | 190.9 | 14.353 | 14.341 | 37.3 | 237.0 | 14.358 | 14.344 | 41.2 | 217.5 | 496.0 | 214.0 | 41.8 | 2.5 | .1 |
| 735 | 196.9 | 14.353 | 14.340 | 39.4 | 243.0 | 14.355 | 14.342 | 39.6 | 223.5 | 497.0 | 220.0 | 40.6 | 2.8 | .2 |

TABLE 22.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 736 | 203.5 | 14.353 | 14.338 | 41.5 | 249.6 | 14.355 | 14.344 | 36.4 | 230.1 | 499.0 | 226.6 | 39.5 | 3.3 | -0.9 |
| 737 | 209.0 | 14.356 | 14.341 | 42.7 | 255.2 | 14.352 | 14.340 | 36.5 | 235.7 | 500.6 | 232.2 | 38.9 | 3.8 | -1.4 |
| 738 | 214.2 | 14.356 | 14.341 | 42.8 | 260.3 | 14.348 | 14.339 | 34.0 | 240.8 | 501.4 | 237.3 | 35.5 | 2.7 | 1.0 |
| 739 | 221.2 | 14.356 | 14.340 | 43.0 | 267.3 | 14.348 | 14.339 | 33.2 | 247.8 | 501.6 | 244.3 | 34.8 | 3.5 | -1.9 |
| 740 | 227.4 | 14.356 | 14.341 | 42.2 | 273.6 | 14.348 | 14.341 | 30.8 | 254.1 | 501.8 | 250.6 | 30.8 | 3.8 | -4.4 |
| 741 | 232.6 | 14.356 | 14.341 | 41.7 | 278.7 | 14.345 | 14.339 | 28.1 | 259.2 | 501.8 | 255.7 | 37.1 | 4.6 | 0.1 |
| 742 | 238.9 | 14.356 | 14.342 | 41.0 | 285.0 | 14.348 | 14.344 | 22.4 | 265.5 | 502.2 | 262.0 | 20.1 | 2.9 | 4.6 |
| 743 | 245.5 | 14.356 | 14.343 | 38.6 | 299.7 | 14.342 | 14.339 | 19.3 | 272.2 | 502.2 | 268.7 | 26.5 | 5.2 | 2.1 |
| 744 | 251.1 | 14.356 | 14.344 | 37.9 | 297.2 | 14.342 | 14.340 | 16.8 | 277.7 | 502.5 | 274.2 | 24.5 | 6.2 | .6 |
| 745 | 255.1 | 14.353 | 14.342 | 35.6 | 301.2 | 14.339 | 14.338 | 12.5 | 281.7 | 502.7 | 278.2 | 9.9 | 9.8 | -1.6 |
| 746 | 243.4 | 14.359 | 14.345 | 40.4 | 289.5 | 14.345 | 14.342 | 21.2 | 270.0 | 502.9 | 266.5 | 24.2 | 6.1 | 0.1 |
| 747 | 225.3 | 14.359 | 14.343 | 43.8 | 271.5 | 14.348 | 14.340 | 31.6 | 252.0 | 502.9 | 248.5 | 38.7 | 6.0 | -1.6 |
| 748 | 207.2 | 14.359 | 14.343 | 43.1 | 253.4 | 14.352 | 14.340 | 38.1 | 233.9 | 502.7 | 230.4 | 40.5 | 3.8 | .6 |
| 749 | 189.8 | 14.353 | 14.341 | 37.6 | 236.0 | 14.355 | 14.340 | 41.8 | 216.5 | 501.4 | 213.0 | 42.3 | 2.4 | -7 |
| 750 | 170.5 | 14.353 | 14.344 | 32.2 | 216.6 | 14.358 | 14.341 | 44.3 | 197.1 | 497.8 | 193.6 | 35.3 | 2.9 | -2.4 |
| 751 | 153.4 | 14.349 | 14.344 | 25.1 | 199.5 | 14.355 | 14.342 | 38.7 | 180.0 | 495.1 | 176.5 | 27.9 | 1.2 | -2.2 |
| 752 | 135.4 | 14.349 | 14.343 | 27.3 | 181.5 | 14.355 | 14.345 | 34.6 | 162.0 | 494.3 | 158.5 | 19.1 | 2.9 | -1.0 |
| 753 | 117.4 | 14.353 | 14.341 | 37.4 | 163.5 | 14.348 | 14.342 | 28.0 | 144.0 | 494.3 | 140.5 | 20.2 | 4.5 | 1.4 |
| 754 | 99.3 | 14.365 | 14.348 | 45.5 | 145.4 | 14.345 | 14.340 | 25.7 | 125.9 | 495.1 | 122.4 | 31.0 | 6.1 | -.9 |
| 755 | 81.3 | 14.365 | 14.346 | 47.4 | 127.4 | 14.355 | 14.346 | 31.8 | 107.9 | 496.0 | 104.4 | 37.8 | 5.8 | -2.1 |
| 756 | 62.9 | 14.365 | 14.347 | 45.8 | 109.0 | 14.361 | 14.346 | 42.0 | 89.5 | 496.8 | 86.0 | 48.0 | 6.4 | -1.6 |
| 757 | 44.9 | 14.359 | 14.346 | 38.7 | 91.1 | 14.361 | 14.343 | 46.5 | 71.6 | 495.6 | 68.1 | 40.2 | 7.2 | -3.1 |
| 758 | 27.0 | 14.353 | 14.345 | 29.6 | 73.2 | 14.364 | 14.346 | 46.9 | 53.7 | 495.3 | 50.2 | 35.8 | 4.5 | -9.2 |
| 759 | 9.2 | 14.349 | 14.346 | 20.9 | 55.4 | 14.361 | 14.346 | 42.3 | 35.9 | 494.9 | 32.4 | 24.2 | 5.1 | -2.4 |
| 760 | 5.5 | 14.349 | 14.346 | 19.2 | 51.7 | 14.361 | 14.347 | 41.0 | 32.2 | 495.0 | 28.7 | 24.9 | .7 | .6 |

TABLE 23.—DATA LISTING FOR TRAVERSE 1 AT STATION 5—VERTICAL SURVEY
 [Test section data for reading 991; total pressure, 14.273; static pressure, 12.190 psia; total temperature, 498 °R; velocity, 350.4 mph; fan speed, 395.5 rpm.]

| Reading number | Position, in. | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|-----------------|------------------|------------|----------|
| | | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 991 | 6.8 | 14.254 | 14.250 | 21.3 | 53.8 | 14.263 | 14.248 | 42.8 | 35.6 | 486.3 | 30.7 | 27.1 | 4.9 | 0.8 |
| 992 | 11.1 | 14.255 | 14.250 | 24.6 | 58.1 | 14.265 | 14.249 | 43.6 | 39.9 | 486.8 | 35.0 | 29.6 | 5.7 | -1.0 |
| 993 | 17.1 | 14.257 | 14.250 | 27.5 | 64.1 | 14.265 | 14.249 | 44.3 | 45.9 | 486.6 | 41.0 | 31.9 | 5.0 | -8 |
| 994 | 22.9 | 14.257 | 14.249 | 30.5 | 69.9 | 14.265 | 14.248 | 44.3 | 51.7 | 486.4 | 46.8 | 33.9 | 5.4 | -7 |
| 995 | 28.2 | 14.259 | 14.250 | 33.2 | 75.2 | 14.264 | 14.247 | 43.4 | 57.0 | 486.5 | 52.1 | 36.0 | 6.4 | -1.0 |
| 996 | 35.3 | 14.260 | 14.249 | 36.4 | 82.3 | 14.262 | 14.246 | 42.9 | 64.0 | 486.4 | 59.2 | 37.5 | 7.4 | -1.1 |
| 997 | 40.9 | 14.263 | 14.250 | 38.9 | 87.9 | 14.263 | 14.247 | 43.4 | 69.7 | 486.8 | 64.8 | 37.8 | 8.3 | 0.0 |
| 998 | 46.9 | 14.263 | 14.249 | 41.2 | 93.9 | 14.263 | 14.246 | 44.3 | 75.6 | 488.2 | 70.8 | 38.2 | 8.1 | -8 |
| 999 | 53.0 | 14.264 | 14.249 | 42.9 | 100.0 | 14.262 | 14.246 | 44.1 | 81.7 | 489.8 | 76.9 | 38.3 | 8.1 | .2 |
| 1000 | 59.2 | 14.265 | 14.249 | 43.9 | 106.2 | 14.261 | 14.245 | 43.0 | 87.9 | 492.2 | 83.1 | 37.7 | 8.1 | .1 |
| 1001 | 65.1 | 14.265 | 14.248 | 44.0 | 112.1 | 14.259 | 14.245 | 40.8 | 93.9 | 494.0 | 89.0 | 38.0 | 8.0 | 0.4 |
| 1002 | 70.9 | 14.264 | 14.248 | 43.3 | 117.9 | 14.257 | 14.245 | 39.0 | 99.7 | 495.8 | 94.8 | 38.5 | 8.5 | .1 |
| 1003 | 76.9 | 14.264 | 14.249 | 43.1 | 123.9 | 14.256 | 14.245 | 36.3 | 105.7 | 497.1 | 100.8 | 38.1 | 9.2 | 0.0 |
| 1004 | 83.3 | 14.265 | 14.249 | 43.2 | 130.3 | 14.254 | 14.244 | 33.4 | 112.0 | 497.4 | 107.1 | 35.6 | 8.8 | .4 |
| 1005 | 95.0 | 14.264 | 14.248 | 44.3 | 142.0 | 14.252 | 14.245 | 30.6 | 123.7 | 496.9 | 118.9 | 31.2 | 9.5 | .3 |
| 1006 | 106.7 | 14.262 | 14.247 | 42.5 | 153.7 | 14.251 | 14.243 | 29.3 | 135.5 | 496.1 | 130.6 | 26.2 | 9.2 | 1.0 |
| 1007 | 119.0 | 14.260 | 14.247 | 39.1 | 166.0 | 14.250 | 14.243 | 28.4 | 147.7 | 495.3 | 142.9 | 22.8 | 8.8 | 2.7 |
| 1008 | 131.0 | 14.254 | 14.245 | 33.0 | 178.0 | 14.250 | 14.243 | 28.9 | 159.8 | 494.9 | 154.9 | 22.6 | 8.8 | 1.6 |
| 1009 | 143.1 | 14.252 | 14.245 | 29.9 | 190.1 | 14.252 | 14.242 | 34.5 | 171.8 | 494.2 | 166.9 | 20.5 | 9.2 | 1.1 |
| 1010 | 155.0 | 14.252 | 14.245 | 29.5 | 202.0 | 14.255 | 14.243 | 37.4 | 183.7 | 493.9 | 178.9 | 22.3 | 7.9 | 2.1 |
| 1011 | 166.9 | 14.252 | 14.245 | 27.6 | 213.9 | 14.255 | 14.242 | 39.5 | 195.6 | 495.2 | 190.8 | 27.6 | 6.5 | 0.1 |
| 1012 | 179.2 | 14.251 | 14.244 | 30.0 | 226.2 | 14.256 | 14.242 | 40.0 | 207.9 | 498.4 | 203.0 | 32.3 | 6.9 | -.3 |
| 1013 | 185.0 | 14.253 | 14.244 | 32.4 | 232.0 | 14.256 | 14.243 | 39.4 | 213.8 | 499.8 | 208.9 | 32.8 | 6.9 | -.3 |
| 1014 | 190.7 | 14.254 | 14.244 | 35.1 | 237.7 | 14.254 | 14.241 | 38.2 | 219.5 | 501.0 | 214.6 | 34.2 | 6.9 | .3 |
| 1015 | 197.0 | 14.254 | 14.243 | 37.2 | 244.0 | 14.252 | 14.241 | 36.9 | 225.8 | 501.6 | 220.9 | 34.7 | 7.6 | .7 |

TABLE 23.—Concluded.

| Reading number | Probe one | | | Probe two o | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1016 | 202.8 | 14.255 | 14.243 | 37.9 | 249.8 | 14.250 | 14.240 | 35.1 | 231.6 | 501.8 | 226.7 | 34.6 | 7.3 | 0.7 |
| 1017 | 208.8 | 14.255 | 14.242 | 38.9 | 255.8 | 14.249 | 14.240 | 34.2 | 237.6 | 501.9 | 232.7 | 34.4 | 7.5 | .2 |
| 1018 | 214.9 | 14.255 | 14.242 | 39.3 | 261.9 | 14.248 | 14.239 | 32.5 | 243.6 | 502.1 | 238.8 | 32.4 | 7.4 | .5 |
| 1019 | 220.9 | 14.255 | 14.242 | 40.0 | 267.9 | 14.247 | 14.239 | 30.7 | 249.7 | 502.1 | 244.8 | 31.1 | 7.4 | 1.0 |
| 1020 | 227.0 | 14.255 | 14.242 | 39.9 | 274.0 | 14.246 | 14.239 | 29.0 | 255.8 | 502.0 | 250.9 | 29.5 | 8.5 | .5 |
| 1021 | 232.9 | 14.254 | 14.242 | 38.9 | 279.9 | 14.245 | 14.239 | 27.5 | 261.7 | 502.1 | 256.8 | 27.1 | 7.2 | 1.7 |
| 1022 | 238.8 | 14.254 | 14.242 | 37.7 | 285.8 | 14.244 | 14.238 | 26.0 | 267.6 | 502.2 | 262.7 | 26.8 | 8.0 | 1.7 |
| 1023 | 245.0 | 14.252 | 14.241 | 36.0 | 292.0 | 14.242 | 14.238 | 24.0 | 273.8 | 502.3 | 268.9 | 23.5 | 9.9 | .8 |
| 1024 | 250.8 | 14.251 | 14.241 | 34.7 | 297.8 | 14.242 | 14.238 | 22.6 | 279.5 | 502.4 | 274.7 | 22.9 | 8.6 | 2.3 |
| 1025 | 256.8 | 14.249 | 14.240 | 32.6 | 303.8 | 14.241 | 14.237 | 20.0 | 285.5 | 502.5 | 280.7 | 21.0 | 8.2 | 1.6 |
| 1026 | 261.2 | 14.248 | 14.240 | 32.1 | 308.2 | 14.239 | 14.237 | 17.2 | 290.0 | 502.4 | 285.1 | 18.3 | 8.3 | 0.7 |
| 1027 | 242.8 | 14.250 | 14.239 | 36.7 | 289.8 | 14.240 | 14.235 | 24.3 | 271.6 | 502.3 | 266.7 | 25.1 | 8.3 | 1.3 |
| 1028 | 225.3 | 14.252 | 14.239 | 40.1 | 272.3 | 14.242 | 14.235 | 29.8 | 254.0 | 502.2 | 249.1 | 30.5 | 7.5 | 1.2 |
| 1029 | 206.8 | 14.251 | 14.239 | 38.7 | 253.8 | 14.246 | 14.236 | 34.3 | 235.5 | 502.0 | 230.7 | 34.6 | 7.6 | .6 |
| 1030 | 189.0 | 14.248 | 14.238 | 34.7 | 236.0 | 14.248 | 14.235 | 38.8 | 217.7 | 500.7 | 212.8 | 33.7 | 7.0 | .3 |
| 1031 | 171.3 | 14.243 | 14.237 | 27.8 | 218.3 | 14.249 | 14.235 | 39.9 | 200.0 | 496.4 | 195.1 | 30.1 | 6.2 | -0.6 |
| 1032 | 152.9 | 14.244 | 14.237 | 29.4 | 199.9 | 14.247 | 14.235 | 37.4 | 181.6 | 493.8 | 176.8 | 21.3 | 8.9 | 1.6 |
| 1033 | 135.1 | 14.245 | 14.236 | 32.0 | 182.1 | 14.242 | 14.234 | 31.0 | 163.8 | 494.3 | 159.0 | 21.5 | 9.4 | 1.1 |
| 1034 | 116.9 | 14.250 | 14.237 | 39.8 | 163.9 | 14.240 | 14.233 | 28.9 | 145.6 | 494.8 | 140.7 | 23.2 | 9.5 | 2.0 |
| 1035 | 99.2 | 14.255 | 14.238 | 44.2 | 146.2 | 14.241 | 14.234 | 30.0 | 128.0 | 495.8 | 123.1 | 29.2 | 9.9 | .4 |
| 1036 | 80.8 | 14.252 | 14.237 | 42.8 | 127.8 | 14.243 | 14.233 | 35.0 | 109.6 | 496.5 | 104.7 | 36.2 | 9.3 | 0.1 |
| 1037 | 62.9 | 14.254 | 14.238 | 43.6 | 109.9 | 14.249 | 14.234 | 41.8 | 91.7 | 493.5 | 86.8 | 37.7 | 8.4 | .2 |
| 1038 | 45.0 | 14.251 | 14.238 | 40.0 | 92.0 | 14.250 | 14.233 | 43.9 | 73.7 | 489.2 | 68.8 | 37.2 | 7.6 | -1.0 |
| 1039 | 25.4 | 14.244 | 14.236 | 31.6 | 72.4 | 14.249 | 14.233 | 43.1 | 54.1 | 488.1 | 49.3 | 34.2 | 5.8 | -1.7 |
| 1040 | 8.8 | 14.241 | 14.236 | 23.1 | 55.8 | 14.249 | 14.233 | 43.3 | 37.6 | 489.3 | 32.7 | 29.1 | 5.0 | .4 |
| 1041 | 7.1 | 14.240 | 14.236 | 21.8 | 54.1 | 14.248 | 14.232 | 42.7 | 35.8 | 489.5 | 31.0 | 26.4 | 5.6 | -2.7 |

TABLE 24.—DATA LISTING FOR TRAVERSE 1 AT STATION 5—VERTICAL SURVEY AT INSIDE WALL
 [Test section data for reading 761; total pressure, 14.378; static pressure, 13.271 psia; total temperature, 497°R; velocity, 250.7 mph; fan speed, 291.1 rpm.]

| Reading number | Probe one | | Probe two | | Thermocouple | | Wind anemometer | | | | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 761 | 6.5 | 14.348 | 14.347 | 13.2 | 53.5 | 14.356 | 14.349 | 29.3 | 35.2 | 493.0 | 30.4 | 13.8 | 9.5 | -4.6 |
| 762 | 11.3 | 14.348 | 14.346 | 15.1 | 58.3 | 14.356 | 14.347 | 31.9 | 40.1 | 494.0 | 35.2 | 11.1 | 8.4 | .2 |
| 763 | 17.2 | 14.348 | 14.346 | 16.7 | 64.2 | 14.356 | 14.347 | 33.0 | 45.9 | 494.9 | 41.0 | 19.7 | 4.5 | -4.0 |
| 764 | 23.1 | 14.348 | 14.345 | 20.3 | 70.1 | 14.359 | 14.350 | 32.7 | 51.8 | 494.9 | 47.0 | 20.9 | 1.9 | -3.2 |
| 765 | 28.9 | 14.348 | 14.344 | 21.5 | 75.9 | 14.356 | 14.347 | 32.5 | 57.7 | 494.8 | 52.8 | 20.7 | 5.6 | .4 |
| 766 | 35.2 | 14.351 | 14.347 | 22.6 | 82.2 | 14.356 | 14.348 | 29.8 | 63.9 | 493.8 | 59.1 | 24.5 | 1.2 | -4.9 |
| 767 | 40.9 | 14.354 | 14.349 | 24.8 | 87.9 | 14.359 | 14.351 | 29.9 | 69.7 | 492.2 | 64.8 | 26.3 | 3.4 | 1.8 |
| 768 | 47.1 | 14.354 | 14.348 | 27.7 | 94.1 | 14.359 | 14.350 | 31.8 | 75.8 | 493.1 | 70.9 | 27.7 | -1.4 | 5.8 |
| 769 | 53.3 | 14.354 | 14.347 | 29.1 | 100.3 | 14.359 | 14.350 | 33.2 | 82.0 | 491.7 | 77.2 | 29.5 | -3.8 | 8.7 |
| 770 | 59.0 | 14.358 | 14.349 | 31.3 | 106.0 | 14.359 | 14.350 | 32.0 | 87.8 | 491.1 | 82.9 | 24.9 | -4.8 | 7.1 |
| 771 | 64.9 | 14.358 | 14.348 | 33.3 | 111.9 | 14.362 | 14.353 | 32.3 | 93.6 | 494.5 | 88.7 | 24.2 | -4.4 | 2.1 |
| 772 | 71.1 | 14.358 | 14.349 | 32.8 | 118.1 | 14.362 | 14.353 | 32.7 | 99.9 | 498.9 | 95.0 | 27.5 | 1.2 | -1.3 |
| 773 | 77.3 | 14.361 | 14.353 | 31.1 | 124.3 | 14.362 | 14.354 | 32.0 | 106.1 | 500.2 | 101.2 | 26.9 | 6.1 | -2.1 |
| 774 | 83.4 | 14.358 | 14.350 | 29.4 | 130.4 | 14.365 | 14.358 | 29.8 | 112.1 | 499.1 | 107.3 | 26.9 | 7.0 | -9 |
| 775 | 95.0 | 14.361 | 14.352 | 32.7 | 142.0 | 14.358 | 14.353 | 24.0 | 123.7 | 500.3 | 118.8 | 28.0 | 6.5 | -1.9 |
| 776 | 107.0 | 14.362 | 14.353 | 32.5 | 154.0 | 14.356 | 14.353 | 19.5 | 135.8 | 499.3 | 130.9 | 24.4 | 6.9 | -1.4 |
| 777 | 118.9 | 14.362 | 14.353 | 32.6 | 165.9 | 14.356 | 14.353 | 20.9 | 147.6 | 499.9 | 142.8 | 15.8 | 6.4 | -2.5 |
| 778 | 131.0 | 14.360 | 14.352 | 29.6 | 178.0 | 14.359 | 14.353 | 26.2 | 159.8 | 501.0 | 154.9 | 12.2 | 4.7 | -6.4 |
| 779 | 143.3 | 14.358 | 14.354 | 22.6 | 190.3 | 14.362 | 14.355 | 29.1 | 172.1 | 501.8 | 167.2 | 14.3 | 4.3 | -5.6 |
| 780 | 155.1 | 14.358 | 14.355 | 19.3 | 202.1 | 14.362 | 14.355 | 28.9 | 183.9 | 501.3 | 179.0 | 20.7 | 4.1 | -2.8 |
| 781 | 167.0 | 14.358 | 14.354 | 21.4 | 214.0 | 14.364 | 14.355 | 31.8 | 195.8 | 500.9 | 190.9 | 22.9 | 4.4 | -1.7 |
| 782 | 179.1 | 14.359 | 14.353 | 26.6 | 226.1 | 14.361 | 14.355 | 28.2 | 207.9 | 500.1 | 203.0 | 24.8 | 3.2 | 1.8 |
| 783 | 185.2 | 14.361 | 14.354 | 28.5 | 232.2 | 14.362 | 14.355 | 28.3 | 213.9 | 500.1 | 209.1 | 26.4 | 3.2 | 3.9 |
| 784 | 191.2 | 14.362 | 14.355 | 29.0 | 238.2 | 14.364 | 14.356 | 30.4 | 220.0 | 501.1 | 215.1 | 24.6 | 2.7 | 5.7 |
| 785 | 197.0 | 14.363 | 14.357 | 28.4 | 244.0 | 14.365 | 14.358 | 29.7 | 225.8 | 501.8 | 220.9 | 23.4 | .2 | 5.8 |

TABLE 24.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 786 | 203.0 | 14.364 | 14.357 | 29.0 | 250.0 | 14.364 | 14.358 | 27.8 | 231.7 | 501.7 | 226.8 | 23.4 | -2.6 | 3.2 |
| 787 | 209.1 | 14.365 | 14.357 | 31.9 | 256.1 | 14.363 | 14.357 | 25.6 | 237.8 | 500.8 | 232.9 | 25.1 | -1.2 | .1 |
| 788 | 215.1 | 14.363 | 14.355 | 31.3 | 262.1 | 14.361 | 14.357 | 23.4 | 243.9 | 500.2 | 239.0 | 26.4 | 1.6 | -.3 |
| 789 | 221.4 | 14.363 | 14.356 | 29.3 | 268.4 | 14.361 | 14.357 | 20.7 | 250.1 | 501.3 | 245.3 | 23.7 | 3.6 | -.5 |
| 790 | 226.9 | 14.363 | 14.356 | 28.0 | 273.9 | 14.362 | 14.359 | 19.0 | 255.7 | 502.0 | 250.8 | 22.1 | 4.9 | -.1 |
| 791 | 233.4 | 14.365 | 14.358 | 28.8 | 280.4 | 14.361 | 14.359 | 17.1 | 262.2 | 501.5 | 257.3 | 17.6 | 6.7 | 2.0 |
| 792 | 239.0 | 14.365 | 14.358 | 30.0 | 286.0 | 14.360 | 14.358 | 15.7 | 267.8 | 500.4 | 262.9 | 14.4 | 5.9 | .9 |
| 793 | 245.1 | 14.364 | 14.357 | 29.0 | 292.1 | 14.359 | 14.357 | 14.4 | 273.8 | 500.1 | 269.0 | 12.7 | 7.6 | -.2 |
| 794 | 251.4 | 14.363 | 14.357 | 26.6 | 298.4 | 14.360 | 14.358 | 14.4 | 280.1 | 501.1 | 275.3 | 6.9 | 6.8 | .8 |
| 795 | 257.3 | 14.363 | 14.358 | 23.9 | 304.3 | 14.361 | 14.359 | 15.3 | 286.1 | 502.7 | 281.2 | 5.6 | 8.3 | -3.2 |
| 796 | 243.0 | 14.367 | 14.359 | 29.8 | 290.0 | 14.362 | 14.360 | 14.4 | 271.7 | 503.0 | 266.9 | 11.9 | 6.3 | -0.5 |
| 797 | 225.0 | 14.366 | 14.360 | 28.3 | 272.0 | 14.363 | 14.360 | 19.6 | 253.8 | 501.5 | 248.9 | 20.2 | 4.9 | .2 |
| 798 | 207.3 | 14.367 | 14.359 | 31.4 | 254.3 | 14.367 | 14.361 | 25.9 | 236.1 | 501.7 | 231.2 | 22.9 | -1.5 | .3 |
| 799 | 189.3 | 14.367 | 14.360 | 28.9 | 236.3 | 14.367 | 14.360 | 29.9 | 218.0 | 502.4 | 213.1 | 24.3 | 3.0 | 5.2 |
| 800 | 171.2 | 14.364 | 14.359 | 23.0 | 218.2 | 14.369 | 14.361 | 30.8 | 199.9 | 502.6 | 195.1 | 22.0 | 4.4 | -1.0 |
| 801 | 152.9 | 14.364 | 14.361 | 19.6 | 199.9 | 14.368 | 14.362 | 28.5 | 181.7 | 501.7 | 176.8 | 19.0 | 4.3 | -3.1 |
| 802 | 135.0 | 14.366 | 14.359 | 27.4 | 182.0 | 14.368 | 14.361 | 27.6 | 163.8 | 502.2 | 158.9 | 11.6 | 4.6 | -6.9 |
| 803 | 117.6 | 14.369 | 14.360 | 32.2 | 164.6 | 14.364 | 14.360 | 20.7 | 146.3 | 502.0 | 141.4 | 17.5 | 7.3 | -1.8 |
| 804 | 99.3 | 14.369 | 14.360 | 33.6 | 146.3 | 14.365 | 14.361 | 21.4 | 128.0 | 501.4 | 123.2 | 27.6 | 6.9 | -1.6 |
| 805 | 80.9 | 14.367 | 14.359 | 30.8 | 127.9 | 14.369 | 14.361 | 30.8 | 109.7 | 498.5 | 104.8 | 26.9 | 6.6 | -1.3 |
| 806 | 63.2 | 14.370 | 14.361 | 32.8 | 110.2 | 14.371 | 14.362 | 32.3 | 92.0 | 492.5 | 87.1 | 25.2 | -4.6 | 3.0 |
| 807 | 45.2 | 14.367 | 14.361 | 27.0 | 92.2 | 14.369 | 14.361 | 31.5 | 73.9 | 493.8 | 69.0 | 27.4 | -.3 | 4.1 |
| 808 | 27.1 | 14.364 | 14.361 | 20.2 | 74.1 | 14.372 | 14.362 | 33.0 | 55.9 | 496.2 | 51.0 | 22.7 | 4.9 | -1.7 |
| 809 | 9.1 | 14.363 | 14.362 | 13.3 | 56.1 | 14.370 | 14.362 | 31.1 | 37.9 | 496.8 | 33.0 | 14.6 | 6.9 | -2.9 |
| 810 | 6.5 | 14.363 | 14.362 | 12.4 | 53.5 | 14.370 | 14.362 | 30.4 | 35.2 | 496.5 | 30.4 | 11.9 | 8.1 | -4.2 |

TABLE 25.—DATA LISTING FOR TRAVERSE 2 AT STATION 5—VERTICAL SURVEY
 [Test section data for reading 761; total pressure, 14.378; static pressure, 13.271 psia; total temperature, 497 °R; velocity, 250.7 mph; fan speed, 291.1 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 761 | 5.5 | 14.359 | 14.357 | 13.6 | 51.7 | 14.372 | 14.361 | 29.8 | 32.2 | 491.1 | 28.7 | 11.6 | 4.2 | 5.3 |
| 762 | 11.0 | 14.362 | 14.360 | 15.9 | 57.1 | 14.369 | 14.359 | 31.9 | 37.6 | 492.0 | 34.1 | 14.6 | 3.2 | -5.4 |
| 763 | 17.1 | 14.362 | 14.359 | 19.5 | 63.2 | 14.369 | 14.359 | 34.3 | 43.7 | 492.5 | 40.2 | 23.2 | 3.4 | -7.9 |
| 764 | 23.0 | 14.362 | 14.358 | 22.7 | 69.1 | 14.369 | 14.359 | 35.4 | 49.6 | 492.5 | 46.1 | 22.2 | 3.6 | -3.4 |
| 765 | 29.3 | 14.362 | 14.358 | 22.5 | 75.5 | 14.369 | 14.359 | 34.9 | 56.0 | 491.7 | 52.5 | 24.6 | 2.1 | -7.3 |
| 766 | 34.9 | 14.362 | 14.357 | 25.4 | 81.0 | 14.372 | 14.362 | 35.0 | 61.5 | 492.0 | 58.0 | 28.6 | 5.8 | -2.3 |
| 767 | 41.0 | 14.365 | 14.359 | 27.3 | 87.1 | 14.372 | 14.362 | 35.0 | 67.6 | 492.1 | 64.1 | 29.3 | 6.4 | -3.5 |
| 768 | 46.8 | 14.368 | 14.362 | 27.6 | 93.0 | 14.369 | 14.359 | 34.6 | 73.5 | 492.2 | 70.0 | 29.2 | 6.4 | -1.4 |
| 769 | 53.3 | 14.365 | 14.357 | 30.4 | 99.4 | 14.369 | 14.360 | 33.8 | 79.9 | 492.0 | 76.4 | 32.8 | 6.2 | -2.0 |
| 770 | 59.1 | 14.368 | 14.359 | 33.1 | 105.2 | 14.369 | 14.360 | 32.3 | 85.7 | 493.5 | 82.2 | 31.6 | 6.4 | -2.2 |
| 771 | 65.5 | 14.368 | 14.358 | 34.6 | 111.7 | 14.369 | 14.361 | 31.0 | 92.2 | 496.3 | 88.7 | 33.0 | 6.3 | -0.9 |
| 772 | 71.1 | 14.371 | 14.361 | 35.6 | 117.2 | 14.360 | 14.354 | 27.5 | 97.7 | 499.2 | 94.2 | 32.4 | 5.8 | -9 |
| 773 | 77.0 | 14.365 | 14.355 | 35.1 | 123.1 | 14.363 | 14.358 | 25.2 | 103.6 | 500.2 | 100.1 | 30.9 | 6.2 | -8 |
| 774 | 83.0 | 14.371 | 14.361 | 34.9 | 129.1 | 14.363 | 14.359 | 22.3 | 109.6 | 498.1 | 106.1 | 28.7 | 6.1 | .4 |
| 775 | 95.0 | 14.372 | 14.362 | 35.0 | 141.1 | 14.363 | 14.360 | 18.4 | 121.6 | 495.4 | 118.1 | 22.1 | 5.9 | -2.1 |
| 776 | 107.3 | 14.371 | 14.363 | 31.9 | 153.5 | 14.366 | 14.363 | 18.6 | 134.0 | 493.8 | 130.5 | 15.4 | 6.2 | -1.3 |
| 777 | 119.1 | 14.367 | 14.361 | 27.3 | 165.2 | 14.366 | 14.362 | 22.6 | 145.7 | 495.6 | 142.2 | 11.8 | 4.5 | 0.0 |
| 778 | 131.0 | 14.365 | 14.361 | 21.9 | 177.1 | 14.366 | 14.361 | 25.9 | 157.6 | 498.2 | 154.1 | 12.0 | 3.2 | -1.4 |
| 779 | 143.0 | 14.363 | 14.361 | 18.6 | 189.2 | 14.366 | 14.359 | 28.3 | 169.7 | 499.8 | 166.2 | 16.9 | 2.1 | -1.2 |
| 780 | 154.6 | 14.365 | 14.362 | 19.6 | 200.7 | 14.370 | 14.362 | 30.9 | 181.2 | 499.6 | 177.7 | 21.8 | 2.1 | 0.0 |
| 781 | 167.0 | 14.367 | 14.363 | 23.4 | 213.2 | 14.373 | 14.363 | 32.9 | 193.7 | 499.4 | 190.2 | 25.1 | 2.4 | -1.6 |
| 782 | 179.3 | 14.369 | 14.363 | 26.8 | 225.4 | 14.373 | 14.364 | 32.4 | 205.9 | 499.5 | 202.4 | 29.0 | 2.6 | -1.2 |
| 783 | 185.3 | 14.369 | 14.362 | 27.9 | 231.5 | 14.373 | 14.364 | 31.6 | 212.0 | 499.6 | 208.5 | 29.8 | 2.7 | -8 |
| 784 | 191.1 | 14.371 | 14.364 | 29.1 | 237.3 | 14.370 | 14.362 | 31.3 | 217.8 | 501.1 | 214.3 | 30.2 | 2.5 | -6 |
| 785 | 197.1 | 14.371 | 14.363 | 30.3 | 243.2 | 14.369 | 14.362 | 30.1 | 223.7 | 501.9 | 220.2 | 29.5 | 3.4 | -6 |

TABLE 25.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg |
| 786 | 203.0 | 14.372 | 14.363 | 32.1 | 249.2 | 14.370 | 14.363 | 28.8 | 229.7 | 501.8 | 226.2 | 29.0 | -0.3 |
| 787 | 209.1 | 14.374 | 14.365 | 33.2 | 255.2 | 14.372 | 14.365 | 27.8 | 235.7 | 500.4 | 232.2 | 28.4 | -8 |
| 788 | 215.4 | 14.373 | 14.363 | 33.4 | 261.5 | 14.371 | 14.365 | 26.7 | 242.0 | 499.8 | 238.5 | 27.1 | -1.3 |
| 789 | 221.7 | 14.372 | 14.363 | 32.6 | 267.8 | 14.367 | 14.362 | 23.4 | 248.3 | 501.1 | 244.8 | 25.4 | -2.1 |
| 790 | 227.3 | 14.372 | 14.364 | 32.4 | 273.4 | 14.366 | 14.362 | 22.1 | 253.9 | 501.9 | 250.4 | 25.5 | .1 |
| 791 | 232.7 | 14.374 | 14.366 | 31.8 | 278.8 | 14.369 | 14.366 | 19.7 | 259.3 | 501.2 | 255.8 | 22.9 | 4.5 |
| 792 | 239.0 | 14.374 | 14.366 | 30.9 | 285.1 | 14.368 | 14.366 | 15.6 | 265.6 | 500.2 | 262.1 | 20.2 | 5.4 |
| 793 | 245.0 | 14.373 | 14.365 | 29.9 | 291.1 | 14.367 | 14.365 | 14.5 | 271.6 | 499.8 | 268.1 | 18.7 | .9 |
| 794 | 250.9 | 14.371 | 14.364 | 28.7 | 297.0 | 14.364 | 14.363 | 12.1 | 277.5 | 501.0 | 274.0 | 15.0 | -7 |
| 795 | 255.2 | 14.370 | 14.364 | 27.4 | 301.3 | 14.361 | 14.361 | 9.6 | 281.8 | 502.8 | 278.3 | 9.1 | .2 |
| 796 | 243.1 | 14.374 | 14.366 | 30.4 | 289.2 | 14.365 | 14.364 | 14.5 | 269.7 | 503.1 | 266.2 | 18.2 | 5.7 |
| 797 | 225.9 | 14.377 | 14.368 | 32.2 | 272.0 | 14.373 | 14.368 | 22.9 | 252.5 | 501.3 | 249.0 | 25.3 | -9 |
| 798 | 207.3 | 14.377 | 14.368 | 32.9 | 253.5 | 14.374 | 14.367 | 28.5 | 234.0 | 501.7 | 230.5 | 28.3 | -5 |
| 799 | 189.1 | 14.374 | 14.367 | 28.8 | 235.3 | 14.375 | 14.367 | 31.4 | 215.8 | 502.3 | 212.3 | 30.6 | -5 |
| 800 | 171.4 | 14.372 | 14.367 | 25.0 | 217.6 | 14.375 | 14.366 | 32.9 | 198.1 | 502.0 | 194.6 | 26.4 | -1.6 |
| 801 | 153.6 | 14.371 | 14.368 | 19.4 | 199.7 | 14.375 | 14.368 | 30.5 | 180.2 | 500.2 | 176.7 | 22.1 | -0.4 |
| 802 | 134.9 | 14.370 | 14.367 | 20.2 | 181.0 | 14.373 | 14.366 | 26.9 | 161.5 | 499.8 | 158.0 | 14.5 | -1.2 |
| 803 | 117.3 | 14.374 | 14.367 | 28.0 | 163.4 | 14.372 | 14.368 | 21.9 | 143.9 | 497.7 | 140.4 | 12.8 | -2 |
| 804 | 99.4 | 14.378 | 14.369 | 34.1 | 145.5 | 14.370 | 14.367 | 18.0 | 126.0 | 496.2 | 122.5 | 19.7 | 5.9 |
| 805 | 81.1 | 14.379 | 14.369 | 35.1 | 127.2 | 14.372 | 14.368 | 23.4 | 107.7 | 499.4 | 104.2 | 29.8 | -1.9 |
| 806 | 63.4 | 14.378 | 14.369 | 34.0 | 109.5 | 14.376 | 14.368 | 30.8 | 90.0 | 496.4 | 86.5 | 32.4 | -1.7 |
| 807 | 45.2 | 14.376 | 14.369 | 29.4 | 91.3 | 14.379 | 14.369 | 35.1 | 71.8 | 494.4 | 68.3 | 33.1 | -2.3 |
| 808 | 26.9 | 14.373 | 14.369 | 21.7 | 73.0 | 14.380 | 14.369 | 35.3 | 53.5 | 494.9 | 50.0 | 24.4 | -3.5 |
| 809 | 9.3 | 14.371 | 14.370 | 14.1 | 55.4 | 14.378 | 14.369 | 32.2 | 35.9 | 495.2 | 32.4 | 16.5 | -2.6 |
| 810 | 5.7 | 14.370 | 14.369 | 13.0 | 51.8 | 14.375 | 14.367 | 30.9 | 32.3 | 495.2 | 28.8 | 16.3 | -1.8 |

TABLE 26.—DATA LISTING FOR TRAVERSE 1 AT STATION 5—VERTICAL SURVEY
[Test section data for reading 1050: total pressure, 14.263; static pressure, 13.158 psia; total temperature, 497 °R; velocity, 251.7 mph; fan speed, 292.4 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1050 | 6.8 | 14.245 | 14.243 | 16.7 | 53.8 | 14.252 | 14.244 | 31.2 | 35.6 | 489.8 | 30.7 | 18.4 | 6.4 | -1.0 |
| 1051 | 11.1 | 14.246 | 14.243 | 18.1 | 58.1 | 14.253 | 14.245 | 31.7 | 39.9 | 489.7 | 35.0 | 18.7 | 5.4 | -2.5 |
| 1052 | 17.0 | 14.246 | 14.242 | 20.5 | 64.0 | 14.253 | 14.244 | 32.0 | 45.8 | 489.8 | 40.9 | 21.3 | 5.7 | -3 |
| 1053 | 23.1 | 14.247 | 14.243 | 22.9 | 70.1 | 14.253 | 14.245 | 32.1 | 51.9 | 489.5 | 47.0 | 23.1 | 6.6 | -1.6 |
| 1054 | 29.0 | 14.248 | 14.243 | 24.6 | 76.0 | 14.253 | 14.245 | 31.4 | 57.7 | 489.3 | 52.9 | 24.3 | 6.0 | -4 |
| 1055 | 35.2 | 14.249 | 14.243 | 26.8 | 82.2 | 14.253 | 14.244 | 31.8 | 63.9 | 488.9 | 59.1 | 24.9 | 7.3 | -1.3 |
| 1056 | 40.8 | 14.251 | 14.244 | 28.2 | 87.8 | 14.254 | 14.245 | 32.1 | 69.6 | 488.7 | 64.7 | 25.4 | 8.2 | -5 |
| 1057 | 47.0 | 14.251 | 14.244 | 30.2 | 94.0 | 14.254 | 14.246 | 32.4 | 75.8 | 488.7 | 70.9 | 25.5 | 8.3 | -2 |
| 1058 | 53.1 | 14.252 | 14.244 | 31.0 | 100.1 | 14.253 | 14.245 | 31.8 | 81.9 | 489.0 | 77.0 | 25.2 | 8.4 | -4 |
| 1059 | 59.2 | 14.252 | 14.244 | 31.7 | 106.2 | 14.253 | 14.245 | 30.9 | 87.9 | 489.9 | 83.1 | 25.4 | 8.2 | .6 |
| 1060 | 65.0 | 14.253 | 14.244 | 31.8 | 112.0 | 14.253 | 14.246 | 29.4 | 93.8 | 491.6 | 88.9 | 25.7 | 8.1 | 0.3 |
| 1061 | 71.0 | 14.252 | 14.243 | 31.5 | 118.0 | 14.252 | 14.246 | 27.8 | 99.8 | 493.2 | 94.9 | 25.7 | 8.9 | .5 |
| 1062 | 78.9 | 14.252 | 14.244 | 31.2 | 125.9 | 14.251 | 14.245 | 25.7 | 107.6 | 494.7 | 102.8 | 24.2 | 8.8 | .8 |
| 1063 | 83.0 | 14.253 | 14.244 | 31.4 | 130.0 | 14.250 | 14.245 | 24.7 | 111.7 | 495.1 | 106.8 | 23.0 | 8.7 | .9 |
| 1064 | 95.1 | 14.254 | 14.245 | 32.5 | 142.1 | 14.249 | 14.245 | 22.4 | 123.8 | 495.7 | 119.0 | 20.0 | 9.5 | .8 |
| 1065 | 106.8 | 14.252 | 14.245 | 30.4 | 153.8 | 14.250 | 14.246 | 21.9 | 135.6 | 495.7 | 130.7 | 15.2 | 9.0 | 2.8 |
| 1066 | 118.9 | 14.251 | 14.245 | 26.9 | 165.9 | 14.249 | 14.246 | 20.9 | 147.6 | 495.4 | 142.8 | 12.7 | 8.8 | 2.9 |
| 1067 | 131.4 | 14.250 | 14.245 | 23.7 | 178.4 | 14.250 | 14.246 | 22.1 | 160.2 | 495.1 | 155.3 | 12.6 | 9.0 | 1.7 |
| 1068 | 142.9 | 14.248 | 14.244 | 21.9 | 189.9 | 14.252 | 14.246 | 26.3 | 171.6 | 495.2 | 166.7 | 12.5 | 8.6 | 1.4 |
| 1069 | 155.2 | 14.249 | 14.245 | 21.3 | 202.2 | 14.254 | 14.247 | 28.6 | 184.0 | 495.4 | 179.1 | 13.8 | 7.2 | 1.1 |
| 1070 | 167.4 | 14.248 | 14.244 | 20.5 | 214.4 | 14.255 | 14.248 | 30.1 | 196.1 | 496.1 | 191.3 | 18.1 | 6.3 | 0.9 |
| 1071 | 179.3 | 14.249 | 14.245 | 22.2 | 226.3 | 14.256 | 14.248 | 30.5 | 208.0 | 496.7 | 203.1 | 21.1 | 7.6 | -.1 |
| 1072 | 184.8 | 14.251 | 14.246 | 24.4 | 231.8 | 14.256 | 14.249 | 30.3 | 213.6 | 496.8 | 208.7 | 22.1 | 7.7 | .6 |
| 1073 | 190.8 | 14.251 | 14.245 | 26.5 | 237.8 | 14.256 | 14.249 | 29.4 | 219.6 | 496.7 | 214.7 | 23.8 | 7.2 | .7 |
| 1074 | 197.4 | 14.252 | 14.245 | 28.0 | 244.4 | 14.255 | 14.249 | 28.1 | 226.2 | 496.4 | 221.3 | 24.8 | 7.7 | .9 |

TABLE 26.—Concluded.

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | | Wind anemometer | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1075 | 203.0 | 14.252 | 14.245 | 28.6 | 250.0 | 14.256 | 14.249 | 26.9 | 231.7 | 496.4 | 226.8 | 24.5 | 7.3 | 0.7 |
| 1076 | 208.9 | 14.252 | 14.245 | 29.3 | 255.9 | 14.254 | 14.249 | 25.8 | 237.7 | 496.9 | 232.8 | 23.8 | 7.0 | .1 |
| 1077 | 215.3 | 14.254 | 14.247 | 29.8 | 262.3 | 14.255 | 14.250 | 24.2 | 244.1 | 497.6 | 239.2 | 22.3 | 7.1 | .2 |
| 1078 | 221.6 | 14.255 | 14.247 | 30.5 | 268.6 | 14.256 | 14.251 | 23.4 | 250.3 | 498.1 | 245.4 | 21.4 | 7.8 | .5 |
| 1079 | 227.0 | 14.256 | 14.248 | 30.3 | 274.0 | 14.255 | 14.251 | 22.4 | 255.7 | 498.2 | 250.8 | 20.7 | 8.2 | .7 |
| 1080 | 233.2 | 14.256 | 14.249 | 29.6 | 280.2 | 14.256 | 14.252 | 21.1 | 261.9 | 498.4 | 257.0 | 18.8 | 8.0 | 1.5 |
| 1081 | 238.8 | 14.256 | 14.249 | 28.7 | 285.8 | 14.255 | 14.252 | 20.0 | 267.5 | 498.4 | 262.6 | 16.7 | 8.2 | 1.5 |
| 1082 | 244.7 | 14.256 | 14.250 | 27.6 | 291.7 | 14.256 | 14.253 | 18.9 | 273.4 | 498.5 | 268.5 | 15.7 | 9.0 | 2.3 |
| 1083 | 250.7 | 14.256 | 14.251 | 26.5 | 297.7 | 14.256 | 14.253 | 17.7 | 279.5 | 498.6 | 274.6 | 14.6 | 10.0 | 1.6 |
| 1084 | 257.0 | 14.256 | 14.251 | 25.3 | 304.0 | 14.256 | 14.254 | 15.0 | 285.7 | 498.7 | 280.9 | 12.2 | 10.0 | 3.7 |
| 1085 | 260.7 | 14.256 | 14.251 | 24.4 | 307.7 | 14.255 | 14.254 | 13.9 | 289.4 | 498.7 | 284.5 | 12.3 | 10.2 | 2.2 |
| 1086 | 243.3 | 14.258 | 14.252 | 27.6 | 290.3 | 14.257 | 14.254 | 18.5 | 272.1 | 498.7 | 267.2 | 15.9 | 8.9 | 2.3 |
| 1087 | 224.8 | 14.260 | 14.253 | 30.3 | 271.8 | 14.258 | 14.254 | 23.0 | 253.6 | 498.6 | 248.7 | 20.8 | 7.4 | .9 |
| 1088 | 207.0 | 14.261 | 14.254 | 29.1 | 254.0 | 14.261 | 14.255 | 26.1 | 235.8 | 498.4 | 230.9 | 24.2 | 7.2 | .9 |
| 1089 | 188.9 | 14.260 | 14.254 | 25.5 | 235.9 | 14.263 | 14.255 | 29.7 | 217.7 | 498.1 | 212.8 | 23.6 | 7.1 | .7 |
| 1090 | 171.2 | 14.258 | 14.254 | 20.3 | 218.2 | 14.264 | 14.256 | 30.5 | 200.0 | 497.3 | 195.1 | 19.3 | 7.0 | 0.7 |
| 1091 | 153.2 | 14.259 | 14.255 | 21.5 | 200.2 | 14.262 | 14.256 | 28.0 | 182.0 | 496.1 | 177.1 | 13.2 | 7.9 | 1.4 |
| 1092 | 135.1 | 14.259 | 14.254 | 22.8 | 182.1 | 14.261 | 14.257 | 23.3 | 163.8 | 495.7 | 159.0 | 12.4 | 9.1 | 1.5 |
| 1093 | 116.0 | 14.262 | 14.255 | 27.8 | 163.0 | 14.261 | 14.258 | 21.3 | 144.7 | 496.2 | 139.8 | 13.7 | 8.9 | 2.6 |
| 1094 | 99.0 | 14.264 | 14.256 | 31.7 | 146.0 | 14.262 | 14.258 | 21.9 | 127.8 | 496.8 | 122.9 | 18.1 | 9.8 | 2.2 |
| 1095 | 81.1 | 14.264 | 14.256 | 31.2 | 128.1 | 14.263 | 14.258 | 24.5 | 109.8 | 496.1 | 105.0 | 23.6 | 9.0 | 1.0 |
| 1096 | 63.3 | 14.265 | 14.256 | 31.8 | 110.3 | 14.265 | 14.257 | 29.7 | 92.1 | 492.1 | 87.2 | 25.8 | 7.9 | .3 |
| 1097 | 44.8 | 14.264 | 14.257 | 29.7 | 91.8 | 14.267 | 14.258 | 32.4 | 73.6 | 489.3 | 68.7 | 25.7 | 7.8 | .3 |
| 1098 | 27.3 | 14.262 | 14.257 | 24.4 | 74.3 | 14.265 | 14.257 | 31.3 | 56.0 | 489.6 | 51.2 | 24.2 | 5.6 | -1.8 |
| 1099 | 8.9 | 14.260 | 14.257 | 17.6 | 55.9 | 14.267 | 14.259 | 31.3 | 37.7 | 490.1 | 32.8 | 20.2 | 5.8 | -2.8 |
| 1100 | 7.4 | 14.259 | 14.256 | 16.2 | 54.4 | 14.266 | 14.257 | 31.4 | 36.1 | 490.1 | 31.2 | 21.0 | 2.4 | -1.7 |

TABLE 27.—DATA LISTING FOR TRAVERSE 1 AT STATION 5—HORIZONTAL SURVEY NEAR FLOOR
[Test section data for reading 1265; total pressure, 14.209; static pressure, 12.148 psia; total temperature, 500 °R; velocity, 349.9 mph; fan speed, 395.3 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1265 | 5.4 | 14.194 | 14.188 | 26.5 | 52.4 | 14.198 | 14.189 | 32.4 | 34.2 | 504.7 | 29.3 | 13.5 | 1.7 | -0.8 |
| 1266 | 14.9 | 14.192 | 14.188 | 21.3 | 61.9 | 14.201 | 14.189 | 38.5 | 43.7 | 504.2 | 38.8 | 17.1 | .4 | -1.1 |
| 1267 | 24.9 | 14.192 | 14.188 | 21.0 | 71.9 | 14.204 | 14.189 | 43.0 | 53.6 | 495.6 | 48.8 | 25.2 | .3 | -5.3 |
| 1268 | 35.0 | 14.193 | 14.189 | 20.9 | 82.0 | 14.204 | 14.188 | 43.7 | 63.8 | 494.1 | 58.9 | 32.3 | 3.6 | 1.2 |
| 1269 | 45.4 | 14.195 | 14.188 | 28.6 | 92.4 | 14.205 | 14.189 | 44.3 | 74.2 | 496.1 | 69.3 | 37.4 | 3.9 | -4.3 |
| 1270 | 54.9 | 14.198 | 14.189 | 34.1 | 101.9 | 14.205 | 14.189 | 44.1 | 83.7 | 497.4 | 78.8 | 36.7 | -1.1 | -3.4 |
| 1271 | 65.4 | 14.201 | 14.188 | 39.6 | 112.4 | 14.205 | 14.188 | 45.8 | 94.2 | 499.4 | 89.3 | 38.6 | -4.8 | 8.0 |
| 1272 | 75.2 | 14.204 | 14.188 | 44.3 | 122.2 | 14.207 | 14.189 | 46.9 | 104.0 | 497.3 | 99.1 | 39.3 | -2.8 | 10.7 |
| 1273 | 85.1 | 14.203 | 14.188 | 42.3 | 132.1 | 14.208 | 14.189 | 47.4 | 113.8 | 499.2 | 109.0 | 37.3 | 3.2 | .6 |
| 1274 | 95.3 | 14.204 | 14.188 | 44.8 | 142.3 | 14.210 | 14.190 | 49.1 | 124.0 | 499.7 | 119.1 | 40.9 | 3.3 | -1.8 |
| 1275 | 104.9 | 14.202 | 14.187 | 41.7 | 151.9 | 14.209 | 14.190 | 47.1 | 133.7 | 494.2 | 128.8 | 40.0 | 3.6 | 1.7 |
| 1276 | 114.9 | 14.208 | 14.189 | 47.0 | 161.9 | 14.206 | 14.189 | 44.4 | 143.6 | 492.5 | 138.8 | 43.6 | 2.8 | .7 |
| 1277 | 124.8 | 14.207 | 14.190 | 46.0 | 171.8 | 14.206 | 14.190 | 43.3 | 153.6 | 495.0 | 148.7 | 42.4 | 3.6 | -4 |
| 1278 | 134.8 | 14.209 | 14.190 | 47.9 | 181.8 | 14.209 | 14.190 | 47.5 | 163.5 | 493.8 | 158.6 | 39.5 | 2.7 | 1.2 |
| 1279 | 145.2 | 14.211 | 14.190 | 49.5 | 192.2 | 14.208 | 14.190 | 45.6 | 174.0 | 493.8 | 169.1 | 37.2 | 2.2 | 1.6 |
| 1280 | 154.9 | 14.207 | 14.189 | 46.6 | 201.9 | 14.208 | 14.189 | 47.9 | 183.6 | 494.3 | 178.7 | 42.3 | 1.8 | 1.9 |
| 1281 | 164.9 | 14.205 | 14.190 | 43.0 | 211.9 | 14.211 | 14.191 | 48.8 | 193.7 | 495.3 | 188.8 | 40.6 | 2.2 | 1.9 |
| 1282 | 174.8 | 14.207 | 14.190 | 44.7 | 221.8 | 14.209 | 14.191 | 46.6 | 203.6 | 494.7 | 198.7 | 42.2 | 1.8 | 1.6 |
| 1283 | 184.7 | 14.209 | 14.190 | 46.8 | 231.7 | 14.208 | 14.191 | 45.5 | 213.5 | 494.3 | 208.6 | 42.5 | 2.1 | .6 |
| 1284 | 195.1 | 14.208 | 14.191 | 46.1 | 242.1 | 14.208 | 14.192 | 44.4 | 223.9 | 494.3 | 219.0 | 41.4 | 1.9 | .2 |
| 1285 | 205.4 | 14.210 | 14.191 | 48.7 | 252.4 | 14.207 | 14.191 | 43.7 | 234.1 | 494.5 | 229.3 | 40.4 | 1.9 | 1.5 |
| 1286 | 215.1 | 14.210 | 14.191 | 47.8 | 262.1 | 14.208 | 14.192 | 43.1 | 243.8 | 493.0 | 239.0 | 39.3 | 1.7 | 2.0 |
| 1287 | 224.8 | 14.209 | 14.191 | 46.1 | 271.8 | 14.207 | 14.192 | 42.3 | 253.6 | 491.6 | 248.7 | 38.8 | 1.5 | 1.0 |
| 1288 | 235.2 | 14.208 | 14.191 | 44.4 | 282.2 | 14.207 | 14.192 | 41.6 | 263.9 | 490.2 | 259.1 | 38.6 | .9 | 1.1 |
| 1289 | 244.8 | 14.207 | 14.191 | 43.4 | 291.8 | 14.206 | 14.192 | 40.8 | 273.6 | 489.8 | 268.7 | 37.2 | 1.0 | -.1 |

TABLE 27.—Concluded.

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | | Wind anemometer | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1290 | 255.4 | 14.207 | 14.192 | 43.2 | 302.4 | 14.206 | 14.193 | 39.3 | 284.2 | 490.1 | 279.3 | 35.5 | 0.9 | -0.3 |
| 1291 | 264.8 | 14.207 | 14.192 | 42.7 | 311.8 | 14.205 | 14.193 | 38.6 | 293.6 | 490.1 | 288.7 | 34.8 | .8 | -6 |
| 1292 | 275.3 | 14.207 | 14.192 | 41.4 | 322.3 | 14.206 | 14.194 | 37.4 | 304.1 | 491.2 | 299.2 | 33.4 | 1.4 | -1.3 |
| 1293 | 284.9 | 14.207 | 14.193 | 40.8 | 331.9 | 14.205 | 14.194 | 35.5 | 313.7 | 491.1 | 308.8 | 32.4 | 1.5 | -1.5 |
| 1294 | 290.1 | 14.207 | 14.193 | 40.5 | 337.1 | 14.204 | 14.195 | 34.2 | 318.9 | 490.0 | 314.0 | 31.9 | 2.2 | -2.6 |
| 1295 | 270.4 | 14.209 | 14.194 | 42.4 | 317.4 | 14.206 | 14.194 | 37.5 | 299.1 | 490.5 | 294.2 | 34.3 | 0.8 | -0.5 |
| 1296 | 249.9 | 14.208 | 14.193 | 42.9 | 296.9 | 14.206 | 14.193 | 39.6 | 278.7 | 490.1 | 273.8 | 36.0 | 7 | .5 |
| 1297 | 230.4 | 14.212 | 14.194 | 45.7 | 277.4 | 14.209 | 14.194 | 41.6 | 259.2 | 490.8 | 254.3 | 39.0 | 1.2 | 2.0 |
| 1298 | 209.8 | 14.214 | 14.194 | 49.3 | 256.8 | 14.211 | 14.195 | 43.7 | 238.6 | 493.8 | 233.7 | 39.8 | 1.9 | 2.4 |
| 1299 | 190.3 | 14.211 | 14.194 | 45.5 | 237.3 | 14.211 | 14.195 | 44.8 | 219.1 | 494.3 | 214.2 | 43.0 | 2.1 | 1.2 |
| 1300 | 170.0 | 14.210 | 14.194 | 43.5 | 217.0 | 14.213 | 14.194 | 47.4 | 198.7 | 495.0 | 193.9 | 41.1 | 2.6 | 1.9 |
| 1301 | 150.1 | 14.213 | 14.194 | 48.3 | 197.1 | 14.212 | 14.194 | 46.2 | 178.8 | 493.9 | 173.9 | 39.4 | 2.1 | 2.2 |
| 1302 | 130.0 | 14.211 | 14.194 | 45.9 | 177.0 | 14.212 | 14.194 | 46.0 | 158.8 | 494.3 | 153.9 | 41.9 | 3.3 | -2 |
| 1303 | 110.0 | 14.207 | 14.192 | 43.2 | 157.0 | 14.212 | 14.193 | 46.8 | 138.8 | 494.1 | 133.9 | 42.5 | 2.7 | .8 |
| 1304 | 90.1 | 14.208 | 14.193 | 42.7 | 137.1 | 14.213 | 14.193 | 49.0 | 118.9 | 500.6 | 114.0 | 42.6 | 3.3 | -3.1 |
| 1305 | 69.9 | 14.207 | 14.193 | 40.8 | 116.9 | 14.212 | 14.193 | 48.0 | 98.6 | 497.9 | 93.8 | 40.0 | -4.2 | 8.5 |
| 1306 | 50.4 | 14.198 | 14.192 | 27.0 | 97.4 | 14.209 | 14.192 | 45.6 | 79.2 | 497.4 | 74.3 | 38.5 | .4 | -5.1 |
| 1307 | 30.1 | 14.196 | 14.192 | 20.4 | 77.1 | 14.211 | 14.194 | 45.0 | 58.9 | 494.7 | 54.0 | 28.4 | 1.6 | 5.2 |
| 1308 | 10.5 | 14.197 | 14.192 | 25.8 | 57.5 | 14.205 | 14.193 | 37.5 | 39.3 | 503.2 | 34.4 | 13.8 | 1.5 | 0.0 |

TABLE 28—DATA LISTING FOR TRAVERSE 2 AT STATION 5—HORIZONTAL SURVEY AT CENTERLINE
 [Test section data for reading 1265: total pressure, 14.209; static pressure, 12.148 psia; total temperature, 500 °R; velocity, 349.9 mph; fan speed, 395.3 rpm.]

| Reading number | Probe one | | | | | | Probe two | | | | | | Thermocouple | | | | Wind anemometer | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|---------------|------------|----------|--|-----------------|--|--|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Position, in. | Pitch, deg | Yaw, deg | | | | |
| 1265 | 5.1 | 14.194 | 14.190 | 22.2 | 51.3 | 14.195 | 14.189 | 26.9 | 31.8 | 504.7 | 28.3 | 16.2 | -0.2 | 1.4 | | | | | |
| 1266 | 15.0 | 14.193 | 14.189 | 21.2 | 61.2 | 14.200 | 14.190 | 35.1 | 41.7 | 504.9 | 38.2 | 20.7 | 2.0 | -.5 | | | | | |
| 1267 | 24.9 | 14.193 | 14.190 | 20.0 | 71.0 | 14.197 | 14.189 | 31.6 | 51.5 | 504.9 | 48.0 | 22.2 | 3.9 | -.5 | | | | | |
| 1268 | 35.4 | 14.195 | 14.191 | 23.5 | 81.5 | 14.195 | 14.190 | 25.1 | 62.0 | 504.4 | 58.5 | 29.7 | 3.3 | -.9 | | | | | |
| 1269 | 45.4 | 14.197 | 14.191 | 25.0 | 91.5 | 14.195 | 14.190 | 25.5 | 72.0 | 503.2 | 68.5 | 26.9 | 4.5 | 1.6 | | | | | |
| 1270 | 54.8 | 14.199 | 14.191 | 31.3 | 100.9 | 14.196 | 14.190 | 25.1 | 81.4 | 501.3 | 77.9 | 19.8 | 5.7 | 6.1 | | | | | |
| 1271 | 65.0 | 14.200 | 14.191 | 34.4 | 111.1 | 14.196 | 14.191 | 23.7 | 91.6 | 500.3 | 88.1 | 20.0 | 4.3 | 5.2 | | | | | |
| 1272 | 75.1 | 14.196 | 14.190 | 27.6 | 121.2 | 14.196 | 14.191 | 23.7 | 101.7 | 499.5 | 98.2 | 20.7 | 5.0 | 3.2 | | | | | |
| 1273 | 85.1 | 14.196 | 14.191 | 25.1 | 131.3 | 14.197 | 14.192 | 25.3 | 111.8 | 498.2 | 108.3 | 19.2 | 4.1 | 2.4 | | | | | |
| 1274 | 95.4 | 14.197 | 14.191 | 25.6 | 141.5 | 14.197 | 14.191 | 25.6 | 122.0 | 496.6 | 118.5 | 18.4 | 1.6 | 2.0 | | | | | |
| 1275 | 105.0 | 14.196 | 14.191 | 25.1 | 151.1 | 14.198 | 14.193 | 24.1 | 131.6 | 496.0 | 128.1 | 20.7 | 0.4 | 1.6 | | | | | |
| 1276 | 115.1 | 14.196 | 14.191 | 23.6 | 161.2 | 14.196 | 14.192 | 22.0 | 141.7 | 496.3 | 138.2 | 21.4 | .2 | .4 | | | | | |
| 1277 | 125.0 | 14.196 | 14.191 | 24.7 | 171.1 | 14.197 | 14.192 | 24.5 | 151.6 | 495.9 | 148.1 | 20.7 | .8 | .1 | | | | | |
| 1278 | 134.9 | 14.197 | 14.191 | 25.8 | 181.0 | 14.196 | 14.191 | 24.4 | 161.5 | 494.8 | 158.0 | 17.4 | -.5 | .8 | | | | | |
| 1279 | 145.0 | 14.196 | 14.190 | 26.2 | 191.1 | 14.197 | 14.192 | 24.0 | 171.6 | 493.9 | 168.1 | 20.1 | -.3 | -.1 | | | | | |
| 1280 | 154.9 | 14.196 | 14.192 | 23.0 | 201.0 | 14.197 | 14.192 | 24.8 | 181.5 | 493.3 | 178.0 | 21.0 | -2.1 | -1.1 | | | | | |
| 1281 | 165.0 | 14.195 | 14.191 | 23.5 | 211.1 | 14.198 | 14.193 | 25.7 | 191.6 | 492.8 | 188.1 | 17.5 | -.7 | .9 | | | | | |
| 1282 | 174.9 | 14.197 | 14.192 | 25.2 | 221.0 | 14.198 | 14.193 | 26.1 | 201.5 | 492.5 | 198.0 | 17.9 | -2.0 | 2.6 | | | | | |
| 1283 | 185.2 | 14.195 | 14.191 | 24.1 | 231.3 | 14.199 | 14.193 | 27.9 | 211.8 | 492.5 | 208.3 | 19.7 | -2.9 | 1.7 | | | | | |
| 1284 | 194.7 | 14.196 | 14.191 | 24.4 | 240.8 | 14.202 | 14.194 | 32.0 | 221.3 | 492.7 | 217.8 | 20.8 | -3.9 | 2.1 | | | | | |
| 1285 | 205.4 | 14.196 | 14.191 | 25.5 | 251.5 | 14.203 | 14.194 | 34.3 | 232.0 | 493.5 | 228.5 | 22.5 | -4.4 | 1.5 | | | | | |
| 1286 | 214.8 | 14.197 | 14.192 | 26.2 | 261.0 | 14.202 | 14.194 | 30.9 | 241.4 | 494.3 | 237.9 | 27.6 | -3.2 | -.6 | | | | | |
| 1287 | 225.0 | 14.198 | 14.192 | 26.9 | 271.1 | 14.201 | 14.194 | 27.4 | 251.6 | 494.9 | 248.1 | 31.4 | -2.8 | -2.6 | | | | | |
| 1288 | 235.1 | 14.199 | 14.192 | 30.1 | 281.2 | 14.202 | 14.195 | 28.1 | 261.7 | 495.4 | 258.2 | 27.3 | -2.6 | -1.4 | | | | | |
| 1289 | 245.3 | 14.203 | 14.193 | 34.4 | 291.5 | 14.204 | 14.195 | 32.3 | 272.0 | 495.7 | 268.5 | 21.2 | -3.9 | 0.0 | | | | | |

TABLE 28.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1290 | 255.0 | 14.203 | 14.194 | 33.6 | 301.1 | 14.204 | 14.195 | 32.0 | 281.6 | 496.4 | 278.1 | 21.6 | -5.4 | 0.9 |
| 1291 | 265.2 | 14.201 | 14.194 | 29.4 | 311.3 | 14.204 | 14.195 | 31.8 | 291.8 | 497.0 | 288.3 | 26.4 | -5.3 | -3 |
| 1292 | 275.4 | 14.201 | 14.195 | 27.3 | 321.5 | 14.204 | 14.196 | 31.1 | 302.0 | 496.4 | 298.5 | 28.3 | -5.2 | -4 |
| 1293 | 285.1 | 14.203 | 14.195 | 30.7 | 331.2 | 14.205 | 14.197 | 30.8 | 311.7 | 496.1 | 308.2 | 27.4 | -4.9 | -2 |
| 1294 | 290.5 | 14.204 | 14.195 | 32.2 | 336.7 | 14.206 | 14.198 | 29.9 | 317.2 | 496.0 | 313.7 | 27.2 | -5.4 | -7 |
| 1295 | 269.8 | 14.202 | 14.195 | 27.8 | 316.0 | 14.205 | 14.197 | 31.2 | 296.5 | 496.4 | 293.0 | 28.8 | -5.3 | 0.0 |
| 1296 | 250.2 | 14.203 | 14.193 | 34.6 | 296.3 | 14.206 | 14.197 | 32.4 | 276.8 | 496.4 | 273.3 | 21.3 | -4.9 | 1.1 |
| 1297 | 230.4 | 14.201 | 14.194 | 28.3 | 276.5 | 14.203 | 14.197 | 27.1 | 257.0 | 495.6 | 253.5 | 30.3 | -2.4 | -2.1 |
| 1298 | 210.3 | 14.200 | 14.195 | 25.9 | 256.4 | 14.207 | 14.198 | 33.1 | 236.9 | 494.2 | 233.4 | 26.0 | -4.5 | -1 |
| 1299 | 190.2 | 14.199 | 14.194 | 24.2 | 236.3 | 14.204 | 14.197 | 29.9 | 216.8 | 492.8 | 213.3 | 19.5 | -3.8 | 2.0 |
| 1300 | 169.9 | 14.200 | 14.195 | 24.5 | 216.1 | 14.202 | 14.197 | 25.7 | 196.6 | 492.6 | 193.1 | 16.8 | -2.2 | 1.5 |
| 1301 | 150.2 | 14.199 | 14.194 | 24.4 | 196.3 | 14.201 | 14.196 | 24.0 | 176.8 | 493.4 | 173.3 | 19.0 | -2.8 | -1 |
| 1302 | 130.0 | 14.199 | 14.194 | 25.3 | 176.1 | 14.201 | 14.196 | 24.8 | 156.6 | 494.8 | 153.1 | 17.5 | -9 | .6 |
| 1303 | 110.3 | 14.199 | 14.195 | 24.0 | 156.5 | 14.200 | 14.196 | 22.2 | 137.0 | 496.0 | 133.5 | 20.1 | -7 | 1.0 |
| 1304 | 89.9 | 14.199 | 14.194 | 25.4 | 136.1 | 14.201 | 14.196 | 25.3 | 116.6 | 496.9 | 113.1 | 17.4 | 2.7 | 1.5 |
| 1305 | 70.0 | 14.203 | 14.195 | 32.1 | 116.2 | 14.201 | 14.196 | 22.9 | 96.7 | 499.8 | 93.2 | 20.1 | 4.7 | 2.8 |
| 1306 | 50.3 | 14.200 | 14.194 | 26.9 | 96.5 | 14.201 | 14.196 | 25.4 | 77.0 | 501.5 | 73.5 | 22.6 | 5.4 | 4.4 |
| 1307 | 30.1 | 14.198 | 14.195 | 21.4 | 76.2 | 14.202 | 14.196 | 26.7 | 56.7 | 503.5 | 53.2 | 24.2 | 2.8 | -9.9 |
| 1308 | 10.4 | 14.199 | 14.195 | 23.8 | 56.5 | 14.205 | 14.195 | 34.2 | 37.0 | 504.4 | 33.5 | 18.3 | 1.5 | 1.0 |

TABLE 29.—DATA LISTING FOR TRAVERSE 2 AT STATION 5—HORIZONTAL SURVEY
 [Test section data for reading 1480; total pressure, 14.106; static pressure, 12.048 psia; total temperature, 498 °R; velocity, 250.3 mph; fan speed, 389.9 rpm.]

| Reading number | Probe one | | | | | Probe two | | | | | Thermocouple | | | | Wind anemometer | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|-----------------|--|--|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg | | | |
| 1480 | 35.2 | 14.094 | 14.092 | 14.6 | 24.9 | 14.107 | 14.106 | 8.7 | 33.4 | 367.9 | 27.4 | 20.6 | 0.4 | -2.5 | | | |
| 1481 | 45.6 | 14.094 | 14.091 | 9.2 | 35.4 | 14.107 | 14.106 | 5.0 | 43.9 | 118.3 | 37.9 | 21.5 | -1.0 | .8 | | | |
| 1482 | 55.0 | 14.106 | 14.098 | 16.0 | 44.7 | 14.108 | 14.108 | 5.0 | 53.2 | 118.3 | 47.2 | 21.7 | .8 | 2.3 | | | |
| 1483 | 65.5 | 14.109 | 14.099 | 17.3 | 55.2 | 14.108 | 14.107 | 5.0 | 63.7 | 118.3 | 57.7 | 39.1 | 7.0 | 10.3 | | | |
| 1484 | 75.0 | 14.110 | 14.099 | 17.6 | 64.8 | 14.108 | 14.107 | 5.0 | 73.3 | 118.3 | 67.3 | 41.6 | -2.7 | 5.7 | | | |
| 1485 | 85.3 | 14.110 | 14.099 | 17.8 | 75.0 | 14.108 | 14.107 | 5.0 | 83.5 | 118.3 | 77.5 | 42.1 | -4.8 | 2.6 | | | |
| 1486 | 95.5 | 14.113 | 14.100 | 19.5 | 85.3 | 14.111 | 14.110 | 5.0 | 93.8 | 118.3 | 87.8 | 41.1 | 5.7 | .7 | | | |
| 1487 | 105.1 | 14.112 | 14.098 | 20.0 | 94.9 | 14.112 | 14.111 | 5.0 | 103.4 | 118.3 | 97.4 | 47.2 | 10.0 | 2.1 | | | |
| 1488 | 115.8 | 14.110 | 14.097 | 19.2 | 105.6 | 14.110 | 14.109 | 5.0 | 114.1 | 118.3 | 108.1 | 45.3 | 7.8 | 2.6 | | | |
| 1489 | 125.3 | 14.111 | 14.098 | 19.5 | 115.0 | 14.108 | 14.107 | 5.0 | 123.5 | 118.3 | 117.5 | 44.3 | 3.2 | 2.6 | | | |
| 1490 | 135.7 | 14.112 | 14.097 | 21.0 | 125.4 | 14.109 | 14.108 | 5.0 | 133.9 | 118.3 | 127.9 | 46.7 | -0.5 | -0.3 | | | |
| 1491 | 145.3 | 14.112 | 14.097 | 20.6 | 135.0 | 14.111 | 14.110 | 5.0 | 143.5 | 118.3 | 137.5 | 47.7 | -6 | -1.7 | | | |
| 1492 | 155.2 | 14.109 | 14.096 | 19.4 | 145.0 | 14.111 | 14.110 | 5.0 | 153.5 | 118.3 | 147.5 | 44.0 | .4 | -1.1 | | | |
| 1493 | 165.3 | 14.107 | 14.096 | 17.8 | 155.1 | 14.111 | 14.111 | 5.0 | 163.6 | 118.3 | 157.6 | 42.4 | 3.2 | -5 | | | |
| 1494 | 175.3 | 14.110 | 14.096 | 19.9 | 165.1 | 14.109 | 14.109 | 5.0 | 173.6 | 118.3 | 167.6 | 43.7 | 2.7 | .2 | | | |
| 1495 | 185.5 | 14.112 | 14.097 | 21.1 | 175.2 | 14.109 | 14.109 | 5.0 | 183.7 | 118.3 | 177.7 | 46.9 | 2.4 | 0.4 | | | |
| 1496 | 195.2 | 14.112 | 14.097 | 20.9 | 184.9 | 14.110 | 14.109 | 5.0 | 193.4 | 118.3 | 187.4 | 47.9 | 2.6 | .7 | | | |
| 1497 | 205.3 | 14.110 | 14.096 | 20.3 | 195.0 | 14.109 | 14.109 | 5.0 | 203.5 | 118.3 | 197.5 | 46.0 | 2.6 | 1.1 | | | |
| 1498 | 215.5 | 14.111 | 14.097 | 20.3 | 205.3 | 14.108 | 14.108 | 5.0 | 213.8 | 118.3 | 207.8 | 47.3 | 2.6 | 1.7 | | | |
| 1499 | 225.2 | 14.110 | 14.097 | 19.8 | 215.0 | 14.108 | 14.107 | 5.0 | 223.5 | 118.3 | 217.5 | 45.2 | 3.6 | 2.1 | | | |

TABLE 29.—Concluded.

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|-----------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1500 | 235.1 | 14.110 | 14.096 | 19.5 | 224.8 | 14.108 | 14.107 | 5.0 | 233.3 | 118.3 | 227.3 | 44.9 | 3.5 | 2.3 |
| 1501 | 245.6 | 14.110 | 14.096 | 20.1 | 235.4 | 14.108 | 14.107 | 5.0 | 243.9 | 118.3 | 237.9 | 45.4 | 2.9 | 2.1 |
| 1502 | 255.0 | 14.109 | 14.095 | 20.1 | 244.7 | 14.107 | 14.106 | 5.0 | 253.2 | 118.3 | 247.2 | 46.0 | 2.0 | 2.1 |
| 1503 | 265.3 | 14.109 | 14.096 | 19.0 | 255.1 | 14.108 | 14.107 | 5.0 | 263.6 | 118.3 | 257.6 | 44.1 | 1.9 | 2.1 |
| 1504 | 275.0 | 14.110 | 14.098 | 18.6 | 264.7 | 14.108 | 14.107 | 5.0 | 273.2 | 118.3 | 267.2 | 43.2 | 1.8 | 2.3 |
| 1505 | 285.2 | 14.111 | 14.100 | 18.2 | 275.0 | 14.109 | 14.108 | 5.0 | 283.5 | 118.3 | 277.5 | 43.1 | 1.6 | 1.4 |
| 1506 | 295.6 | 14.111 | 14.101 | 17.3 | 285.4 | 14.109 | 14.108 | 5.0 | 293.9 | 118.3 | 287.9 | 41.9 | 1.4 | 1.3 |
| 1507 | 305.3 | 14.110 | 14.101 | 16.5 | 295.0 | 14.109 | 14.108 | 5.0 | 303.5 | 118.3 | 297.5 | 41.0 | 1.6 | 1.1 |
| 1508 | 315.4 | 14.108 | 14.099 | 15.8 | 305.1 | 14.108 | 14.107 | 5.0 | 313.6 | 118.3 | 307.6 | 38.1 | 2.3 | .7 |
| 1509 | 320.8 | 14.106 | 14.098 | 15.6 | 310.6 | 14.108 | 14.107 | 5.0 | 319.1 | 118.3 | 313.1 | 38.0 | 2.1 | 0.0 |
| 1510 | 260.0 | 14.111 | 14.097 | 19.6 | 249.8 | 14.108 | 14.107 | 5.0 | 258.3 | 118.3 | 252.3 | 45.2 | 1.5 | 2.7 |
| 1511 | 210.3 | 14.112 | 14.098 | 20.3 | 200.1 | 14.108 | 14.107 | 5.1 | 208.6 | 118.3 | 202.6 | 45.8 | 3.0 | 1.7 |
| 1512 | 160.6 | 14.109 | 14.097 | 18.4 | 150.4 | 14.108 | 14.107 | 5.1 | 158.9 | 118.3 | 152.9 | 42.3 | 3.0 | -.5 |
| 1513 | 110.5 | 14.110 | 14.098 | 19.1 | 100.3 | 14.108 | 14.107 | 5.1 | 108.8 | 118.3 | 102.8 | 44.7 | 8.2 | 2.2 |
| 1514 | 58.3 | 14.109 | 14.098 | 17.3 | 48.0 | 14.109 | 14.108 | 5.0 | 56.5 | 118.3 | 50.5 | 32.2 | 2.3 | 5.0 |
| 1515 | 35.4 | 14.102 | 14.099 | 8.5 | 25.2 | 14.109 | 14.108 | 5.0 | 33.7 | 118.3 | 27.7 | 20.3 | .2 | -2.6 |

TABLE 30.—DATA LISTING FOR TRAVERSE 1 AT STATION 5—HORIZONTAL SURVEY NEAR FLOOR
 [Test section data for reading 1317; total pressure, 14.219; static pressure, 13.132 psia; total temperature, 500 °R; velocity, 267.5 mph; fan speed, 292.9 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1317 | 8.1 | 14.204 | 14.201 | 19.2 | 55.1 | 14.205 | 14.200 | 24.8 | 36.8 | 496.7 | 32.0 | 6.9 | 2.3 | -0.7 |
| 1318 | 5.1 | 14.205 | 14.202 | 20.4 | 52.1 | 14.206 | 14.202 | 22.5 | 33.9 | 500.8 | 29.0 | 5.7 | 2.8 | .3 |
| 1319 | 5.1 | 14.205 | 14.201 | 20.3 | 52.1 | 14.205 | 14.201 | 22.8 | 33.9 | 500.7 | 29.0 | 5.7 | 3.0 | .2 |
| 1320 | 8.4 | 14.204 | 14.201 | 19.3 | 55.4 | 14.206 | 14.201 | 24.6 | 37.2 | 500.9 | 32.3 | 1.4 | 2.4 | .2 |
| 1321 | 15.1 | 14.203 | 14.201 | 16.1 | 62.1 | 14.207 | 14.200 | 28.2 | 43.8 | 499.9 | 38.9 | 8.2 | 1.3 | 0.0 |
| 1322 | 25.1 | 14.203 | 14.201 | 15.8 | 72.1 | 14.209 | 14.200 | 33.0 | 53.8 | 491.3 | 49.0 | 13.8 | 1.6 | -4.4 |
| 1323 | 35.5 | 14.202 | 14.200 | 16.1 | 82.5 | 14.209 | 14.199 | 34.0 | 64.2 | 490.3 | 59.4 | 21.1 | 5.1 | -2 |
| 1324 | 45.1 | 14.204 | 14.200 | 21.7 | 92.1 | 14.207 | 14.199 | 31.5 | 73.8 | 494.9 | 69.0 | 24.2 | 4.8 | -4.5 |
| 1325 | 55.3 | 14.205 | 14.200 | 24.9 | 102.3 | 14.207 | 14.199 | 31.0 | 84.1 | 494.3 | 79.2 | 26.7 | -4 | -2.7 |
| 1326 | 65.2 | 14.207 | 14.201 | 27.7 | 112.2 | 14.210 | 14.199 | 35.5 | 94.0 | 494.1 | 89.1 | 24.9 | -2.5 | 3.9 |
| 1327 | 74.9 | 14.210 | 14.201 | 34.3 | 121.9 | 14.210 | 14.199 | 35.5 | 103.7 | 494.1 | 98.8 | 25.2 | -0.3 | 5.0 |
| 1328 | 85.3 | 14.208 | 14.199 | 32.5 | 132.3 | 14.209 | 14.199 | 35.9 | 114.0 | 496.9 | 109.2 | 28.9 | 2.7 | .1 |
| 1329 | 95.3 | 14.208 | 14.200 | 31.4 | 142.3 | 14.210 | 14.199 | 36.0 | 124.0 | 495.4 | 119.1 | 29.5 | 4.0 | .1 |
| 1330 | 105.0 | 14.207 | 14.198 | 32.3 | 152.0 | 14.210 | 14.199 | 36.6 | 133.8 | 493.8 | 128.9 | 28.7 | 4.0 | 1.7 |
| 1331 | 114.8 | 14.210 | 14.199 | 36.3 | 161.8 | 14.208 | 14.199 | 32.6 | 143.6 | 492.0 | 138.7 | 30.7 | 3.8 | 1.2 |
| 1332 | 125.0 | 14.208 | 14.199 | 34.0 | 172.0 | 14.207 | 14.198 | 32.0 | 153.8 | 494.5 | 148.9 | 31.1 | 4.3 | 0.4 |
| 1333 | 135.3 | 14.209 | 14.198 | 36.3 | 182.3 | 14.208 | 14.198 | 33.5 | 164.0 | 491.9 | 159.1 | 26.6 | 3.4 | 1.7 |
| 1334 | 145.3 | 14.210 | 14.199 | 36.2 | 192.3 | 14.207 | 14.198 | 32.6 | 174.1 | 490.6 | 169.2 | 25.0 | 2.5 | 2.2 |
| 1335 | 155.0 | 14.210 | 14.200 | 35.4 | 202.0 | 14.210 | 14.199 | 34.6 | 183.7 | 491.3 | 178.8 | 26.9 | 1.9 | 2.1 |
| 1336 | 165.5 | 14.207 | 14.199 | 31.4 | 212.5 | 14.210 | 14.199 | 35.6 | 194.3 | 494.5 | 189.4 | 25.7 | 1.1 | 2.4 |
| 1337 | 175.0 | 14.208 | 14.199 | 32.4 | 222.0 | 14.208 | 14.199 | 34.6 | 203.7 | 497.0 | 198.8 | 28.1 | 1.4 | 3.0 |
| 1338 | 185.0 | 14.209 | 14.200 | 32.7 | 232.0 | 14.209 | 14.200 | 32.6 | 213.7 | 494.5 | 208.9 | 30.4 | 1.4 | 1.5 |
| 1339 | 206.1 | 14.211 | 14.201 | 35.3 | 253.1 | 14.208 | 14.200 | 30.7 | 234.9 | 494.6 | 230.0 | 26.0 | 1.3 | 1.9 |
| 1340 | 195.3 | 14.209 | 14.200 | 33.0 | 242.3 | 14.208 | 14.200 | 31.1 | 224.0 | 492.1 | 219.1 | 28.5 | 1.4 | 1.8 |
| 1341 | 205.2 | 14.210 | 14.200 | 35.0 | 252.2 | 14.208 | 14.200 | 30.8 | 234.0 | 493.1 | 229.1 | 26.4 | 1.4 | 1.6 |

TABLE 30.—Concluded.

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|-----------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1342 | 215.4 | 14.210 | 14.200 | 34.6 | 262.4 | 14.208 | 14.200 | 30.4 | 244.1 | 492.1 | 239.2 | 24.8 | 0.9 | 1.7 |
| 1343 | 225.3 | 14.209 | 14.199 | 33.2 | 272.3 | 14.208 | 14.200 | 30.1 | 254.0 | 490.5 | 249.2 | 23.7 | .2 | 1.8 |
| 1344 | 235.3 | 14.208 | 14.200 | 31.2 | 282.3 | 14.208 | 14.200 | 29.6 | 264.1 | 491.2 | 259.2 | 23.6 | .7 | .6 |
| 1345 | 245.3 | 14.208 | 14.200 | 30.8 | 292.3 | 14.207 | 14.200 | 29.1 | 274.1 | 491.9 | 269.2 | 23.3 | -.1 | .7 |
| 1346 | 255.3 | 14.208 | 14.200 | 30.5 | 302.3 | 14.208 | 14.201 | 28.5 | 284.1 | 491.2 | 279.2 | 22.3 | .5 | .4 |
| | | | | | | | | | | | | | | |
| 1347 | 264.9 | 14.209 | 14.202 | 30.0 | 311.9 | 14.208 | 14.202 | 28.3 | 293.7 | 488.2 | 288.8 | 21.4 | .9 | -0.5 |
| 1348 | 275.1 | 14.211 | 14.203 | 29.6 | 322.1 | 14.210 | 14.204 | 27.0 | 303.9 | 487.5 | 299.0 | 21.3 | 2.3 | -2.2 |
| 1349 | 285.3 | 14.212 | 14.205 | 29.1 | 332.3 | 14.212 | 14.206 | 26.3 | 314.1 | 488.3 | 309.2 | 20.2 | 1.0 | -2.5 |
| 1350 | 289.8 | 14.211 | 14.204 | 29.0 | 336.8 | 14.211 | 14.205 | 25.4 | 318.5 | 492.0 | 313.7 | 19.7 | 1.9 | -1.5 |
| 1351 | 270.0 | 14.212 | 14.205 | 29.9 | 317.0 | 14.211 | 14.205 | 27.7 | 298.8 | 491.7 | 293.9 | 21.7 | 1.1 | -.3 |
| | | | | | | | | | | | | | | |
| 1352 | 250.2 | 14.214 | 14.206 | 30.6 | 297.2 | 14.212 | 14.205 | 29.0 | 279.0 | 489.2 | 274.1 | 23.0 | 0.4 | 0.1 |
| 1353 | 230.4 | 14.215 | 14.207 | 32.2 | 277.4 | 14.214 | 14.207 | 29.8 | 259.1 | 490.3 | 254.3 | 23.5 | -.1 | 2.4 |
| 1354 | 210.3 | 14.217 | 14.206 | 35.1 | 257.3 | 14.215 | 14.207 | 30.7 | 239.0 | 494.5 | 234.1 | 25.6 | 1.2 | 2.4 |
| 1355 | 189.8 | 14.216 | 14.207 | 32.4 | 236.8 | 14.215 | 14.207 | 31.7 | 218.5 | 493.9 | 213.6 | 29.1 | 1.5 | 2.2 |
| 1356 | 170.3 | 14.216 | 14.208 | 31.2 | 217.3 | 14.218 | 14.208 | 34.5 | 199.1 | 494.2 | 194.2 | 27.2 | 1.3 | 3.2 |
| | | | | | | | | | | | | | | |
| 1357 | 150.5 | 14.218 | 14.210 | 32.2 | 197.5 | 14.219 | 14.209 | 34.9 | 179.2 | 493.8 | 174.3 | 26.6 | 1.4 | 2.9 |
| 1358 | 130.6 | 14.221 | 14.210 | 35.6 | 177.6 | 14.218 | 14.210 | 32.5 | 159.4 | 492.2 | 154.5 | 25.0 | 2.7 | 2.7 |
| 1359 | 110.2 | 14.220 | 14.211 | 33.8 | 157.2 | 14.218 | 14.210 | 31.4 | 138.9 | 495.3 | 134.1 | 31.3 | 4.1 | 1.1 |
| 1360 | 89.9 | 14.219 | 14.210 | 32.7 | 136.9 | 14.221 | 14.209 | 37.3 | 118.7 | 492.5 | 113.8 | 28.3 | 4.5 | 1.6 |
| 1361 | 69.9 | 14.221 | 14.211 | 34.8 | 116.9 | 14.221 | 14.211 | 35.3 | 98.6 | 491.8 | 93.8 | 29.9 | 4.1 | 1.1 |
| | | | | | | | | | | | | | | |
| 1362 | 50.9 | 14.220 | 14.211 | 33.0 | 97.9 | 14.222 | 14.210 | 37.5 | 79.7 | 494.5 | 74.8 | 27.8 | 4.4 | 1.9 |
| 1363 | 29.8 | 14.220 | 14.211 | 32.3 | 76.8 | 14.222 | 14.211 | 36.8 | 58.6 | 494.6 | 53.7 | 28.4 | 4.4 | 1.0 |
| 1364 | 9.9 | 14.220 | 14.212 | 32.2 | 56.9 | 14.222 | 14.211 | 36.6 | 38.6 | 494.3 | 33.8 | 28.8 | 4.6 | 1.6 |

TABLE 31.—DATA LISTING FOR TRAVERSE 2 AT STATION 5—HORIZONTAL SURVEY AT CENTERLINE
 [Test section data for reading 1317; total pressure, 14.219; static pressure, 13.132 psia; total temperature, 500 °R; velocity, 267.5 mph; fan speed, 292.9 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1317 | 80.5 | 14.206 | 14.202 | 20.9 | 126.6 | 14.205 | 14.202 | 19.2 | 107.1 | 499.3 | 103.6 | 13.2 | 2.9 | 2.3 |
| 1318 | 5.0 | 14.205 | 14.202 | 16.9 | 51.1 | 14.205 | 14.202 | 20.3 | 31.6 | 501.9 | 28.1 | 9.4 | 1.3 | 2.3 |
| 1319 | 5.0 | 14.204 | 14.202 | 16.8 | 51.1 | 14.205 | 14.202 | 20.3 | 31.6 | 501.8 | 28.1 | 9.2 | .9 | 2.3 |
| 1320 | 7.5 | 14.204 | 14.202 | 16.8 | 53.7 | 14.205 | 14.201 | 22.2 | 34.2 | 501.9 | 30.6 | 10.6 | .5 | 1.8 |
| 1321 | 15.3 | 14.204 | 14.202 | 15.9 | 61.4 | 14.207 | 14.201 | 26.4 | 41.9 | 501.8 | 38.4 | 13.1 | .6 | .1 |
| | | | | | | | | | | | | | | |
| 1322 | 25.1 | 14.203 | 14.201 | 15.0 | 71.2 | 14.206 | 14.202 | 24.1 | 51.7 | 501.7 | 48.2 | 14.9 | 0.7 | -4.8 |
| 1323 | 35.3 | 14.203 | 14.200 | 17.5 | 81.4 | 14.204 | 14.201 | 18.8 | 61.9 | 501.1 | 58.4 | 21.0 | 2.3 | -9.3 |
| 1324 | 44.9 | 14.203 | 14.200 | 18.7 | 91.0 | 14.203 | 14.200 | 19.2 | 71.5 | 501.5 | 68.0 | 18.7 | 4.7 | .4 |
| 1325 | 55.3 | 14.205 | 14.200 | 25.7 | 101.4 | 14.202 | 14.199 | 19.5 | 81.9 | 501.5 | 78.4 | 13.2 | 4.8 | 5.3 |
| 1326 | 64.9 | 14.207 | 14.201 | 26.3 | 111.0 | 14.203 | 14.200 | 18.3 | 91.5 | 501.0 | 88.0 | 13.7 | 4.7 | 4.0 |
| | | | | | | | | | | | | | | |
| 1327 | 74.9 | 14.205 | 14.202 | 21.2 | 121.1 | 14.204 | 14.201 | 18.2 | 101.6 | 500.6 | 98.1 | 14.8 | 3.8 | 2.2 |
| 1328 | 85.4 | 14.203 | 14.200 | 19.2 | 131.5 | 14.205 | 14.202 | 19.2 | 112.0 | 500.0 | 108.5 | 14.4 | 5.7 | 1.4 |
| 1329 | 95.3 | 14.203 | 14.200 | 19.9 | 141.4 | 14.204 | 14.201 | 19.0 | 121.9 | 498.6 | 118.4 | 13.2 | 1.4 | 1.4 |
| 1330 | 105.1 | 14.203 | 14.200 | 19.9 | 151.2 | 14.204 | 14.201 | 18.2 | 131.7 | 498.6 | 128.2 | 14.4 | 1.0 | 1.1 |
| 1331 | 115.4 | 14.201 | 14.198 | 18.2 | 161.5 | 14.202 | 14.200 | 15.6 | 142.0 | 498.7 | 138.5 | 14.4 | .4 | 1.5 |
| | | | | | | | | | | | | | | |
| 1332 | 125.0 | 14.202 | 14.199 | 19.3 | 171.1 | 14.202 | 14.199 | 16.5 | 151.6 | 497.8 | 148.1 | 13.9 | 2.2 | -0.3 |
| 1333 | 135.0 | 14.202 | 14.199 | 19.8 | 181.1 | 14.201 | 14.199 | 16.8 | 161.6 | 497.6 | 158.1 | 10.3 | -.3 | 1.5 |
| 1334 | 145.0 | 14.202 | 14.198 | 19.6 | 191.1 | 14.202 | 14.199 | 17.6 | 171.6 | 496.8 | 168.1 | 11.4 | -2.2 | .4 |
| 1335 | 155.0 | 14.202 | 14.199 | 16.9 | 201.1 | 14.202 | 14.199 | 18.3 | 181.6 | 496.8 | 178.1 | 11.9 | -.9 | .3 |
| 1336 | 165.3 | 14.201 | 14.198 | 16.6 | 211.4 | 14.201 | 14.199 | 18.9 | 191.9 | 497.5 | 188.4 | 10.9 | 0.0 | 2.1 |
| | | | | | | | | | | | | | | |
| 1337 | 175.0 | 14.199 | 14.197 | 17.3 | 221.1 | 14.197 | 14.194 | 19.0 | 201.6 | 499.1 | 198.1 | 11.4 | -0.4 | 3.3 |
| 1338 | 185.4 | 14.200 | 14.197 | 17.4 | 231.5 | 14.199 | 14.195 | 20.8 | 212.0 | 499.1 | 208.5 | 12.6 | -.9 | 2.9 |
| 1339 | 205.6 | 14.202 | 14.199 | 19.0 | 251.7 | 14.203 | 14.198 | 24.3 | 232.2 | 497.3 | 228.7 | 14.5 | -4.7 | 2.4 |
| 1340 | 195.5 | 14.203 | 14.200 | 18.4 | 241.6 | 14.205 | 14.200 | 23.6 | 222.1 | 496.2 | 218.6 | 13.4 | -4.1 | 2.1 |
| 1341 | 205.4 | 14.204 | 14.201 | 19.0 | 251.5 | 14.207 | 14.202 | 24.4 | 232.0 | 497.2 | 228.5 | 15.4 | -4.5 | 1.2 |

TABLE 31.—Concluded.

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|-----------------|----------|--|--|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg | | |
| 1342 | 215.5 | 14.205 | 14.202 | 19.5 | 261.6 | 14.207 | 14.203 | 21.0 | 242.1 | 496.6 | 238.6 | 19.5 | -4.5 | -0.4 | | |
| 1343 | 225.0 | 14.204 | 14.201 | 19.8 | 271.1 | 14.206 | 14.203 | 19.8 | 251.6 | 497.6 | 248.1 | 21.6 | -2.6 | -2.4 | | |
| 1344 | 235.1 | 14.204 | 14.200 | 22.3 | 281.2 | 14.205 | 14.201 | 22.0 | 261.7 | 498.4 | 258.2 | 18.4 | -1.0 | -1.3 | | |
| 1345 | 244.8 | 14.204 | 14.199 | 24.7 | 291.0 | 14.204 | 14.199 | 25.7 | 271.5 | 498.9 | 268.0 | 14.2 | -4.0 | 1.1 | | |
| 1346 | 255.4 | 14.204 | 14.199 | 23.7 | 301.5 | 14.206 | 14.200 | 25.6 | 282.0 | 499.4 | 278.5 | 17.1 | -6.5 | .4 | | |
| 1347 | 264.8 | 14.205 | 14.201 | 20.9 | 310.9 | 14.207 | 14.202 | 24.9 | 291.4 | 499.2 | 287.9 | 22.4 | -6.0 | -0.5 | | |
| 1348 | 275.3 | 14.207 | 14.204 | 20.5 | 321.4 | 14.209 | 14.204 | 24.1 | 301.9 | 498.5 | 298.4 | 22.8 | -5.1 | -.5 | | |
| 1349 | 285.5 | 14.210 | 14.205 | 25.0 | 331.6 | 14.210 | 14.206 | 22.2 | 312.1 | 498.4 | 308.6 | 21.4 | -5.1 | -.3 | | |
| 1350 | 290.4 | 14.208 | 14.203 | 26.0 | 336.5 | 14.207 | 14.203 | 21.0 | 317.0 | 498.9 | 313.5 | 21.0 | -5.3 | -2 | | |
| 1351 | 269.9 | 14.207 | 14.204 | 20.5 | 316.0 | 14.208 | 14.203 | 24.3 | 296.5 | 499.7 | 293.0 | 23.9 | -5.5 | -.9 | | |
| 1352 | 249.8 | 14.209 | 14.204 | 24.8 | 296.0 | 14.211 | 14.205 | 26.1 | 276.5 | 499.2 | 273.0 | 15.0 | -5.6 | 0.9 | | |
| 1353 | 230.0 | 14.209 | 14.206 | 21.0 | 276.1 | 14.211 | 14.208 | 20.4 | 256.6 | 498.3 | 253.1 | 20.3 | -1.7 | -1.6 | | |
| 1354 | 210.2 | 14.209 | 14.206 | 19.4 | 256.3 | 14.211 | 14.207 | 23.1 | 236.8 | 498.3 | 233.3 | 17.2 | -5.0 | -.3 | | |
| 1355 | 190.3 | 14.209 | 14.206 | 18.1 | 236.4 | 14.210 | 14.206 | 22.0 | 216.9 | 498.7 | 213.4 | 13.3 | -3.9 | 2.7 | | |
| 1356 | 170.4 | 14.209 | 14.207 | 16.9 | 216.5 | 14.210 | 14.207 | 19.1 | 197.0 | 499.1 | 193.5 | 11.5 | -3.6 | 3.3 | | |
| 1357 | 150.5 | 14.212 | 14.209 | 18.4 | 196.6 | 14.211 | 14.208 | 18.5 | 177.1 | 498.3 | 173.6 | 11.4 | -1.5 | 0.7 | | |
| 1358 | 130.4 | 14.211 | 14.208 | 19.6 | 176.5 | 14.211 | 14.209 | 16.6 | 157.0 | 499.3 | 153.5 | 11.8 | 1.4 | .4 | | |
| 1359 | 109.9 | 14.212 | 14.209 | 19.0 | 156.0 | 14.211 | 14.209 | 16.4 | 136.5 | 500.4 | 133.0 | 14.5 | 1.4 | .6 | | |
| 1360 | 90.0 | 14.213 | 14.209 | 19.5 | 136.1 | 14.212 | 14.209 | 19.0 | 116.6 | 500.0 | 113.1 | 13.1 | 3.3 | 2.3 | | |
| 1361 | 70.4 | 14.215 | 14.210 | 25.0 | 116.5 | 14.213 | 14.211 | 17.4 | 97.0 | 501.1 | 93.5 | 14.9 | 5.0 | 3.2 | | |
| 1362 | 50.3 | 14.213 | 14.209 | 20.6 | 96.5 | 14.211 | 14.208 | 19.2 | 77.0 | 501.5 | 73.5 | 16.9 | 5.6 | 4.4 | | |
| 1363 | 30.5 | 14.212 | 14.210 | 16.2 | 76.6 | 14.212 | 14.209 | 20.2 | 57.1 | 501.5 | 53.6 | 18.4 | 2.3 | -10.4 | | |
| 1364 | 9.8 | 14.213 | 14.211 | 17.2 | 55.9 | 14.214 | 14.209 | 25.8 | 36.4 | 501.9 | 32.9 | 12.4 | 1.9 | 1.1 | | |

TABLE 32.—DATA LISTING FOR TRAVERSE 2 AT STATION 5—HORIZONTAL SURVEY NEAR CEILING
 [Test section data for reading 1516; total pressure, 14.117; static pressure, 13.031 psia; total temperature, 498 °R; velocity, 251.0 mph; fan speed, 288.6 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1516 | 35.4 | 14.109 | 14.108 | 13.6 | 25.2 | 14.114 | 14.113 | 9.3 | 33.7 | 499.4 | 27.7 | 15.1 | -0.3 | -2.4 |
| 1517 | 45.3 | 14.108 | 14.106 | 15.1 | 35.1 | 14.113 | 14.112 | 9.9 | 43.6 | 500.3 | 37.6 | 12.4 | -.9 | 1.2 |
| 1518 | 55.1 | 14.111 | 14.106 | 25.5 | 44.9 | 14.113 | 14.112 | 10.4 | 53.4 | 499.1 | 47.4 | 14.6 | .9 | 3.4 |
| 1519 | 65.2 | 14.112 | 14.105 | 27.5 | 55.0 | 14.112 | 14.111 | 10.4 | 63.5 | 499.6 | 57.5 | 28.3 | 6.9 | 9.7 |
| 1520 | 75.8 | 14.112 | 14.105 | 28.2 | 65.6 | 14.110 | 14.109 | 10.4 | 74.1 | 500.4 | 68.1 | 30.6 | -2.4 | 5.1 |
| 1521 | 85.1 | 14.110 | 14.104 | 28.2 | 74.9 | 14.110 | 14.110 | 10.4 | 83.4 | 500.8 | 77.4 | 31.4 | -4.5 | 3.3 |
| 1522 | 95.6 | 14.113 | 14.105 | 31.0 | 85.3 | 14.113 | 14.112 | 10.4 | 93.8 | 501.3 | 87.8 | 29.1 | 6.5 | 1.7 |
| 1523 | 105.4 | 14.112 | 14.104 | 31.1 | 95.2 | 14.113 | 14.112 | 10.4 | 103.7 | 501.5 | 97.7 | 34.3 | 9.6 | 1.9 |
| 1524 | 115.4 | 14.112 | 14.105 | 30.6 | 105.1 | 14.113 | 14.112 | 10.4 | 113.6 | 501.3 | 107.6 | 33.4 | 7.7 | 2.5 |
| 1525 | 125.6 | 14.113 | 14.105 | 31.2 | 115.4 | 14.113 | 14.112 | 10.4 | 123.9 | 501.0 | 117.9 | 32.3 | 2.6 | 2.3 |
| 1526 | 135.5 | 14.114 | 14.105 | 33.8 | 125.3 | 14.113 | 14.112 | 10.4 | 133.8 | 500.9 | 127.8 | 34.9 | -1.0 | -0.2 |
| 1527 | 145.3 | 14.113 | 14.105 | 32.6 | 135.1 | 14.113 | 14.112 | 10.4 | 143.6 | 500.9 | 137.6 | 35.5 | -.6 | -1.1 |
| 1528 | 155.2 | 14.111 | 14.103 | 30.6 | 145.0 | 14.113 | 14.112 | 10.4 | 153.5 | 500.8 | 147.5 | 33.5 | .6 | -.9 |
| 1529 | 164.9 | 14.110 | 14.104 | 28.4 | 154.6 | 14.112 | 14.111 | 10.4 | 163.1 | 500.7 | 157.1 | 31.6 | 3.1 | -.3 |
| 1530 | 175.2 | 14.112 | 14.104 | 31.0 | 165.0 | 14.112 | 14.111 | 10.4 | 173.5 | 500.7 | 167.5 | 32.3 | 3.4 | 0.0 |
| 1531 | 185.1 | 14.113 | 14.104 | 33.6 | 174.8 | 14.113 | 14.112 | 10.4 | 183.3 | 500.8 | 177.3 | 35.8 | 2.2 | 0.7 |
| 1532 | 195.5 | 14.112 | 14.103 | 33.2 | 185.2 | 14.112 | 14.111 | 10.4 | 193.7 | 500.6 | 187.7 | 36.3 | 2.5 | .7 |
| 1533 | 205.1 | 14.111 | 14.103 | 32.3 | 194.9 | 14.112 | 14.111 | 10.4 | 203.4 | 500.3 | 197.4 | 35.6 | 2.7 | .8 |
| 1534 | 215.4 | 14.113 | 14.105 | 31.9 | 205.2 | 14.110 | 14.109 | 10.4 | 213.7 | 500.2 | 207.7 | 35.0 | 2.4 | 2.1 |
| 1535 | 225.2 | 14.111 | 14.103 | 31.2 | 215.0 | 14.110 | 14.109 | 10.4 | 223.5 | 500.4 | 217.5 | 33.7 | 3.9 | 2.4 |
| 1536 | 235.6 | 14.110 | 14.102 | 30.7 | 225.3 | 14.110 | 14.109 | 10.4 | 233.8 | 500.4 | 227.8 | 34.0 | 3.7 | 2.5 |
| 1537 | 245.4 | 14.112 | 14.103 | 32.0 | 235.1 | 14.110 | 14.109 | 10.4 | 243.6 | 500.0 | 237.6 | 34.7 | 2.1 | 2.6 |
| 1538 | 255.2 | 14.113 | 14.104 | 31.8 | 244.9 | 14.110 | 14.109 | 10.4 | 253.4 | 499.9 | 247.4 | 35.7 | 1.5 | 2.2 |
| 1539 | 265.4 | 14.111 | 14.104 | 30.0 | 255.2 | 14.110 | 14.109 | 10.4 | 263.7 | 499.6 | 257.7 | 33.4 | 2.2 | 2.3 |
| 1540 | 275.4 | 14.110 | 14.103 | 30.0 | 265.1 | 14.110 | 14.109 | 10.4 | 273.6 | 499.7 | 267.6 | 32.8 | 1.9 | 2.2 |

TABLE 32.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 1541 | 285.3 | 14.107 | 14.101 | 29.1 | 275.0 | 14.109 | 14.108 | 10.4 | 283.5 | 500.6 | 277.5 | 32.1 | 2.1 | 2.6 |
| 1542 | 295.7 | 14.105 | 14.099 | 27.6 | 285.5 | 14.108 | 14.107 | 10.5 | 294.0 | 501.6 | 288.0 | 31.5 | 1.5 | 2.2 |
| 1543 | 305.5 | 14.103 | 14.098 | 25.4 | 295.2 | 14.108 | 14.107 | 10.5 | 303.7 | 501.8 | 297.7 | 30.3 | 2.4 | 1.7 |
| 1544 | 315.3 | 14.103 | 14.098 | 24.5 | 305.0 | 14.108 | 14.107 | 10.5 | 313.5 | 501.4 | 307.5 | 29.2 | 2.0 | .9 |
| 1545 | 321.3 | 14.106 | 14.101 | 23.7 | 311.0 | 14.108 | 14.107 | 10.5 | 319.5 | 500.8 | 313.5 | 26.7 | 2.9 | .6 |
| 1546 | 260.1 | 14.110 | 14.102 | 31.0 | 249.8 | 14.109 | 14.108 | 10.5 | 258.3 | 500.2 | 252.3 | 34.1 | 1.6 | 2.5 |
| 1547 | 210.2 | 14.111 | 14.102 | 32.3 | 200.0 | 14.109 | 14.108 | 10.6 | 208.5 | 500.5 | 202.5 | 35.3 | 2.5 | 2.0 |
| 1548 | 160.6 | 14.105 | 14.099 | 28.6 | 150.4 | 14.107 | 14.106 | 10.6 | 158.9 | 500.8 | 152.9 | 32.6 | 2.5 | -.8 |
| 1549 | 110.3 | 14.107 | 14.099 | 30.3 | 100.0 | 14.107 | 14.106 | 10.6 | 108.5 | 501.0 | 102.5 | 35.1 | 8.7 | 2.3 |
| 1550 | 60.4 | 14.107 | 14.101 | 27.8 | 50.1 | 14.108 | 14.107 | 10.6 | 58.6 | 501.1 | 52.6 | 27.2 | 3.9 | 6.9 |
| 1551 | 35.7 | 14.102 | 14.101 | 13.6 | 25.5 | 14.108 | 14.108 | 9.2 | 34.0 | 501.7 | 28.0 | 14.6 | .4 | -2.4 |

TABLE 33.—DATA LISTING FOR TRAVERSE 1 AT STATION 6—UPPER HORIZONTAL SURVEY
 [Test section data for reading 2309; total pressure, 14.308; static pressure, 12.215 psia; total temperature, 498 °R; velocity, 350.7 mph; fan speed, 387.6 rpm.]

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|-----------------|----------|--|--|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg | | |
| 2309 | 51.1 | 14.290 | 14.285 | 26.8 | 40.6 | 14.287 | 14.278 | 33.6 | 50.8 | 504.7 | 45.8 | 35.0 | 15.4 | -8.0 | | |
| 2310 | 61.1 | 14.293 | 14.286 | 28.7 | 50.6 | 14.285 | 14.275 | 35.0 | 60.8 | 500.3 | 55.8 | 38.0 | 13.8 | -7.3 | | |
| 2311 | 70.9 | 14.293 | 14.286 | 28.8 | 60.4 | 14.293 | 14.273 | 48.3 | 70.6 | 494.5 | 65.6 | 39.0 | 11.2 | -10.1 | | |
| 2312 | 80.9 | 14.294 | 14.285 | 32.3 | 70.4 | 14.290 | 14.272 | 46.8 | 80.7 | 495.9 | 75.7 | 51.6 | 8.0 | -5.3 | | |
| 2313 | 91.0 | 14.293 | 14.285 | 31.5 | 80.5 | 14.315 | 14.296 | 47.2 | 90.8 | 498.5 | 85.8 | 49.3 | 6.6 | -7.6 | | |
| 2314 | 97.7 | 14.292 | 14.285 | 28.8 | 87.2 | 14.314 | 14.296 | 46.5 | 97.5 | 499.9 | 92.5 | 49.7 | 5.1 | -8.5 | | |
| 2315 | 107.3 | 14.290 | 14.283 | 28.0 | 96.8 | 14.292 | 14.274 | 46.6 | 107.1 | 499.0 | 102.1 | 50.1 | 5.0 | -10.0 | | |
| 2316 | 120.7 | 14.291 | 14.284 | 29.4 | 110.2 | 14.288 | 14.268 | 49.5 | 120.4 | 497.1 | 115.4 | 51.5 | 5.9 | -7.5 | | |
| 2317 | 130.7 | 14.292 | 14.284 | 31.2 | 120.2 | 14.288 | 14.268 | 49.2 | 130.5 | 496.9 | 125.5 | 52.4 | 5.2 | -7.2 | | |
| 2318 | 140.7 | 14.290 | 14.283 | 29.1 | 130.2 | 14.288 | 14.269 | 48.8 | 140.5 | 495.9 | 135.5 | 51.1 | 3.8 | -7.3 | | |
| 2319 | 150.5 | 14.290 | 14.283 | 29.1 | 140.0 | 14.289 | 14.269 | 48.7 | 150.2 | 496.1 | 145.2 | 50.8 | 2.5 | -6.6 | | |
| 2320 | 160.9 | 14.289 | 14.283 | 27.0 | 150.4 | 14.293 | 14.273 | 48.7 | 160.6 | 496.9 | 155.6 | 51.4 | 1.5 | -8.2 | | |
| 2321 | 170.6 | 14.287 | 14.282 | 24.5 | 160.1 | 14.293 | 14.275 | 45.6 | 170.3 | 496.5 | 165.3 | 49.2 | .2 | -8.0 | | |
| 2322 | 181.0 | 14.286 | 14.282 | 22.0 | 170.5 | 14.304 | 14.283 | 50.3 | 180.8 | 496.4 | 175.8 | 49.1 | -.8 | -10.0 | | |
| 2323 | 190.7 | 14.286 | 14.283 | 19.9 | 180.2 | 14.293 | 14.272 | 50.4 | 190.4 | 496.6 | 185.4 | 53.0 | -2.6 | -8.5 | | |
| 2324 | 201.0 | 14.286 | 14.283 | 18.4 | 190.5 | 14.290 | 14.267 | 53.1 | 200.7 | 496.5 | 195.7 | 54.8 | -3.7 | -8.0 | | |
| 2325 | 211.3 | 14.286 | 14.283 | 18.7 | 200.8 | 14.288 | 14.265 | 52.1 | 211.0 | 496.7 | 206.0 | 55.9 | -4.7 | -7.1 | | |
| 2326 | 220.6 | 14.286 | 14.284 | 15.8 | 210.1 | 14.287 | 14.265 | 50.8 | 220.3 | 496.5 | 215.3 | 54.6 | -5.6 | -7.1 | | |
| 2327 | 231.1 | 14.284 | 14.283 | 14.0 | 220.6 | 14.282 | 14.264 | 47.3 | 230.9 | 496.6 | 225.9 | 51.1 | -6.5 | -6.9 | | |
| 2328 | 240.4 | 14.284 | 14.283 | 10.8 | 229.9 | 14.283 | 14.264 | 46.5 | 240.1 | 497.1 | 235.1 | 47.6 | -7.0 | -6.2 | | |
| 2329 | 250.7 | 14.284 | 14.283 | 9.2 | 240.2 | 14.281 | 14.264 | 45.8 | 250.5 | 497.9 | 245.5 | 48.1 | -9.2 | -7.0 | | |
| 2330 | 260.6 | 14.284 | 14.283 | 4.6 | 250.1 | 14.278 | 14.263 | 43.0 | 260.3 | 497.3 | 255.3 | 46.6 | -9.6 | -6.8 | | |
| 2331 | 270.6 | 14.284 | 14.284 | 0.0 | 260.1 | 14.278 | 14.265 | 40.3 | 270.4 | 496.9 | 265.4 | 42.6 | -11.3 | -6.4 | | |
| 2332 | 281.0 | 14.286 | 14.286 | 0.0 | 270.5 | 14.277 | 14.266 | 36.5 | 280.8 | 497.2 | 275.8 | 38.3 | -12.2 | -8.8 | | |
| 2333 | 290.6 | 14.286 | 14.287 | 0.0 | 280.1 | 14.280 | 14.267 | 40.0 | 290.4 | 497.2 | 285.4 | 41.5 | -12.1 | -6.8 | | |

TABLE 33.—Concluded.

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|-----------------|----------|--|--|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg | | |
| 2334 | 300.5 | 14.287 | 14.287 | 0.0 | 290.0 | 14.281 | 14.268 | 39.2 | 300.3 | 497.9 | 295.3 | 41.8 | -12.2 | -6.4 | | |
| 2335 | 310.1 | 14.287 | 14.288 | 0.0 | 299.6 | 14.281 | 14.269 | 37.4 | 309.9 | 498.6 | 304.9 | 40.2 | -13.2 | -7.0 | | |
| 2336 | 315.5 | 14.289 | 14.289 | 0.0 | 305.0 | 14.281 | 14.270 | 36.3 | 315.3 | 499.0 | 310.3 | 39.6 | -13.7 | -6.2 | | |
| 2337 | 295.8 | 14.287 | 14.288 | 0.0 | 285.3 | 14.281 | 14.268 | 39.7 | 295.5 | 498.2 | 290.5 | 42.0 | -12.2 | -6.9 | | |
| 2338 | 276.2 | 14.287 | 14.287 | 0.0 | 265.7 | 14.278 | 14.267 | 36.6 | 276.0 | 497.5 | 271.0 | 40.8 | -11.9 | -7.5 | | |
| | | | | | | | | | | | | | | | | |
| 2339 | 255.9 | 14.285 | 14.285 | 5.9 | 245.4 | 14.282 | 14.265 | 44.8 | 255.6 | 497.6 | 250.6 | 48.2 | -9.1 | -7.4 | | |
| 2340 | 235.8 | 14.286 | 14.285 | 11.3 | 225.3 | 14.282 | 14.264 | 46.1 | 235.6 | 496.9 | 230.6 | 48.8 | -6.7 | -6.6 | | |
| 2341 | 215.8 | 14.287 | 14.285 | 16.8 | 205.3 | 14.286 | 14.263 | 51.7 | 215.5 | 497.0 | 210.5 | 56.2 | -5.4 | -7.3 | | |
| 2342 | 195.6 | 14.287 | 14.284 | 18.6 | 185.1 | 14.286 | 14.264 | 52.4 | 195.3 | 498.0 | 190.3 | 54.2 | -3.2 | -8.6 | | |
| 2343 | 175.7 | 14.289 | 14.284 | 25.2 | 165.2 | 14.281 | 14.262 | 47.6 | 175.5 | 497.2 | 170.5 | 48.0 | -6 | -10.0 | | |
| | | | | | | | | | | | | | | | | |
| 2344 | 155.9 | 14.290 | 14.284 | 27.6 | 145.4 | 14.282 | 14.262 | 49.1 | 155.7 | 498.9 | 150.7 | 51.7 | 1.9 | -7.6 | | |
| 2345 | 135.7 | 14.292 | 14.285 | 30.6 | 125.2 | 14.283 | 14.263 | 49.0 | 135.4 | 499.1 | 130.4 | 52.1 | 4.4 | -7.6 | | |
| 2346 | 116.0 | 14.293 | 14.286 | 28.5 | 105.5 | 14.285 | 14.265 | 49.1 | 115.8 | 501.6 | 110.8 | 52.1 | 5.4 | -8.4 | | |
| 2347 | 96.0 | 14.294 | 14.287 | 29.3 | 85.5 | 14.284 | 14.266 | 46.9 | 95.7 | 503.3 | 90.7 | 50.1 | 5.4 | -8.0 | | |
| 2348 | 76.1 | 14.295 | 14.288 | 29.4 | 65.6 | 14.288 | 14.268 | 48.8 | 75.9 | 504.1 | 70.9 | 47.5 | 9.8 | -6.8 | | |
| 2349 | 56.0 | 14.296 | 14.290 | 27.1 | 45.5 | 14.278 | 14.268 | 35.1 | 55.7 | 504.7 | 50.7 | 35.9 | 14.9 | -7.6 | | |

TABLE 34.—DATA LISTING FOR TRAVERSE 2 AT STATION 6—LOWER HORIZONTAL SURVEY
 [Test section data for reading 2309; total pressure, 14.308; static pressure, 12.215 psia; total temperature, 498 °R; velocity, 350.7 mph; fan speed, 387.6 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 2309 | 50.5 | 14.287 | 14.281 | 27.6 | 40.2 | 14.290 | 14.279 | 37.5 | 48.7 | 500.6 | 42.7 | 37.5 | 13.7 | 15.3 |
| 2310 | 60.8 | 14.293 | 14.282 | 36.6 | 50.5 | 14.293 | 14.281 | 38.1 | 59.0 | 501.0 | 53.0 | 39.0 | 11.5 | 6.7 |
| 2311 | 70.4 | 14.295 | 14.283 | 37.0 | 60.2 | 14.300 | 14.282 | 46.3 | 68.7 | 498.1 | 62.7 | 44.0 | 10.3 | 2.7 |
| 2312 | 80.9 | 14.299 | 14.282 | 45.0 | 70.6 | 14.299 | 14.281 | 47.1 | 79.1 | 495.9 | 73.1 | 49.8 | 13.0 | 10.1 |
| 2313 | 90.4 | 14.300 | 14.282 | 46.1 | 80.2 | 14.300 | 14.281 | 47.5 | 88.7 | 497.0 | 82.7 | 50.7 | 17.2 | 7.8 |
| 2314 | 97.9 | 14.301 | 14.281 | 48.4 | 87.6 | 14.300 | 14.280 | 49.1 | 96.1 | 498.4 | 90.1 | 50.6 | 11.6 | -0.1 |
| 2315 | 108.0 | 14.303 | 14.283 | 48.5 | 97.8 | 14.301 | 14.281 | 49.9 | 106.3 | 499.4 | 100.3 | 52.5 | 3.6 | 1.2 |
| 2316 | 120.6 | 14.305 | 14.284 | 49.7 | 110.3 | 14.305 | 14.282 | 51.7 | 118.8 | 498.5 | 112.8 | 56.1 | 2.2 | 3.8 |
| 2317 | 130.5 | 14.305 | 14.283 | 51.4 | 120.2 | 14.302 | 14.281 | 50.4 | 128.7 | 498.4 | 122.7 | 56.6 | 2.3 | 4.7 |
| 2318 | 140.5 | 14.304 | 14.283 | 50.5 | 130.2 | 14.302 | 14.281 | 49.9 | 138.7 | 497.7 | 132.7 | 57.3 | 3.1 | 5.7 |
| 2319 | 150.4 | 14.303 | 14.283 | 49.3 | 140.2 | 14.307 | 14.281 | 55.2 | 148.7 | 496.3 | 142.7 | 59.7 | 3.1 | 9.0 |
| 2320 | 160.2 | 14.306 | 14.281 | 54.3 | 150.0 | 14.304 | 14.280 | 53.2 | 158.5 | 495.5 | 152.5 | 59.0 | 2.6 | 10.7 |
| 2321 | 170.5 | 14.306 | 14.282 | 53.7 | 160.2 | 14.300 | 14.281 | 47.6 | 168.7 | 495.1 | 162.7 | 56.5 | .3 | 10.1 |
| 2322 | 181.1 | 14.300 | 14.281 | 47.4 | 170.9 | 14.305 | 14.282 | 52.6 | 179.4 | 495.3 | 173.4 | 54.4 | -2.2 | 8.9 |
| 2323 | 190.4 | 14.306 | 14.282 | 53.3 | 180.1 | 14.304 | 14.281 | 52.0 | 188.6 | 495.5 | 182.6 | 57.9 | -2.7 | 6.3 |
| 2324 | 200.9 | 14.305 | 14.282 | 51.8 | 190.6 | 14.306 | 14.283 | 52.9 | 199.1 | 495.4 | 193.1 | 59.7 | -3.4 | 6.0 |
| 2325 | 210.8 | 14.306 | 14.283 | 52.8 | 200.6 | 14.306 | 14.283 | 52.3 | 209.1 | 495.6 | 203.1 | 59.7 | -4.3 | 6.4 |
| 2326 | 220.3 | 14.306 | 14.283 | 52.2 | 210.0 | 14.305 | 14.284 | 50.6 | 218.5 | 495.4 | 212.5 | 58.4 | -4.6 | 7.5 |
| 2327 | 230.8 | 14.304 | 14.283 | 50.5 | 220.5 | 14.304 | 14.283 | 49.1 | 229.0 | 495.1 | 223.0 | 56.7 | -6.1 | 7.6 |
| 2328 | 240.1 | 14.303 | 14.283 | 48.9 | 229.9 | 14.305 | 14.285 | 48.6 | 238.4 | 495.2 | 232.4 | 54.7 | -7.8 | 6.5 |
| 2329 | 250.7 | 14.304 | 14.284 | 48.4 | 240.4 | 14.304 | 14.285 | 46.9 | 248.9 | 495.3 | 242.9 | 55.0 | -8.9 | 6.2 |
| 2330 | 260.3 | 14.304 | 14.285 | 47.1 | 250.1 | 14.300 | 14.284 | 43.3 | 258.6 | 496.1 | 252.6 | 52.1 | -10.0 | 7.2 |
| 2331 | 270.7 | 14.301 | 14.285 | 43.2 | 260.4 | 14.300 | 14.285 | 42.6 | 268.9 | 495.7 | 262.9 | 50.3 | -9.9 | 8.7 |
| 2332 | 280.4 | 14.301 | 14.286 | 42.0 | 270.1 | 14.300 | 14.288 | 37.5 | 278.6 | 495.5 | 272.6 | 42.8 | -12.5 | 9.2 |
| 2333 | 290.4 | 14.298 | 14.287 | 36.9 | 280.1 | 14.300 | 14.287 | 39.1 | 288.6 | 495.2 | 282.6 | 47.0 | -12.3 | 9.8 |

TABLE 34.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | Wind anemometer | | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|-----------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 2334 | 300.6 | 14.301 | 14.288 | 38.5 | 290.3 | 14.300 | 14.288 | 37.9 | 298.8 | 494.5 | 292.8 | 45.3 | -12.4 | 9.2 |
| 2335 | 310.0 | 14.301 | 14.289 | 37.9 | 299.7 | 14.300 | 14.289 | 36.2 | 308.2 | 493.1 | 302.2 | 43.1 | -13.6 | 10.1 |
| 2336 | 315.9 | 14.302 | 14.291 | 37.1 | 305.6 | 14.301 | 14.291 | 34.4 | 314.1 | 492.1 | 308.1 | 42.0 | -14.4 | 9.3 |
| 2337 | 295.3 | 14.302 | 14.288 | 39.8 | 285.0 | 14.301 | 14.289 | 38.7 | 293.5 | 495.2 | 287.5 | 46.5 | -12.4 | 9.1 |
| 2338 | 275.9 | 14.302 | 14.288 | 41.8 | 265.6 | 14.301 | 14.288 | 38.9 | 274.1 | 495.3 | 268.1 | 46.7 | -11.7 | 9.6 |
| 2339 | 255.6 | 14.307 | 14.287 | 48.6 | 245.4 | 14.305 | 14.287 | 45.9 | 253.9 | 495.4 | 247.9 | 53.2 | -9.2 | 6.6 |
| 2340 | 235.9 | 14.307 | 14.286 | 49.6 | 225.6 | 14.306 | 14.286 | 48.4 | 234.1 | 496.0 | 228.1 | 55.6 | -7.1 | 7.3 |
| 2341 | 215.9 | 14.310 | 14.286 | 53.9 | 205.6 | 14.308 | 14.285 | 52.1 | 214.1 | 496.6 | 208.1 | 58.8 | -4.3 | 6.7 |
| 2342 | 195.6 | 14.308 | 14.285 | 51.7 | 185.4 | 14.309 | 14.285 | 53.0 | 193.9 | 496.7 | 187.9 | 59.2 | -3.1 | 5.5 |
| 2343 | 175.6 | 14.307 | 14.285 | 52.1 | 165.3 | 14.307 | 14.285 | 50.8 | 173.8 | 497.2 | 167.8 | 53.2 | -9 | 10.7 |
| 2344 | 155.4 | 14.307 | 14.284 | 52.2 | 145.1 | 14.311 | 14.286 | 54.8 | 153.6 | 494.8 | 147.6 | 60.0 | 2.8 | 9.9 |
| 2345 | 135.3 | 14.309 | 14.287 | 50.9 | 125.0 | 14.307 | 14.286 | 50.1 | 133.5 | 499.2 | 127.5 | 57.7 | 2.7 | 5.1 |
| 2346 | 115.3 | 14.309 | 14.289 | 49.1 | 105.1 | 14.309 | 14.288 | 50.7 | 113.6 | 499.3 | 107.6 | 55.1 | 2.0 | 2.8 |
| 2347 | 95.8 | 14.308 | 14.289 | 47.6 | 85.6 | 14.308 | 14.289 | 47.9 | 94.1 | 498.3 | 88.1 | 49.9 | 13.5 | 1.7 |
| 2348 | 75.6 | 14.306 | 14.291 | 41.3 | 65.3 | 14.308 | 14.289 | 47.5 | 73.8 | 496.8 | 67.8 | 46.8 | 11.8 | 6.8 |
| 2349 | 55.7 | 14.302 | 14.292 | 34.3 | 45.4 | 14.303 | 14.292 | 36.4 | 53.9 | 501.0 | 47.9 | 42.7 | 12.1 | 12.3 |

TABLE 35.—DATA LISTING FOR TRAVERSE 1 AT STATION 6—UPPER HORIZONTAL SURVEY
 [Test section data for reading 2350; total pressure, 14.324; static pressure, 13.227 psia; total temperature, 500 °R; velocity, 250.7 mph; fan speed, 286.2 rpm.]

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | | | Wind anemometer | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|-----------------|----------|--|--|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg | | |
| 2350 | 50.7 | 14.309 | 14.306 | 20.2 | 40.2 | 14.305 | 14.299 | 25.5 | 50.5 | 503.1 | 45.5 | 26.7 | 13.4 | -8.0 | | |
| 2351 | 61.1 | 14.308 | 14.304 | 22.3 | 50.6 | 14.304 | 14.298 | 26.7 | 60.8 | 501.9 | 55.8 | 28.8 | 12.8 | -8.1 | | |
| 2352 | 70.9 | 14.307 | 14.303 | 22.9 | 60.4 | 14.309 | 14.298 | 37.3 | 70.6 | 501.8 | 65.6 | 31.1 | 12.1 | -9.8 | | |
| 2353 | 81.0 | 14.308 | 14.302 | 25.7 | 70.5 | 14.306 | 14.295 | 36.0 | 80.7 | 502.2 | 75.7 | 39.1 | 8.1 | -5.9 | | |
| 2354 | 90.6 | 14.306 | 14.301 | 24.5 | 80.1 | 14.304 | 14.293 | 36.0 | 90.4 | 502.3 | 85.4 | 37.7 | 6.3 | -8.1 | | |
| 2355 | 100.5 | 14.305 | 14.301 | 22.5 | 90.0 | 14.303 | 14.293 | 35.7 | 100.3 | 502.5 | 95.3 | 38.4 | 5.3 | -9.1 | | |
| 2356 | 110.8 | 14.304 | 14.300 | 22.0 | 100.3 | 14.303 | 14.292 | 36.2 | 110.5 | 502.6 | 105.5 | 38.7 | 5.1 | -9.5 | | |
| 2357 | 120.5 | 14.304 | 14.299 | 22.9 | 110.0 | 14.303 | 14.291 | 37.9 | 120.3 | 502.0 | 115.3 | 39.2 | 5.2 | -7.9 | | |
| 2358 | 130.9 | 14.306 | 14.301 | 24.4 | 120.4 | 14.303 | 14.291 | 37.8 | 130.6 | 502.0 | 125.6 | 40.2 | 5.3 | -7.9 | | |
| 2359 | 140.9 | 14.305 | 14.301 | 23.1 | 130.4 | 14.304 | 14.292 | 37.5 | 140.7 | 501.3 | 135.7 | 39.5 | 4.0 | -8.0 | | |
| 2360 | 150.8 | 14.305 | 14.300 | 23.4 | 140.3 | 14.304 | 14.292 | 37.4 | 150.5 | 501.6 | 145.5 | 38.9 | 3.0 | -7.2 | | |
| 2361 | 161.0 | 14.303 | 14.299 | 21.2 | 150.5 | 14.303 | 14.292 | 37.0 | 160.7 | 502.3 | 155.7 | 39.0 | 1.8 | -8.8 | | |
| 2362 | 170.6 | 14.302 | 14.299 | 19.5 | 160.1 | 14.300 | 14.290 | 35.0 | 170.3 | 502.2 | 165.3 | 38.3 | -1 | -8.5 | | |
| 2363 | 180.7 | 14.302 | 14.300 | 17.7 | 170.2 | 14.303 | 14.291 | 38.3 | 180.5 | 502.1 | 175.5 | 37.7 | -7 | -10.7 | | |
| 2364 | 190.7 | 14.301 | 14.299 | 15.6 | 180.2 | 14.304 | 14.291 | 39.1 | 190.4 | 501.9 | 185.4 | 41.0 | -2.8 | -9.0 | | |
| 2365 | 200.8 | 14.301 | 14.299 | 14.6 | 190.3 | 14.306 | 14.292 | 40.5 | 200.6 | 501.7 | 195.6 | 42.3 | -3.8 | -8.2 | | |
| 2366 | 211.1 | 14.302 | 14.300 | 15.4 | 200.6 | 14.306 | 14.293 | 39.8 | 210.8 | 501.8 | 205.8 | 42.9 | -4.7 | -7.8 | | |
| 2367 | 220.6 | 14.301 | 14.299 | 12.6 | 210.1 | 14.304 | 14.292 | 38.2 | 220.3 | 501.5 | 215.3 | 41.2 | -6.2 | -8.1 | | |
| 2368 | 231.0 | 14.300 | 14.299 | 11.4 | 220.5 | 14.303 | 14.292 | 35.5 | 230.7 | 500.9 | 225.7 | 38.0 | -6.6 | -7.9 | | |
| 2369 | 240.8 | 14.300 | 14.300 | 8.2 | 230.3 | 14.303 | 14.292 | 35.4 | 240.6 | 500.7 | 235.6 | 36.4 | -7.3 | -7.8 | | |
| 2370 | 251.1 | 14.300 | 14.299 | 8.8 | 240.6 | 14.303 | 14.293 | 34.6 | 250.9 | 500.6 | 245.9 | 37.0 | -8.6 | -8.0 | | |
| 2371 | 260.9 | 14.300 | 14.300 | 5.6 | 250.4 | 14.301 | 14.293 | 32.6 | 260.6 | 500.1 | 255.6 | 35.5 | -9.8 | -7.8 | | |
| 2372 | 270.7 | 14.300 | 14.300 | 0.0 | 260.2 | 14.301 | 14.293 | 30.7 | 270.4 | 499.6 | 265.4 | 33.1 | -11.3 | -7.3 | | |
| 2373 | 280.6 | 14.299 | 14.299 | 0.0 | 270.1 | 14.299 | 14.293 | 27.7 | 280.3 | 500.2 | 275.3 | 29.8 | -12.6 | -9.9 | | |
| 2374 | 290.6 | 14.299 | 14.300 | 0.0 | 280.1 | 14.301 | 14.293 | 30.7 | 290.4 | 500.5 | 285.4 | 34.2 | -11.8 | -7.7 | | |

TABLE 35.—Concluded.

| Reading number | Probe one | | | | Probe two | | | | Thermocouple | | | | Wind anemometer | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|-----------------|----------|--|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg | |
| 2375 | 300.7 | 14.300 | 14.300 | 0.0 | 290.2 | 14.301 | 14.294 | 29.9 | 300.5 | 500.5 | 295.5 | 32.5 | -12.0 | -7.4 | |
| 2376 | 310.3 | 14.302 | 14.302 | 0.0 | 299.8 | 14.301 | 14.295 | 28.7 | 310.1 | 500.8 | 305.1 | 31.5 | -13.1 | -7.2 | |
| 2377 | 315.9 | 14.301 | 14.301 | 0.0 | 305.4 | 14.301 | 14.294 | 27.7 | 315.7 | 500.8 | 310.7 | 30.6 | -11.9 | -7.1 | |
| 2378 | 295.9 | 14.300 | 14.300 | 0.0 | 285.4 | 14.300 | 14.292 | 30.3 | 295.6 | 500.4 | 290.6 | 33.3 | -12.6 | -8.2 | |
| 2379 | 276.2 | 14.300 | 14.300 | 0.0 | 265.7 | 14.299 | 14.292 | 28.3 | 276.0 | 500.1 | 271.0 | 31.4 | -12.0 | -8.3 | |
| 2380 | 255.6 | 14.299 | 14.299 | 6.5 | 245.1 | 14.301 | 14.292 | 33.8 | 255.3 | 499.9 | 250.3 | 36.4 | -9.3 | -7.7 | |
| 2381 | 235.8 | 14.299 | 14.298 | 10.3 | 225.3 | 14.301 | 14.291 | 35.0 | 235.6 | 499.9 | 230.6 | 36.7 | -6.9 | -7.6 | |
| 2382 | 215.6 | 14.299 | 14.298 | 13.6 | 205.1 | 14.304 | 14.291 | 39.2 | 215.4 | 500.6 | 210.4 | 42.5 | -5.7 | -8.1 | |
| 2383 | 195.6 | 14.300 | 14.298 | 14.8 | 185.1 | 14.303 | 14.290 | 39.9 | 195.3 | 500.9 | 190.3 | 41.4 | -3.3 | -9.2 | |
| 2384 | 175.7 | 14.300 | 14.296 | 20.0 | 165.2 | 14.300 | 14.289 | 36.3 | 175.5 | 500.9 | 170.5 | 36.7 | -5 | -10.8 | |
| 2385 | 155.8 | 14.301 | 14.298 | 21.3 | 145.3 | 14.301 | 14.289 | 37.1 | 155.5 | 501.2 | 150.5 | 39.0 | 1.8 | -7.9 | |
| 2386 | 135.6 | 14.302 | 14.297 | 24.0 | 125.1 | 14.300 | 14.289 | 37.5 | 135.3 | 501.2 | 130.3 | 39.7 | 4.8 | -8.3 | |
| 2387 | 115.8 | 14.303 | 14.299 | 22.7 | 105.3 | 14.301 | 14.290 | 37.4 | 115.6 | 501.3 | 110.6 | 39.9 | 5.6 | -8.8 | |
| 2388 | 95.8 | 14.304 | 14.300 | 23.6 | 85.3 | 14.301 | 14.290 | 35.5 | 95.6 | 501.4 | 90.6 | 38.9 | 5.6 | -8.8 | |
| 2389 | 75.8 | 14.304 | 14.300 | 22.6 | 65.3 | 14.303 | 14.292 | 37.3 | 75.5 | 501.6 | 70.5 | 36.4 | 10.0 | -7.4 | |
| 2390 | 55.6 | 14.304 | 14.301 | 20.0 | 45.1 | 14.298 | 14.292 | 26.6 | 55.4 | 502.1 | 50.4 | 27.8 | 13.2 | -8.3 | |

TABLE 36.—DATA LISTING FOR TRAVERSE 2 AT STATION 6—LOWER HORIZONTAL SURVEY
 [Test section data for reading 2350; total pressure, 14.324; static pressure, 13.227 psi; total temperature, 500°R; velocity, 250.7 mph; fan speed, 286.2 rpm.]

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 2350 | 50.9 | 14.310 | 14.307 | 20.4 | 40.7 | 14.311 | 14.304 | 28.6 | 49.2 | 498.1 | 43.2 | 28.9 | 13.3 | 14.8 |
| 2351 | 60.5 | 14.310 | 14.304 | 27.6 | 50.3 | 14.311 | 14.304 | 29.0 | 58.8 | 497.9 | 52.8 | 29.9 | 13.0 | 6.8 |
| 2352 | 70.2 | 14.311 | 14.304 | 28.0 | 60.0 | 14.314 | 14.304 | 68.5 | 497.2 | 62.5 | 33.1 | 8.8 | 1.8 | |
| 2353 | 80.7 | 14.313 | 14.304 | 34.2 | 70.4 | 14.315 | 14.304 | 36.3 | 78.9 | 496.9 | 72.9 | 38.0 | 11.0 | 8.1 |
| 2354 | 90.3 | 14.315 | 14.305 | 34.9 | 80.1 | 14.315 | 14.304 | 36.5 | 88.6 | 497.3 | 82.6 | 39.8 | 15.6 | 8.5 |
| 2355 | 101.1 | 14.314 | 14.303 | 36.3 | 90.9 | 14.315 | 14.304 | 37.1 | 99.4 | 497.9 | 93.4 | 38.0 | 10.0 | -0.2 |
| 2356 | 110.8 | 14.315 | 14.304 | 36.5 | 100.5 | 14.316 | 14.304 | 37.7 | 109.0 | 497.8 | 103.0 | 38.9 | 4.2 | .3 |
| 2357 | 120.2 | 14.316 | 14.304 | 37.4 | 109.9 | 14.316 | 14.304 | 38.5 | 118.4 | 497.6 | 112.4 | 42.4 | 3.0 | 3.7 |
| 2358 | 130.4 | 14.315 | 14.303 | 38.0 | 120.1 | 14.314 | 14.303 | 37.9 | 128.6 | 498.0 | 122.6 | 42.8 | 3.4 | 4.9 |
| 2359 | 140.3 | 14.315 | 14.304 | 37.3 | 130.0 | 14.315 | 14.303 | 38.2 | 138.5 | 496.2 | 132.5 | 43.1 | 3.7 | 6.2 |
| 2360 | 150.5 | 14.314 | 14.303 | 37.6 | 140.3 | 14.317 | 14.302 | 41.1 | 148.8 | 495.0 | 142.8 | 44.8 | 3.4 | 8.7 |
| 2361 | 160.6 | 14.317 | 14.303 | 40.3 | 150.4 | 14.317 | 14.303 | 39.6 | 158.9 | 494.4 | 152.9 | 44.1 | 3.1 | 9.4 |
| 2362 | 170.2 | 14.316 | 14.303 | 39.7 | 160.0 | 14.312 | 14.302 | 34.9 | 168.5 | 494.7 | 162.5 | 42.6 | 1.6 | 9.7 |
| 2363 | 180.6 | 14.313 | 14.303 | 34.6 | 170.4 | 14.316 | 14.304 | 39.1 | 178.9 | 494.9 | 172.9 | 41.1 | -1.6 | 9.0 |
| 2364 | 190.4 | 14.316 | 14.303 | 38.6 | 180.1 | 14.316 | 14.303 | 38.8 | 188.6 | 495.9 | 182.6 | 43.3 | -2.9 | 6.9 |
| 2365 | 200.5 | 14.316 | 14.303 | 38.7 | 190.3 | 14.317 | 14.304 | 39.5 | 198.8 | 495.4 | 192.8 | 44.1 | -3.3 | 6.3 |
| 2366 | 210.6 | 14.316 | 14.303 | 39.2 | 200.3 | 14.316 | 14.304 | 38.3 | 208.8 | 496.4 | 202.8 | 43.9 | -4.3 | 6.0 |
| 2367 | 220.4 | 14.315 | 14.303 | 38.1 | 210.1 | 14.315 | 14.303 | 37.1 | 218.6 | 497.0 | 212.6 | 42.6 | -4.8 | 6.9 |
| 2368 | 230.7 | 14.315 | 14.304 | 36.7 | 220.4 | 14.315 | 14.304 | 36.4 | 228.9 | 496.4 | 222.9 | 41.3 | -6.2 | 7.2 |
| 2369 | 240.5 | 14.314 | 14.303 | 35.8 | 230.3 | 14.314 | 14.303 | 36.1 | 238.8 | 495.3 | 232.8 | 40.6 | -7.2 | 6.2 |
| 2370 | 250.8 | 14.314 | 14.303 | 35.7 | 240.5 | 14.314 | 14.304 | 34.7 | 249.0 | 494.7 | 243.0 | 40.0 | -8.8 | 6.9 |
| 2371 | 260.6 | 14.313 | 14.303 | 34.5 | 250.4 | 14.312 | 14.303 | 32.0 | 258.9 | 495.9 | 252.9 | 38.7 | -10.4 | 6.5 |
| 2372 | 270.5 | 14.313 | 14.305 | 31.7 | 260.3 | 14.312 | 14.304 | 31.8 | 268.8 | 495.2 | 262.8 | 37.6 | -10.8 | 8.3 |
| 2373 | 280.8 | 14.312 | 14.304 | 31.1 | 270.5 | 14.311 | 14.304 | 28.2 | 279.0 | 495.1 | 273.0 | 31.5 | -12.6 | 9.7 |
| 2374 | 290.6 | 14.310 | 14.304 | 27.4 | 280.3 | 14.312 | 14.305 | 29.1 | 288.8 | 495.4 | 282.8 | 36.1 | -12.9 | 9.5 |

TABLE 36.—Concluded.

| Reading number | Probe one | | | Probe two | | | Thermocouple | | | Wind anemometer | | | | |
|----------------|---------------|----------------------|-----------------------|------------------|---------------|----------------------|-----------------------|------------------|---------------|-----------------------|---------------|------------------|------------|----------|
| | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total pressure, psia | Static pressure, psia | Velocity, ft/sec | Position, in. | Total temperature, °R | Position, in. | Velocity, ft/sec | Pitch, deg | Yaw, deg |
| 2375 | 300.5 | 14.311 | 14.304 | 28.8 | 290.3 | 14.312 | 14.305 | 28.3 | 298.8 | 494.6 | 292.8 | 33.4 | -14.0 | 8.3 |
| 2376 | 310.2 | 14.312 | 14.306 | 28.1 | 299.9 | 14.312 | 14.305 | 26.8 | 308.4 | 492.5 | 302.4 | 30.5 | -14.4 | 7.9 |
| 2377 | 315.6 | 14.312 | 14.305 | 27.1 | 305.3 | 14.311 | 14.306 | 25.5 | 313.8 | 490.6 | 307.8 | 29.1 | -14.4 | 7.9 |
| 2378 | 295.5 | 14.311 | 14.304 | 29.6 | 285.3 | 14.312 | 14.305 | 28.8 | 293.8 | 494.4 | 287.8 | 34.7 | -14.1 | 8.3 |
| 2379 | 275.9 | 14.311 | 14.303 | 30.8 | 265.6 | 14.311 | 14.304 | 28.8 | 274.1 | 494.5 | 268.1 | 35.6 | -12.6 | 9.3 |
| 2380 | 255.9 | 14.313 | 14.302 | 35.3 | 245.6 | 14.313 | 14.304 | 33.1 | 254.1 | 495.0 | 248.1 | 40.4 | -9.8 | 6.6 |
| 2381 | 235.5 | 14.313 | 14.302 | 36.1 | 225.2 | 14.314 | 14.303 | 36.0 | 233.7 | 495.6 | 227.7 | 41.4 | -7.1 | 6.6 |
| 2382 | 215.5 | 14.315 | 14.303 | 39.2 | 205.2 | 14.316 | 14.304 | 38.2 | 213.7 | 496.7 | 207.7 | 43.7 | -4.5 | 6.1 |
| 2383 | 195.4 | 14.315 | 14.302 | 39.0 | 185.1 | 14.317 | 14.305 | 39.1 | 193.6 | 495.7 | 187.6 | 44.6 | -3.8 | 6.4 |
| 2384 | 175.3 | 14.314 | 14.301 | 38.6 | 165.1 | 14.314 | 14.303 | 36.0 | 173.6 | 495.0 | 167.6 | 39.9 | -3 | 10.9 |
| 2385 | 155.8 | 14.316 | 14.302 | 40.2 | 145.6 | 14.318 | 14.304 | 41.2 | 154.1 | 494.6 | 148.1 | 45.4 | 2.0 | 9.6 |
| 2386 | 135.4 | 14.316 | 14.304 | 37.9 | 125.2 | 14.317 | 14.305 | 37.5 | 133.7 | 497.4 | 127.7 | 43.5 | 3.7 | 6.2 |
| 2387 | 115.7 | 14.316 | 14.304 | 37.3 | 105.5 | 14.317 | 14.305 | 38.1 | 114.0 | 498.3 | 108.0 | 41.1 | 1.6 | 1.8 |
| 2388 | 95.5 | 14.316 | 14.305 | 36.1 | 85.2 | 14.317 | 14.306 | 36.1 | 93.7 | 496.6 | 87.7 | 37.6 | 13.5 | 3.1 |
| 2389 | 75.7 | 14.313 | 14.305 | 31.2 | 65.5 | 14.316 | 14.305 | 35.2 | 74.0 | 495.9 | 68.0 | 37.2 | 9.5 | 4.6 |
| 2390 | 55.7 | 14.310 | 14.305 | 23.6 | 45.4 | 14.313 | 14.307 | 27.2 | 53.9 | 497.8 | 47.9 | 32.5 | 13.1 | 13.4 |

TABLE 37.—TEST MATRIX

| Test section air speed, V_{TS} , mph | Tunnel total temperature, $T_{D,\text{avg}}$, °F | Temperature condition | Traverse | Traverse position above floor, Z, in. |
|---|--|-----------------------|----------|---------------------------------------|
| 350 | 48 | Warm | No | 79 |
| 350 | 15 | Outside air matched | No | 79 |
| 300 | 15 | Outside air matched | No | 79 |
| 250 | 14 | Outside air matched | No | 79 |
| 200 | 15 | Outside air matched | No | 79 |
| 350 | -17 | Cold | No | 79 |
| 250 | 14 | Outside air matched | Yes | 0 to 314 |
| 350 | -17 | Cold | Yes | 0 to 314 |

TABLE 38.—TEST MATRIX

| Traverse position, Z, in. | Test section air speed, V_{TS} , mph | Test section blockage | Total temperature, $T_{D,\text{avg}}$, °F |
|---------------------------|--|--|--|
| 18.25 | 100, 150, 200, 250, 300 | Blockage plate at 55°; no blockage plate | 60 to 70 |
| 42.1 | 100, 150, 200, 250, 300 | Blockage plate at 55°; no blockage plate | 60 to 70 |
| 67.5 | 100, 150, 200, 250, 300 | Blockage plate at 55°; no blockage plate | 60 to 70 |

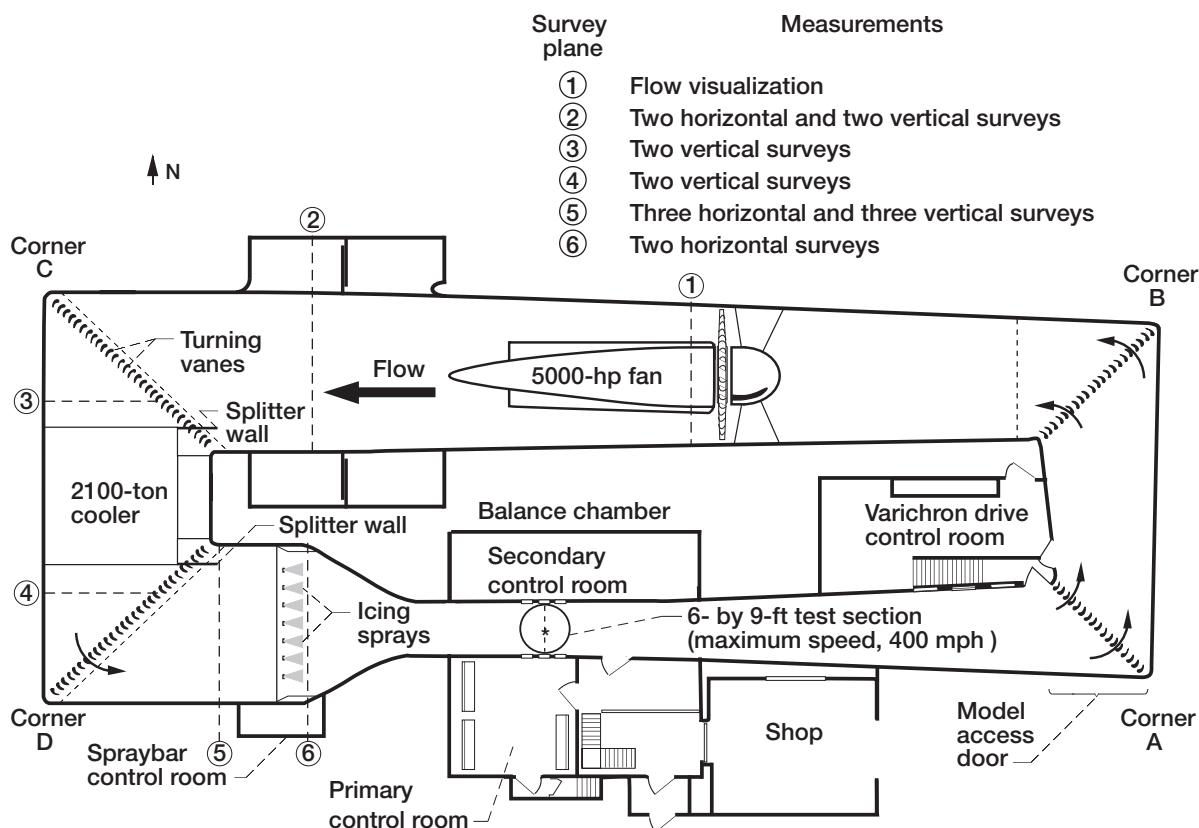


Figure 1.—Plan view of Icing Research Tunnel, shop, and control room showing tunnel loop survey planes.

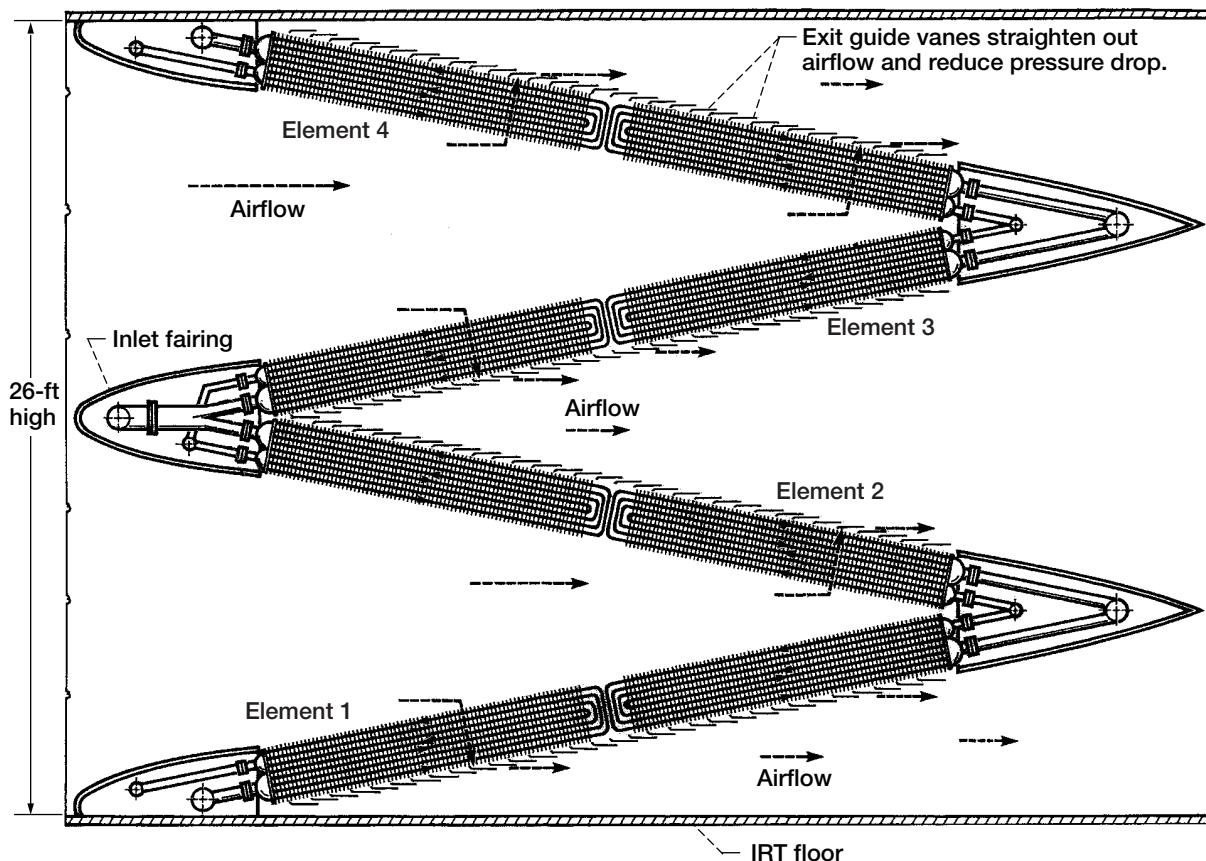


Figure 2.—Elevation view of cooler in IRT.

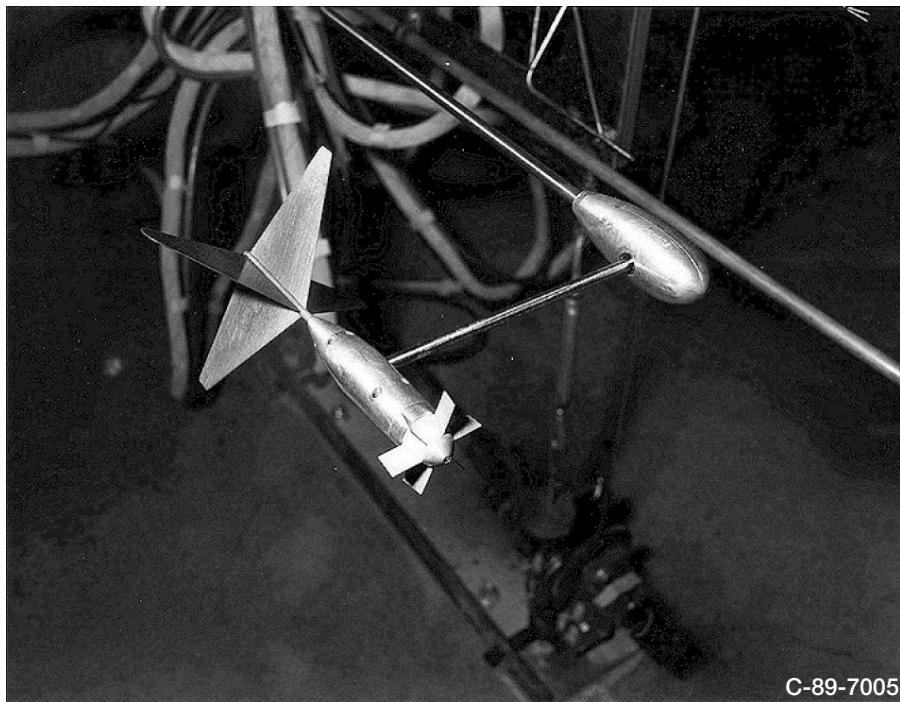


Figure 3.—Typical wind anemometer used on traversing plates during IRT flow quality studies.

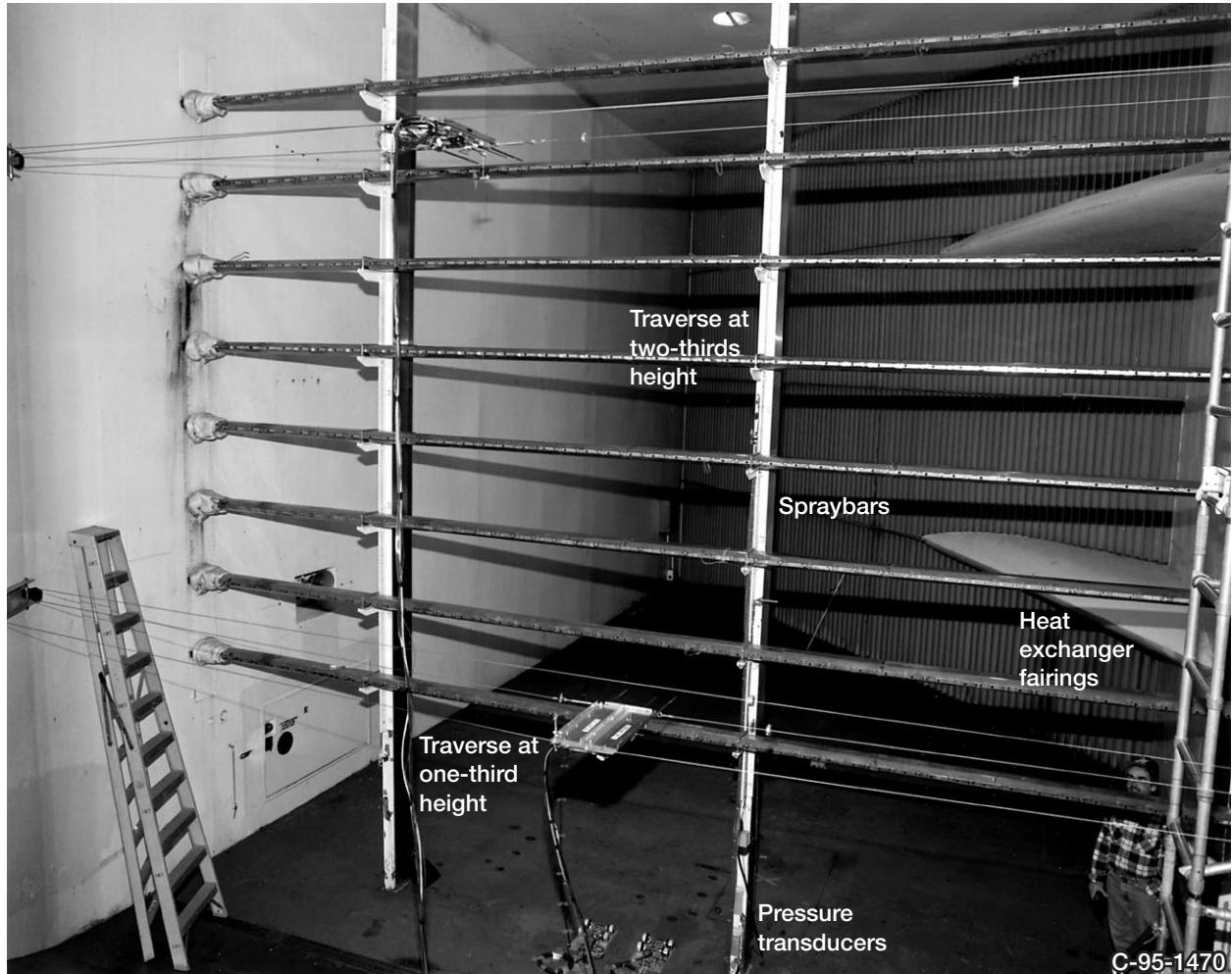


Figure 4.—Setup (at station 6, downstream of spraybars) showing typical flow field survey installation with traversing plates.

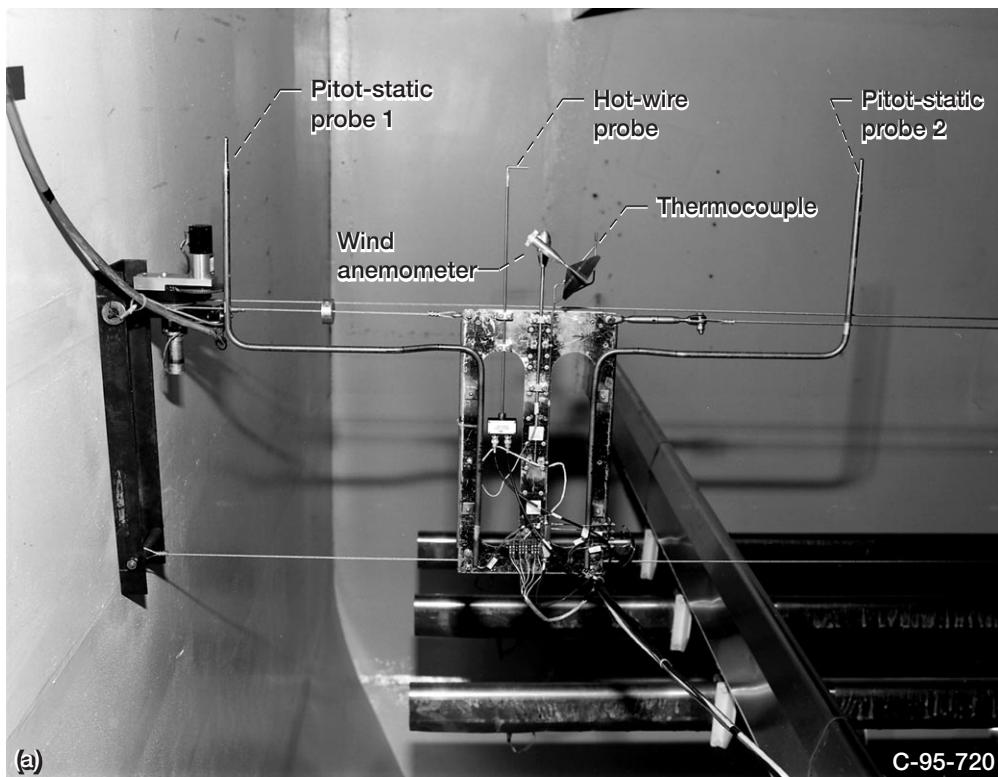


Figure 5.—Instrumentation configuration on traversing plates during tunnel-loop flow quality surveys. (a) Configuration 1, used at stations 4 and 5 for runs 1 to 10 (actual installation at station 5—horizontal, view from floor). (b) Configuration 2, used at stations 2, 3, 5, and 6 (actual installation at station 2—vertical, view from outside tunnel wall).

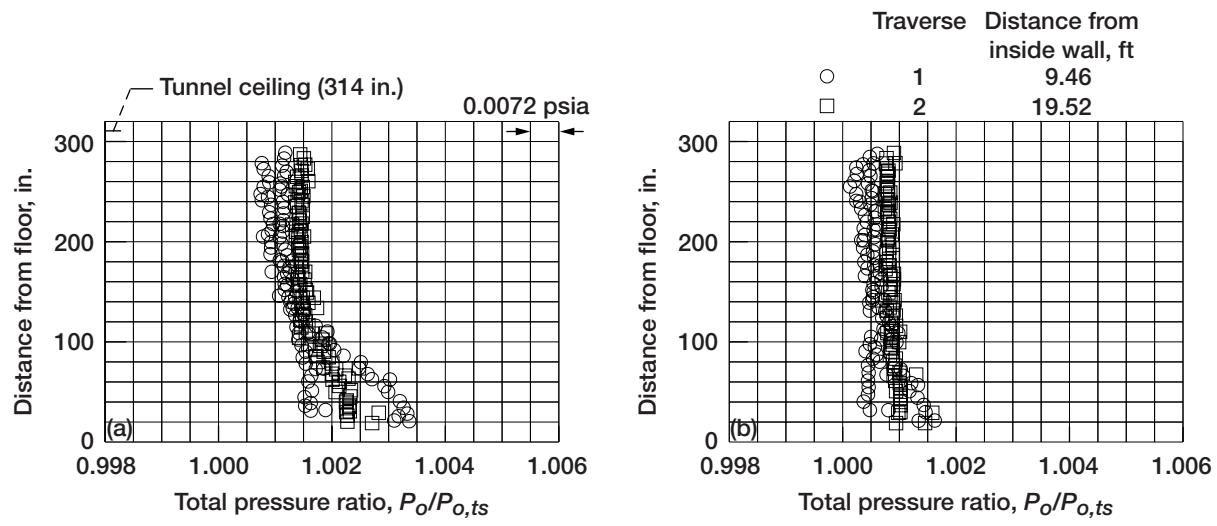


Figure 6.—Total pressure ratio distributions along vertical surveys downstream of drive motor housing (station 2). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

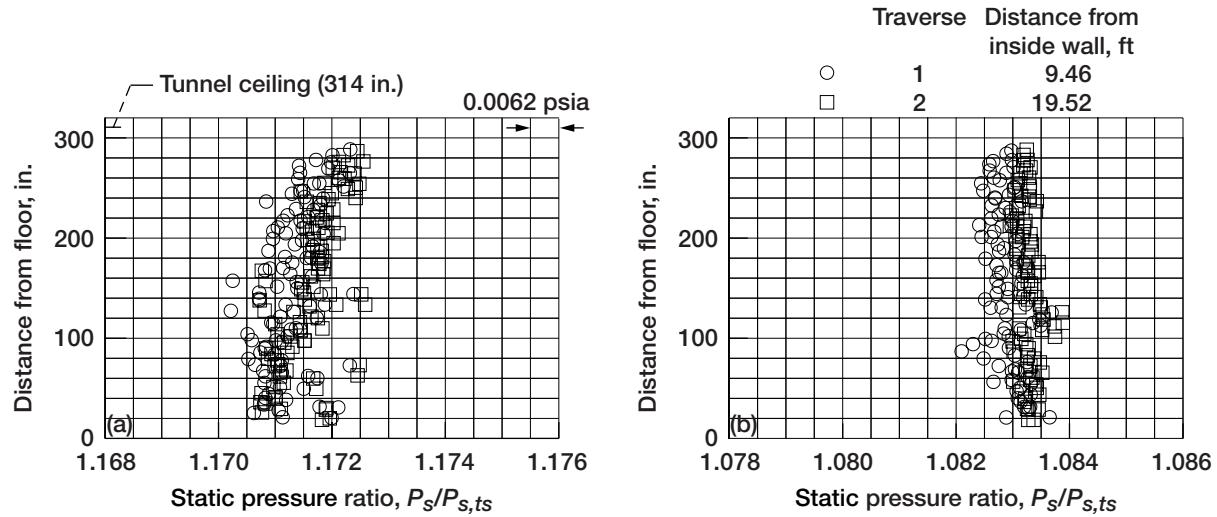


Figure 7.—Static pressure ratio distributions along vertical surveys downstream of drive motor housing (station 2). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

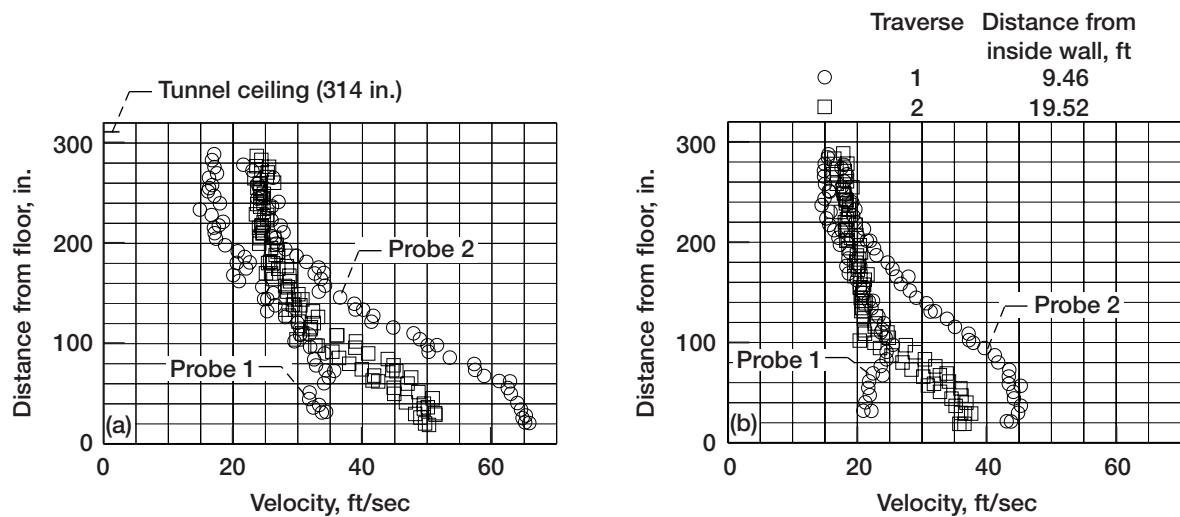


Figure 8.—Velocity distribution measured by pitot-static probes along vertical surveys downstream of drive motor housing (station 2). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

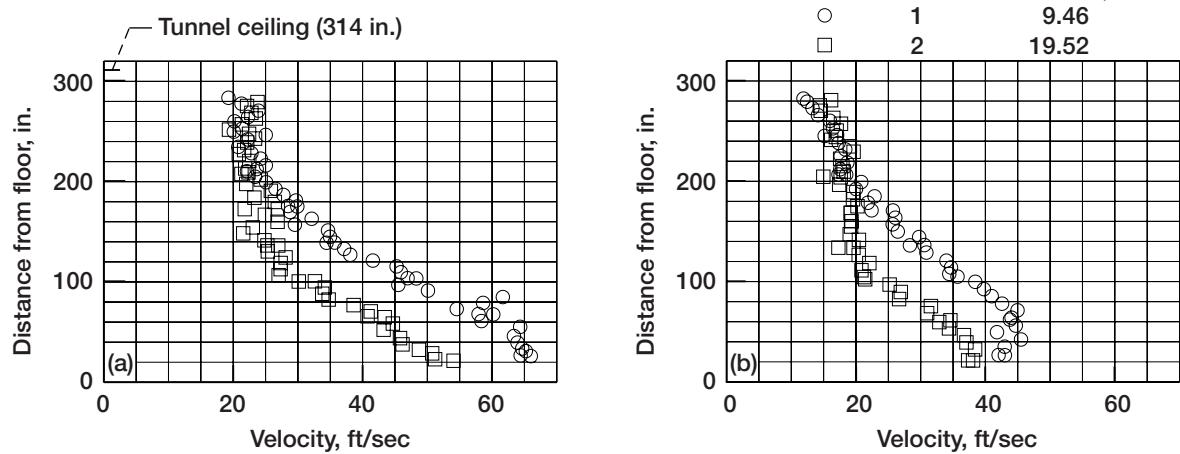


Figure 9.—Velocity distribution measured by wind anemometers along vertical surveys downstream of drive motor housing (station 2). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

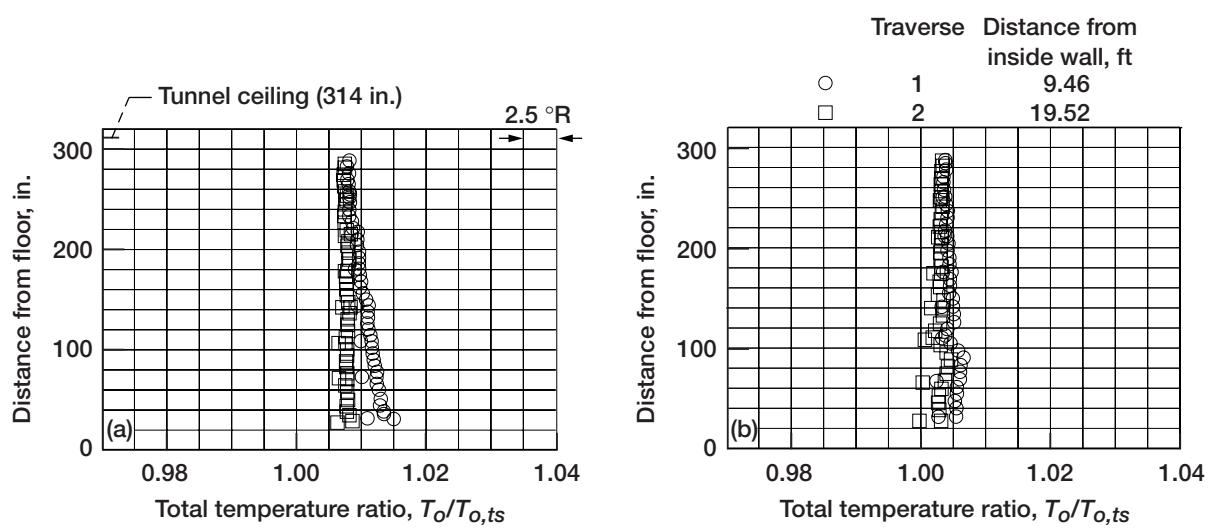


Figure 10.—Total temperature ratio distribution along vertical surveys downstream of drive motor housing (station 2). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.



Figure 11.—IRT fan exit as viewed from corner C of tunnel (i.e., looking upstream, see fig. 1). Direction of fan rotation and components of swirl are indicated. Traverse 1 position was to the right (inside wall) and traverse 2 to the left. Pitch angle is defined as positive for upflow; positive yaw angle is from inside wall toward outside wall.

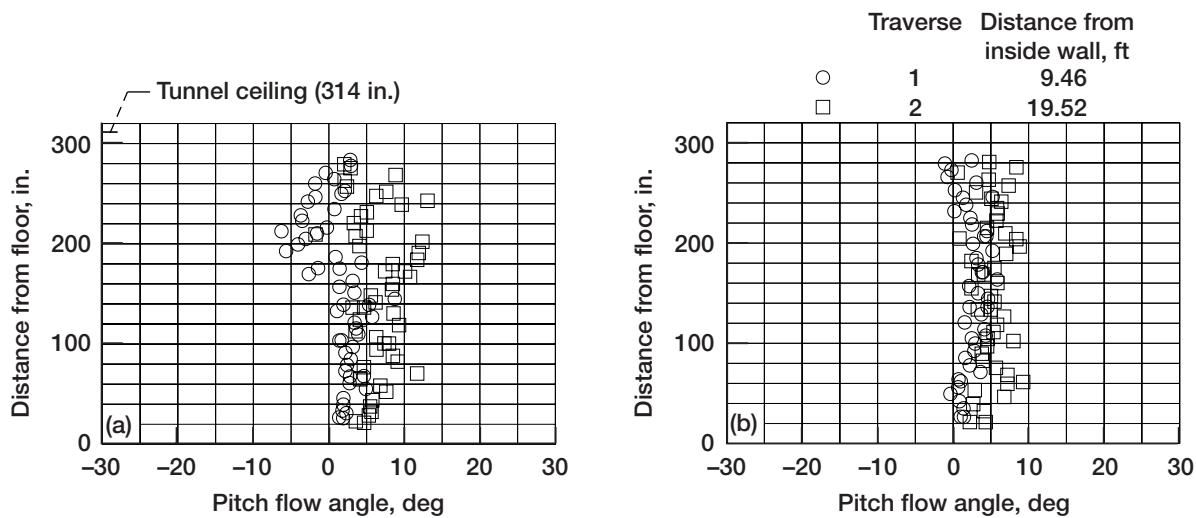


Figure 12.—Pitch flow angle distribution (positive indicates upflow; negative indicates downflow) along vertical surveys downstream of drive motor housing (station 2). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

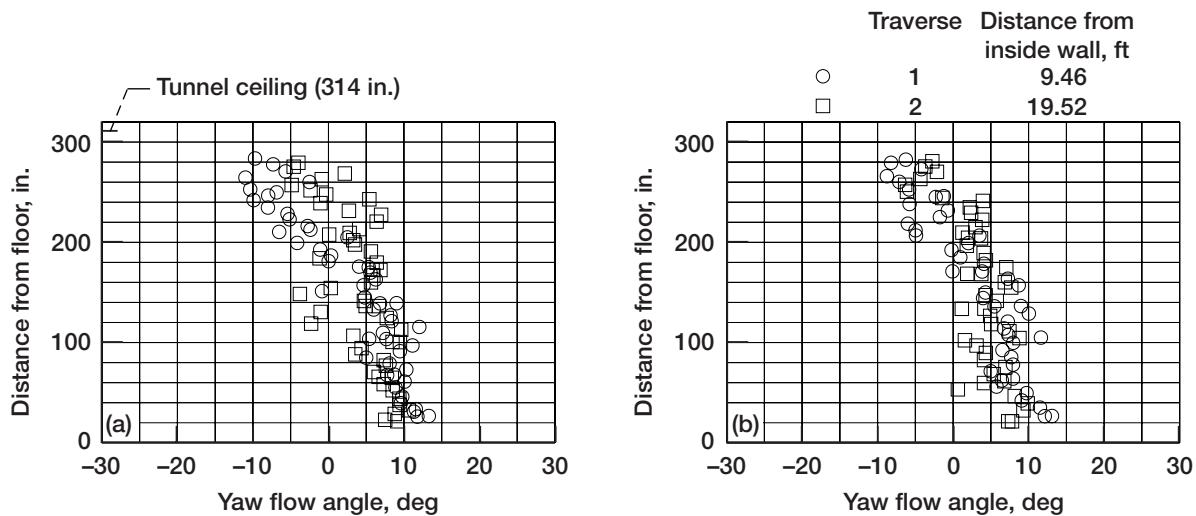


Figure 13.—Yaw flow angle distribution (positive = flow from inside wall to outside wall (outflow); negative = flow from outside to inside wall (inflow)) along vertical surveys downstream of drive motor housing (station 2). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

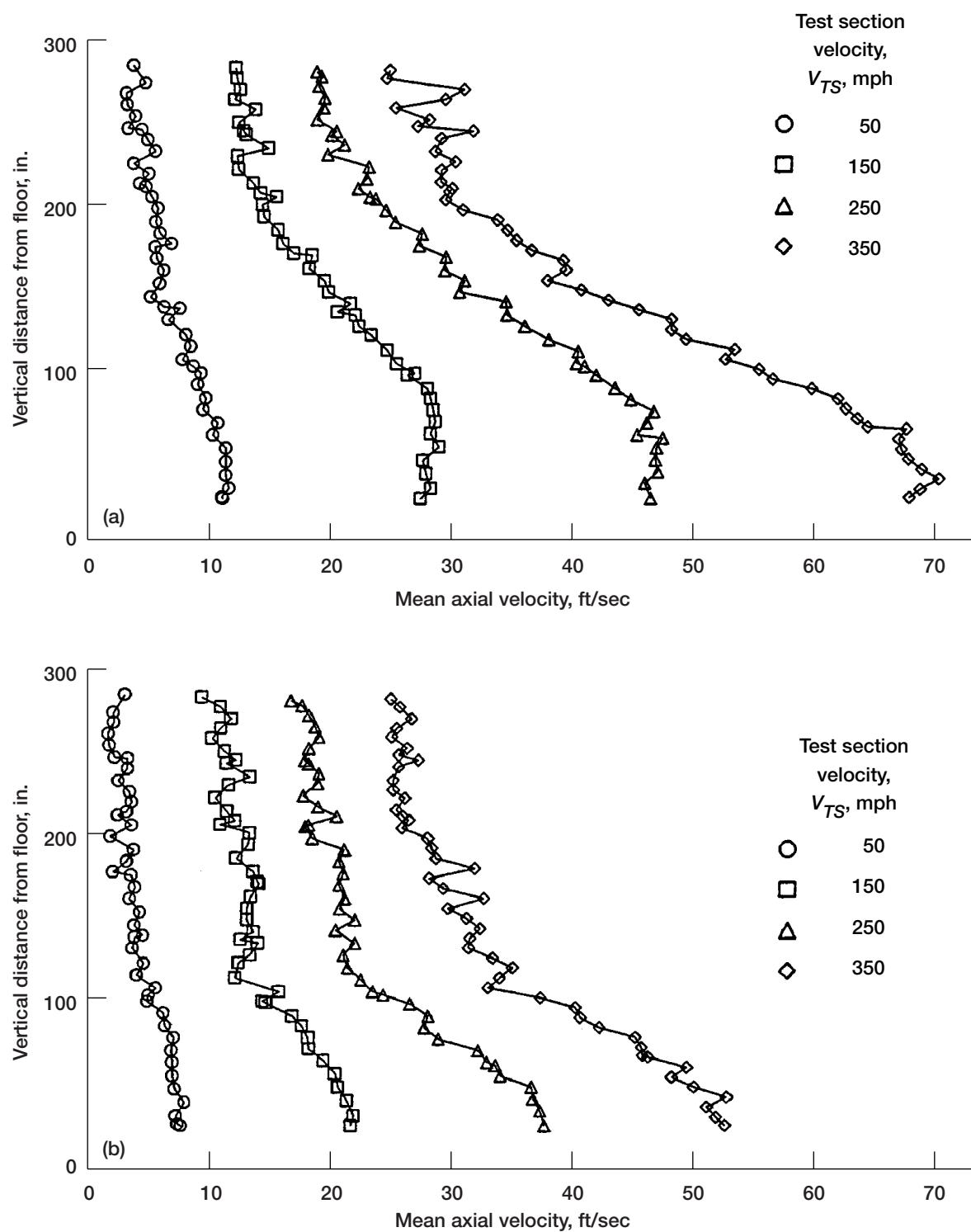


Figure 14.—Mean axial velocity distributions along vertical surveys downstream of drive motor housing (station 2) as measured by hot-wire anemometers. (a) Traverse 1 (9.46 ft from inside wall). (b) Traverse 2 (19.52 ft from inside wall).

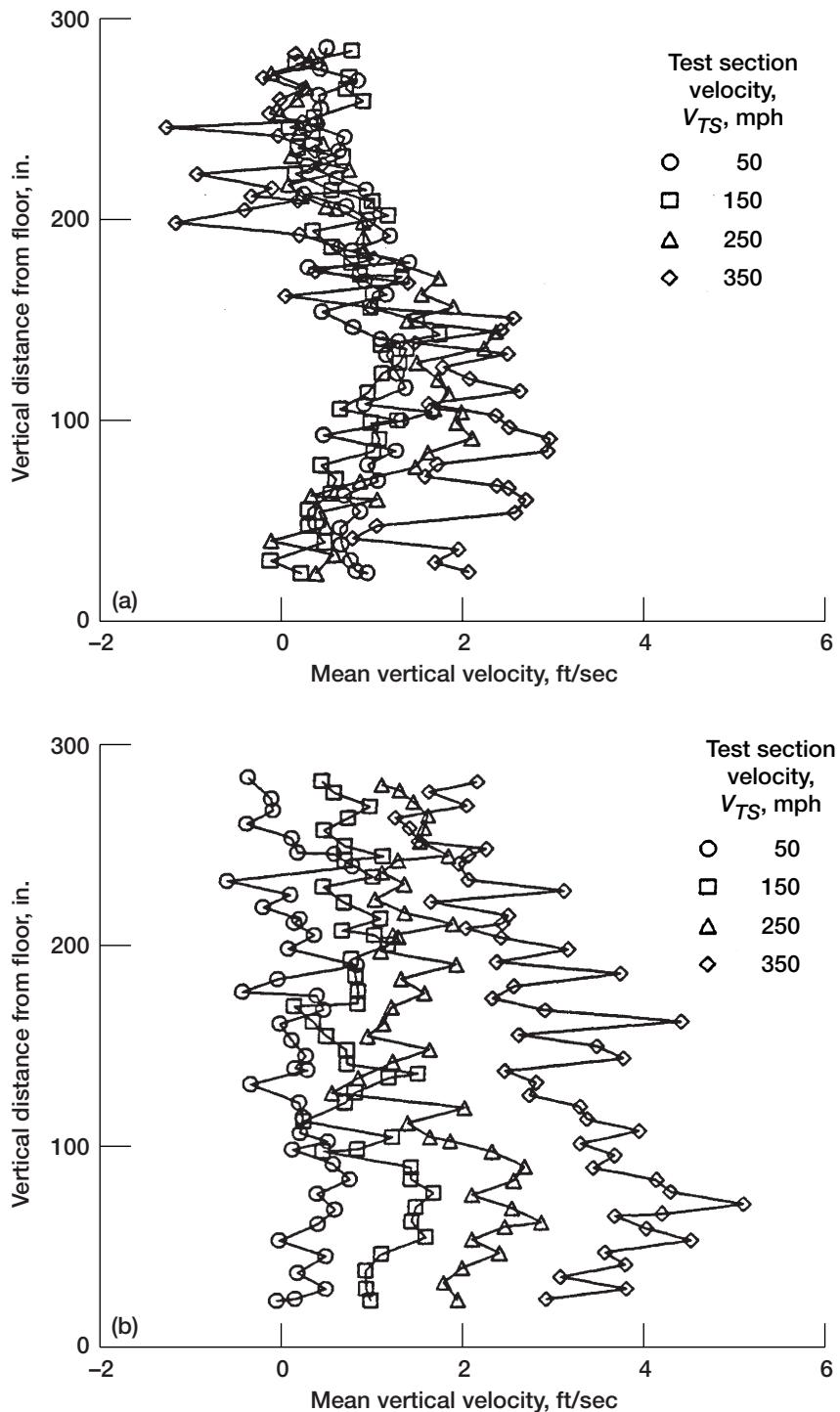


Figure 15.—Mean vertical velocity distributions along vertical surveys downstream of drive motor housing (station 2) as measured by hot-wire anemometers. (a) Traverse 1 (9.46 ft from inside wall). (b) Traverse 2 (19.52 ft from inside wall).

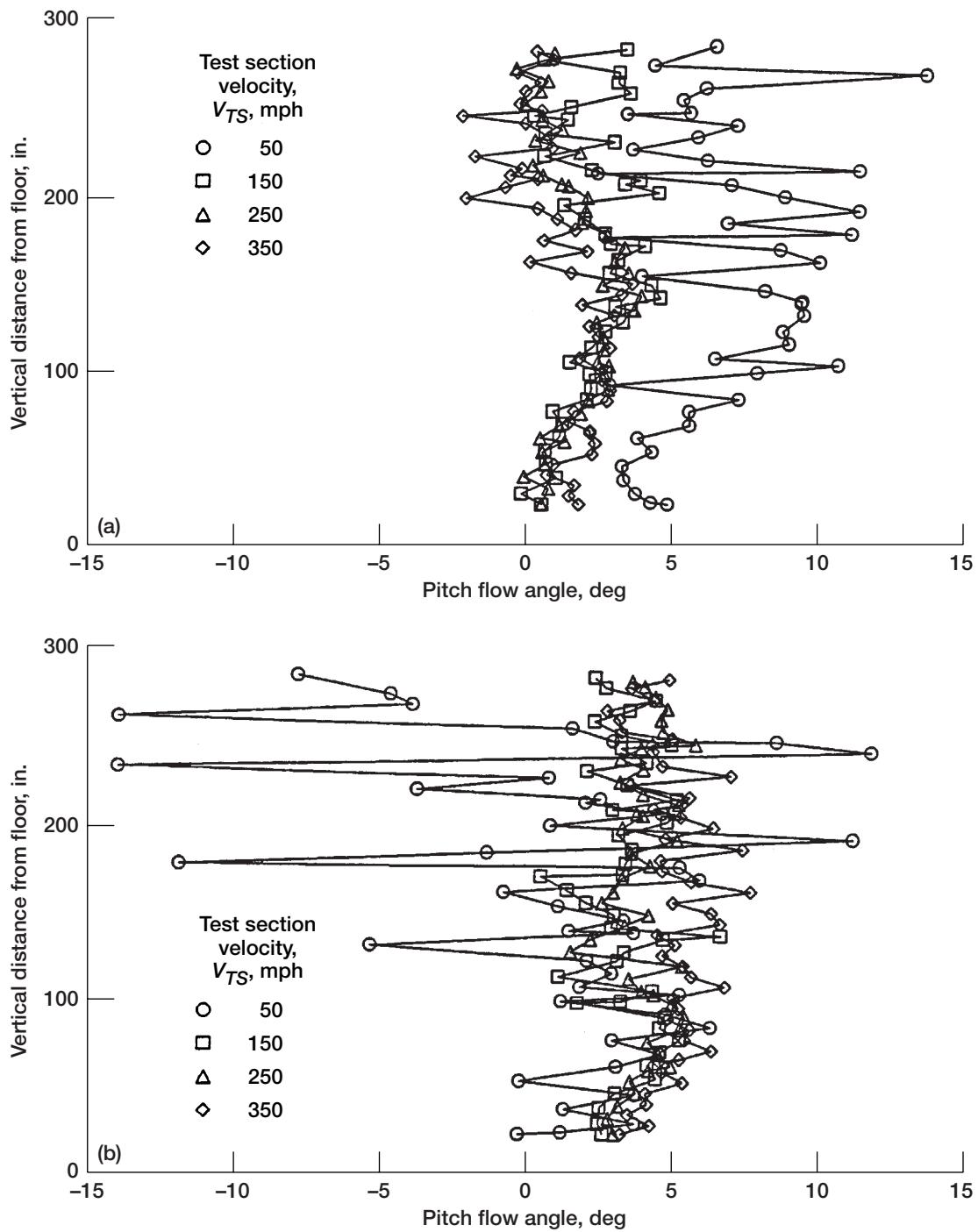


Figure 16.—Pitch flow angle distribution along vertical surveys downstream of drive motor housing (station 2). (a) Traverse 1 (9.46 ft from inside wall). (b) Traverse 2 (19.52 ft from inside wall).

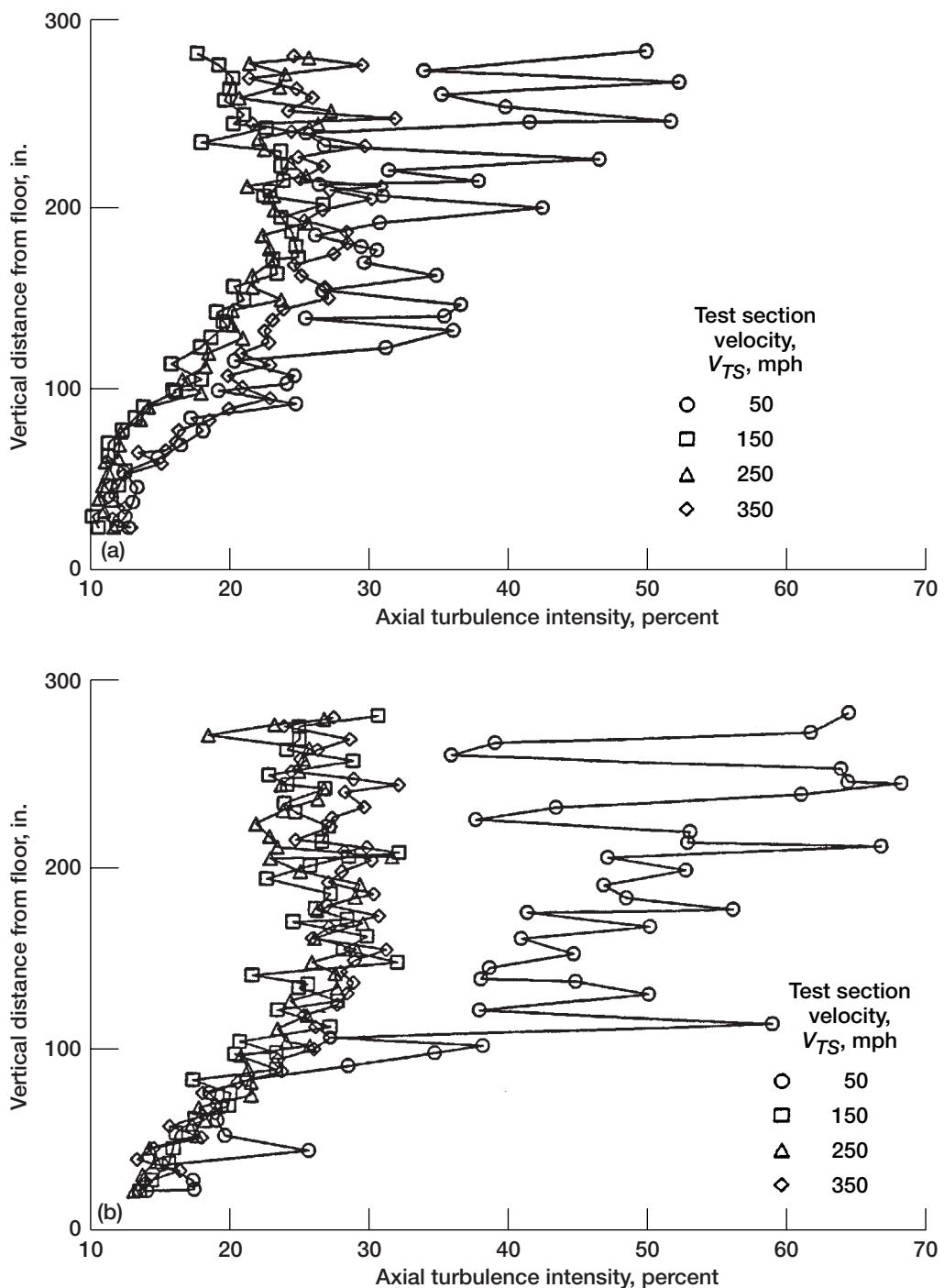


Figure 17.—Axial turbulence intensity distribution along vertical surveys downstream of drive motor housing (station 2). (a) Traverse 1 (9.46 ft from inside wall). (b) Traverse 2 (19.52 ft from inside wall).

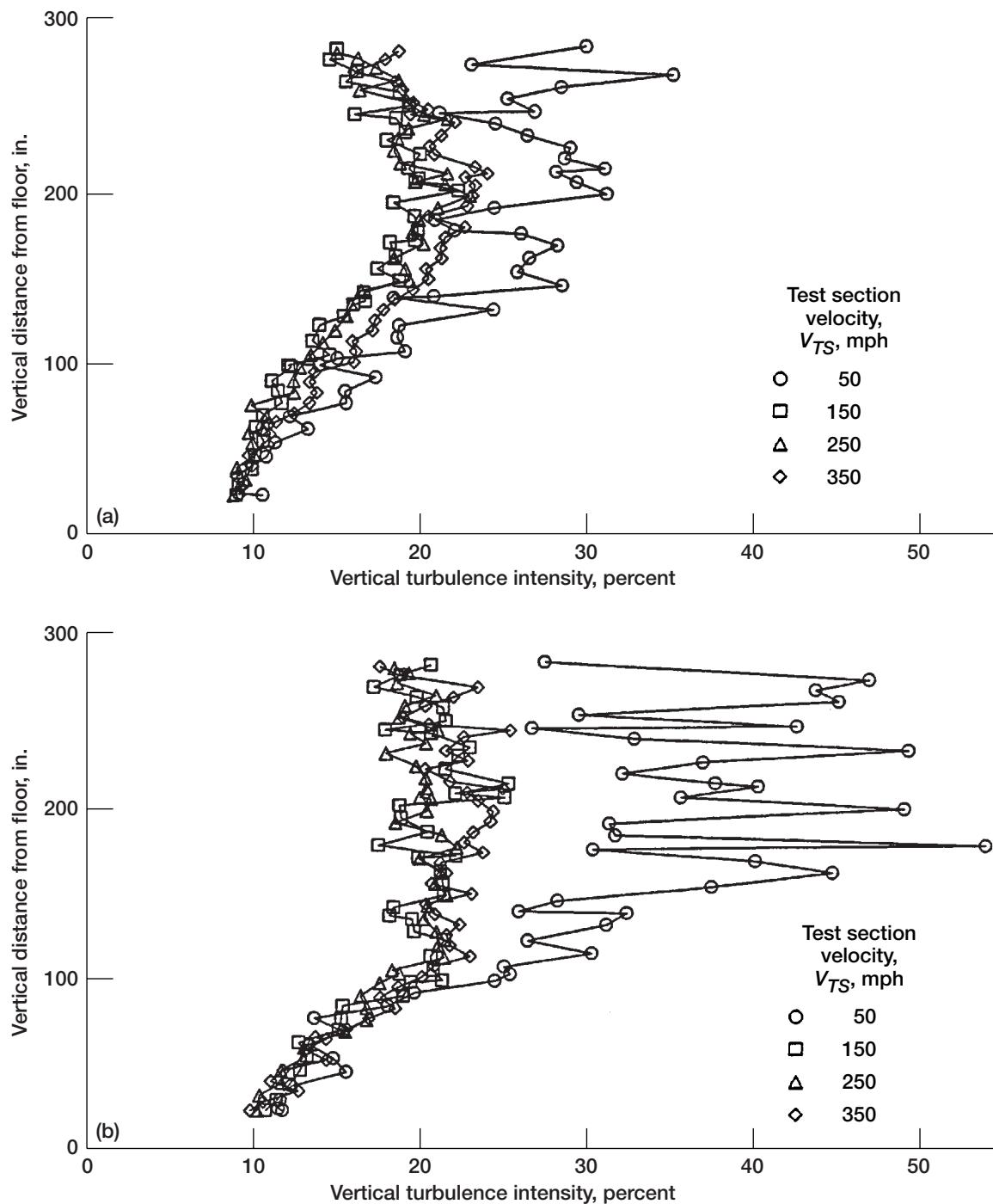


Figure 18.—Vertical turbulence intensity distribution along vertical surveys downstream of drive motor housing (station 2). (a) Traverse 1 (9.46 ft from inside wall). (b) Traverse 2 (19.52 ft from inside wall).

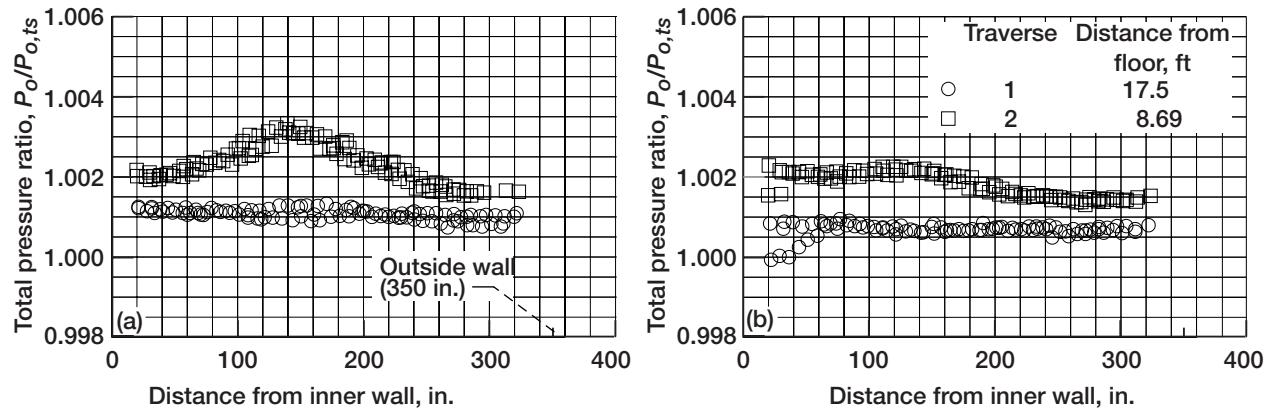


Figure 19.—Total pressure ratio distribution along horizontal surveys downstream of drive motor housing (station 2). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

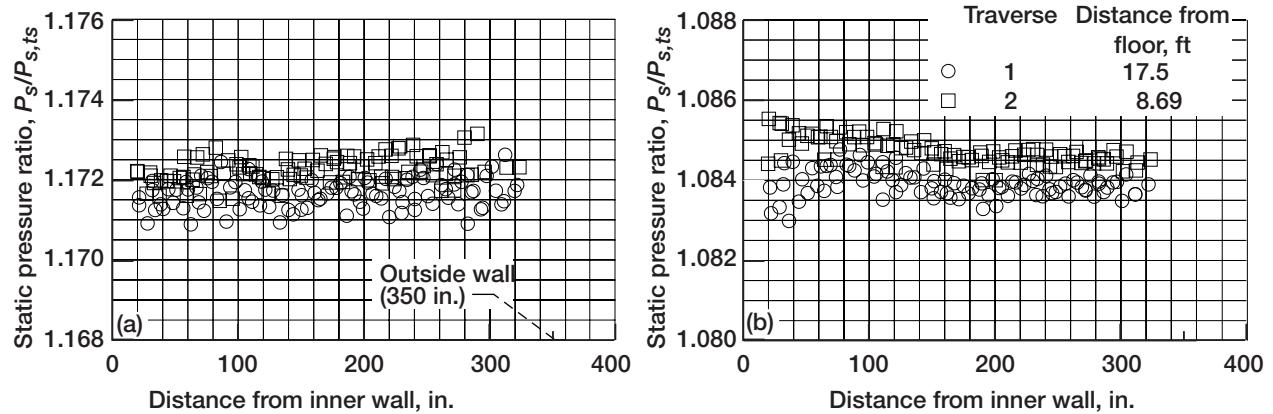


Figure 20.—Static pressure ratio distribution along horizontal surveys downstream of drive motor housing (station 2). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

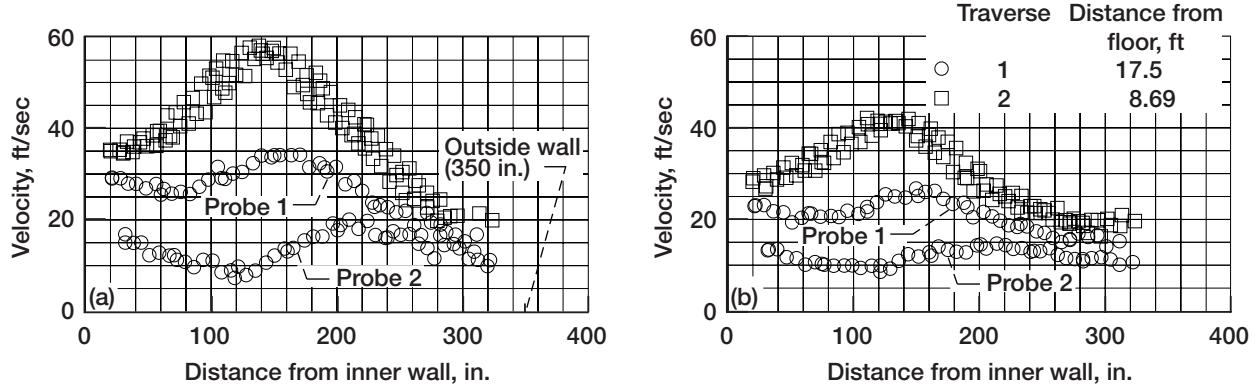


Figure 21.—Velocity distribution measured by pitot-static probes along horizontal surveys downstream of drive motor housing (station 2). (a) $V_{TS} = 350 \text{ mph}$. (b) $V_{TS} = 250 \text{ mph}$.

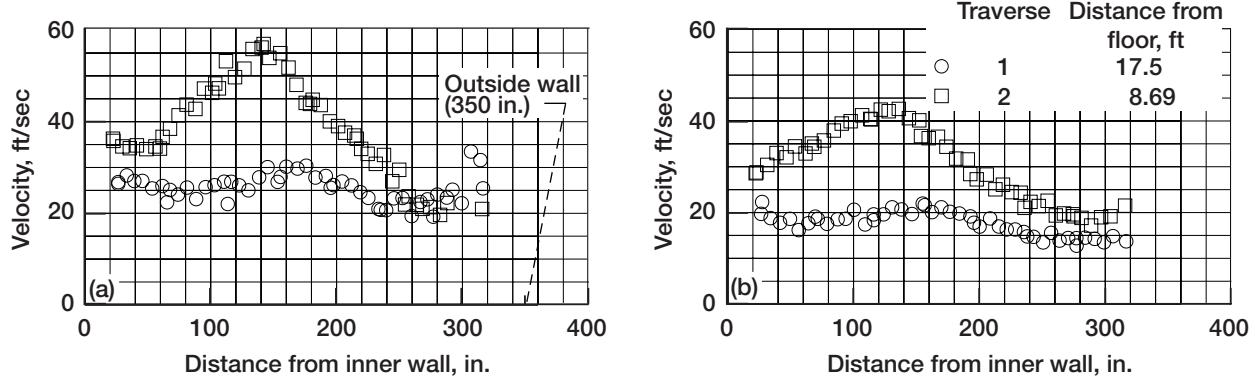


Figure 22.—Velocity distribution measured by wind anemometers along horizontal surveys downstream of drive motor housing (station 2). (a) $V_{TS} = 350 \text{ mph}$. (b) $V_{TS} = 250 \text{ mph}$.

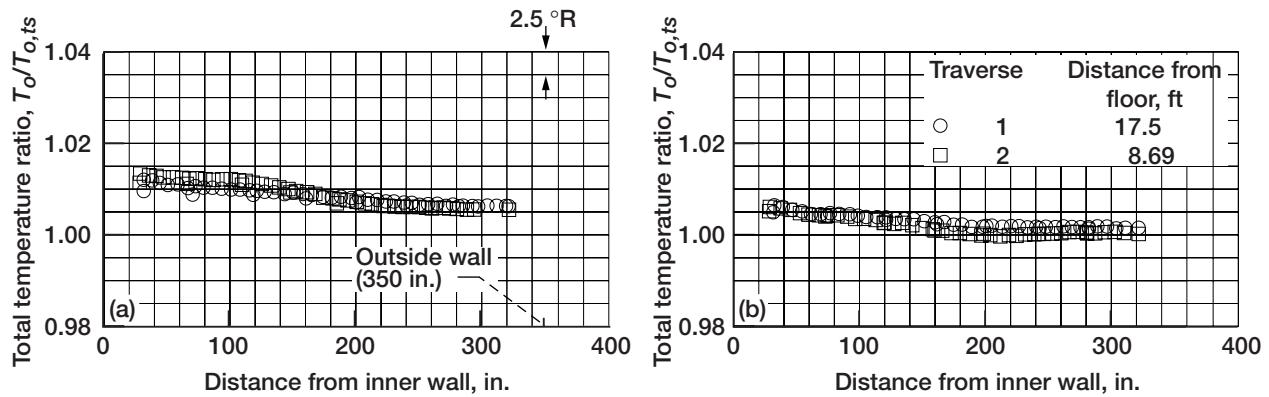


Figure 23.—Total temperature ratio distribution along horizontal surveys downstream of drive motor housing (station 2). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

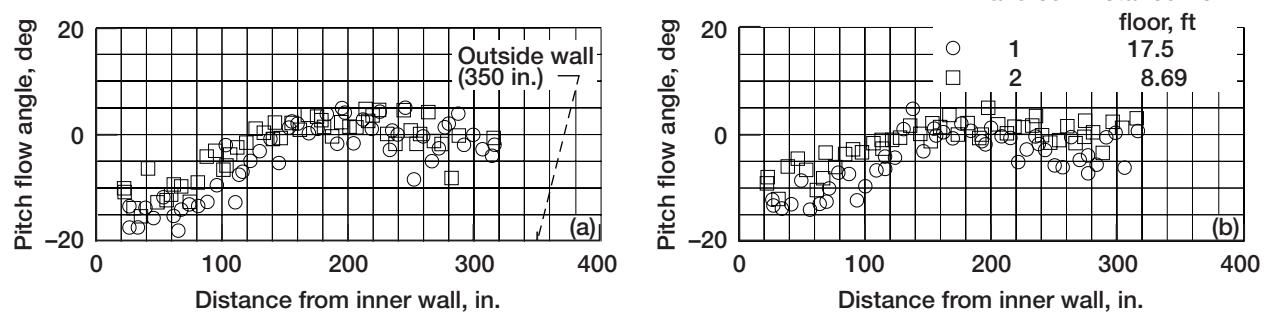


Figure 24.—Pitch flow angle distribution (positive = upflow; negative = downflow) along horizontal surveys downstream of drive motor housing (station 2). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

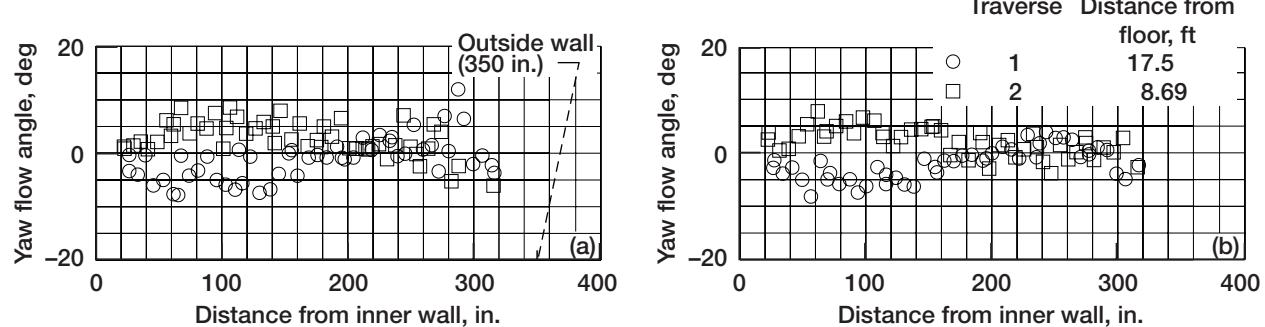


Figure 25.—Yaw flow angle distribution (positive = flow from inside wall to outside wall (outflow); negative = flow from outside to inside wall (inflow)) along horizontal surveys downstream of drive motor housing (station 2). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

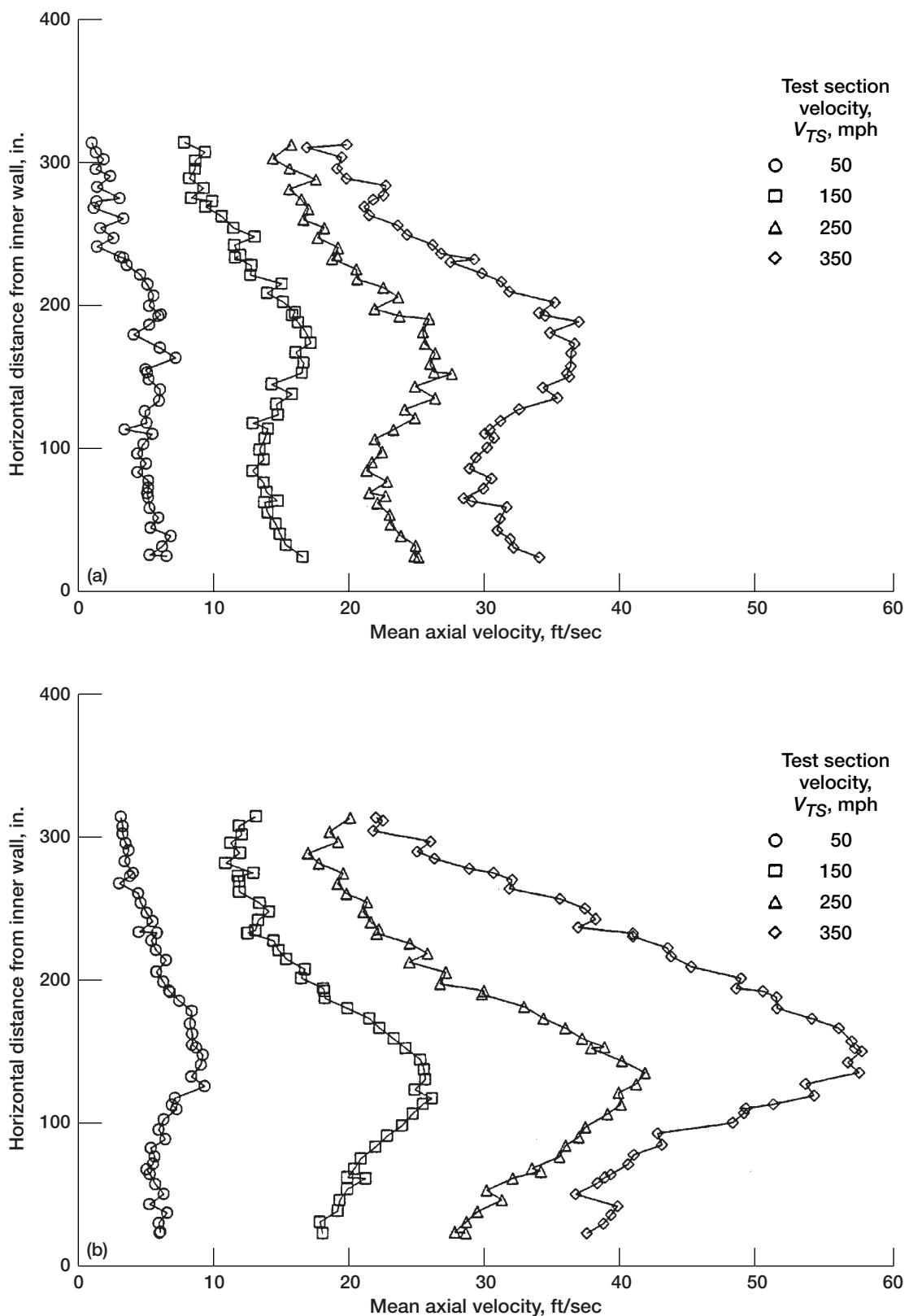


Figure 26.—Mean axial velocity distributions along horizontal surveys downstream of drive motor housing (station 2) as measured by hot-wire anemometers. (a) Traverse 1 (9.46 ft from inside wall). (b) Traverse 2 (19.52 ft from inside wall).

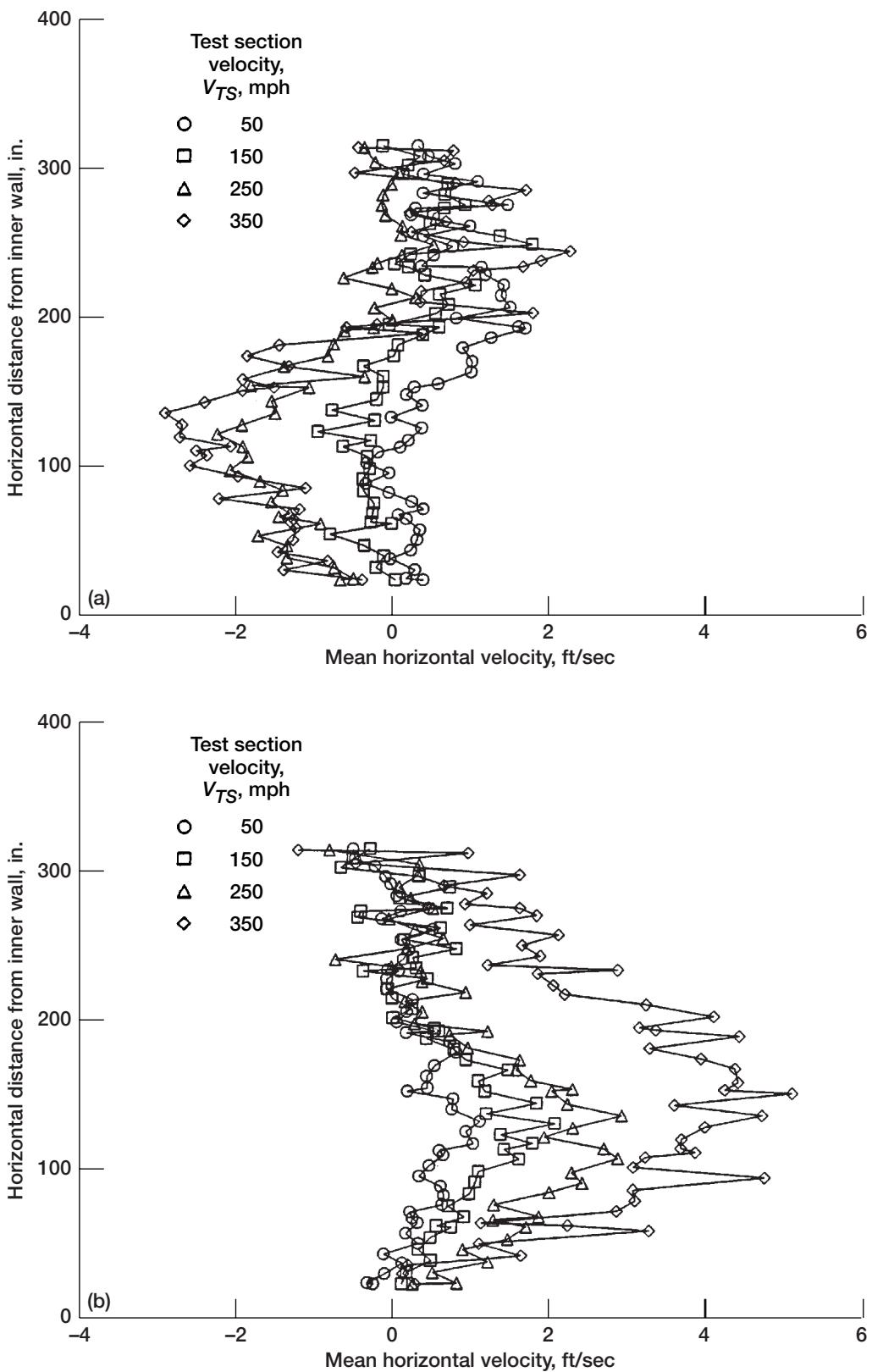


Figure 27.—Mean horizontal velocity distributions along horizontal surveys downstream of drive motor housing (station 2) as measured by hot-wire anemometers. (a) Traverse 1 (9.46 ft from inside wall). (b) Traverse 2 (19.52 ft from inside wall).

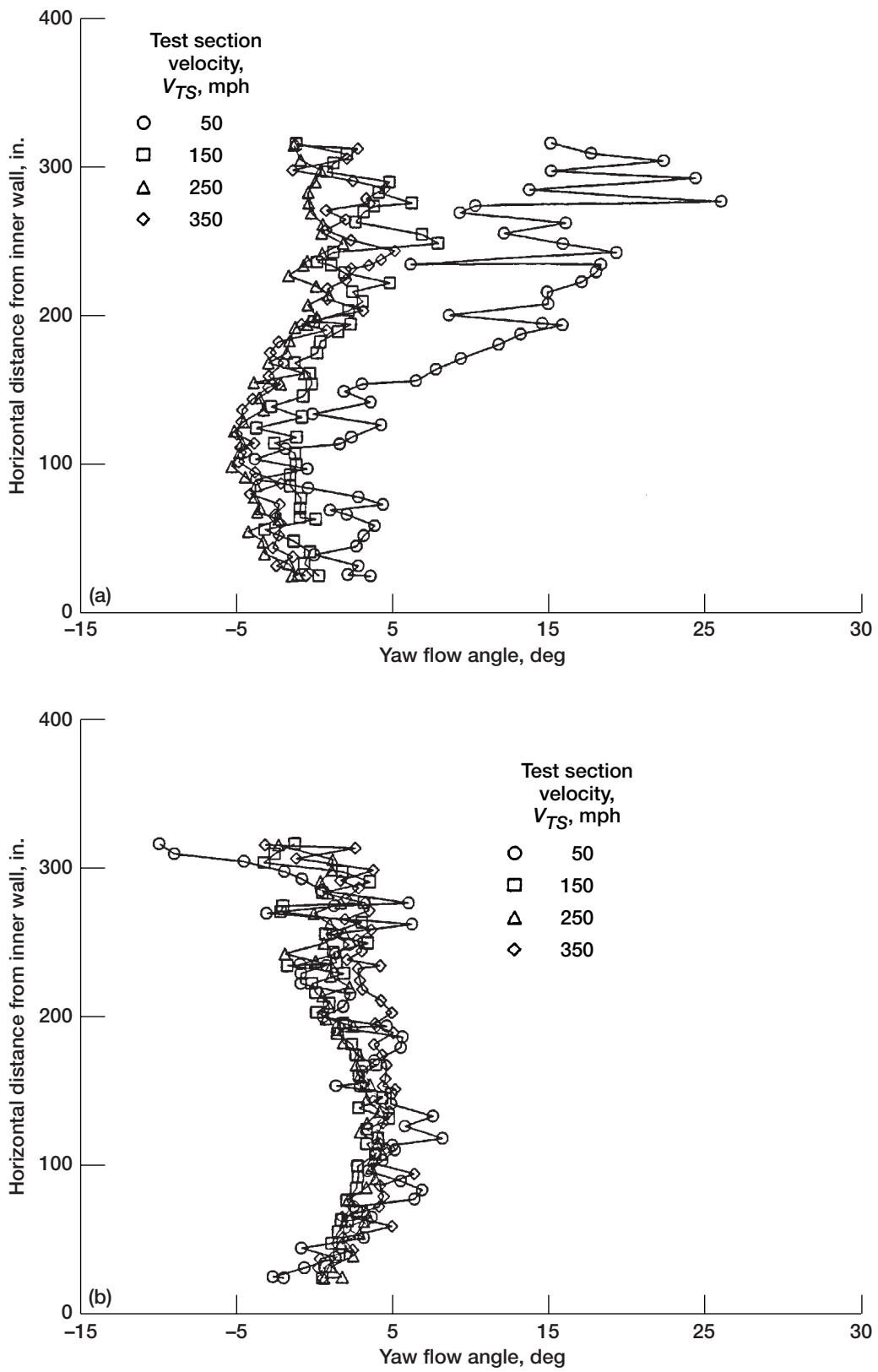


Figure 28.—Yaw flow angle distribution along horizontal surveys downstream of drive motor housing (station 2) as measured by hot-wire anemometers (positive angle indicates flow from inside wall to outside wall (outflow)). (a) Traverse 1 (17.5 ft above tunnel floor). (b) Traverse 2 (8.69 ft above tunnel floor). Positive angles indicate flow inside toward outside wall.

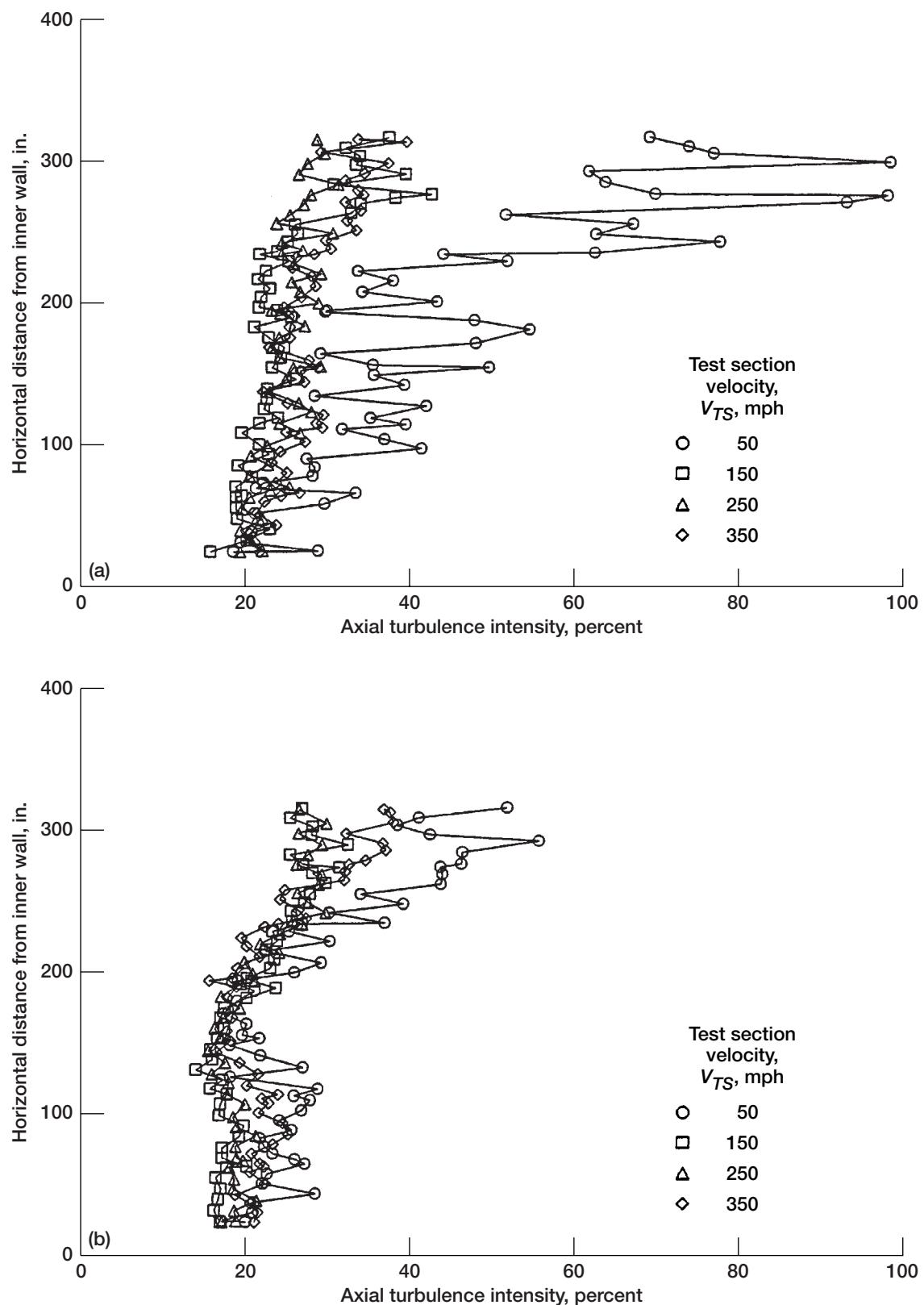


Figure 29.—Axial turbulence intensity distribution along horizontal surveys downstream of drive motor housing (station 2). (a) Traverse 1 (17.5 ft above floor). (b) Traverse 2 (8.69 ft above floor).

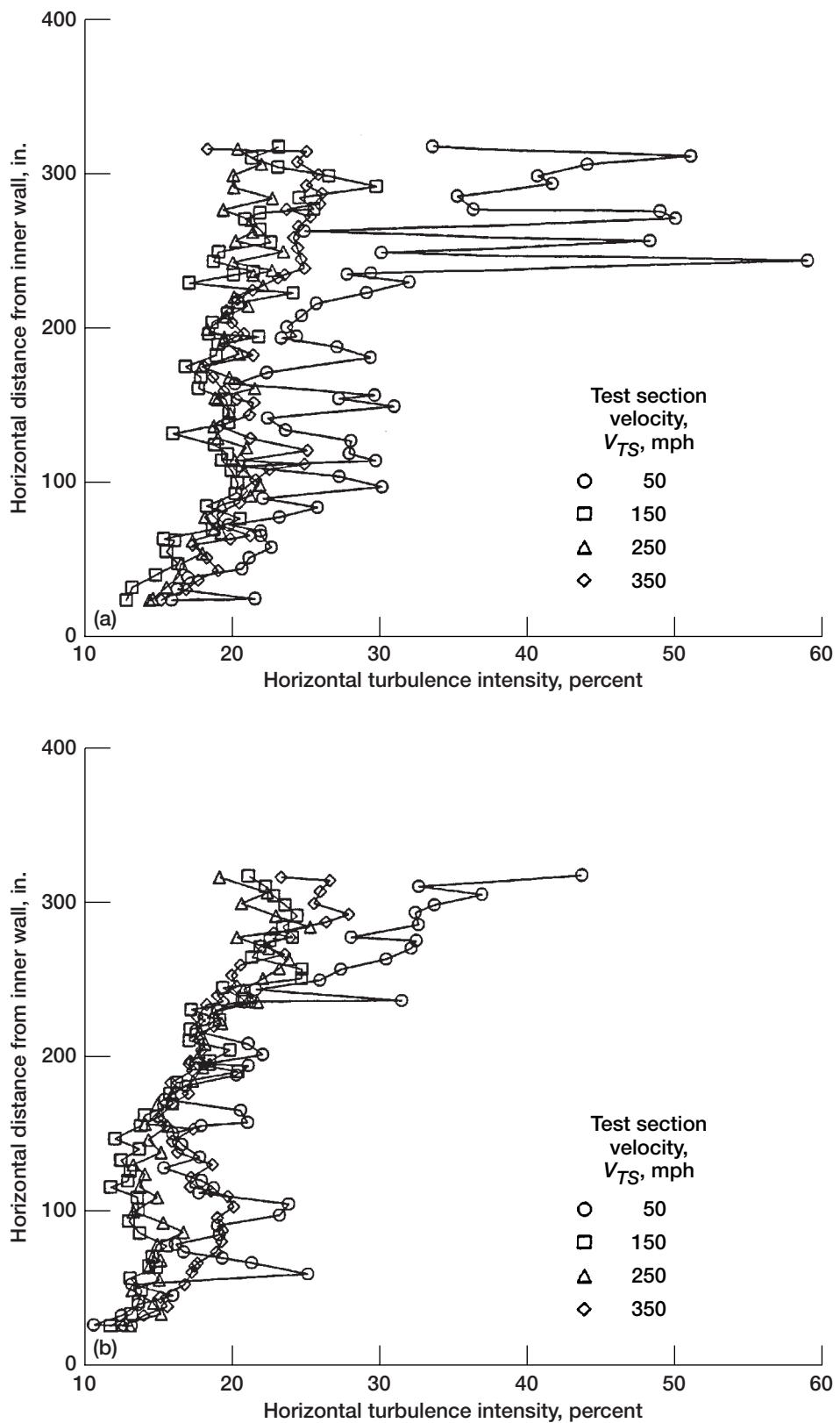


Figure 30.—Horizontal turbulence intensity distribution along horizontal surveys downstream of drive motor housing (station 2). (a) Traverse 1 (17.5 ft above floor). (b) Traverse 2 (8.69 ft above floor).

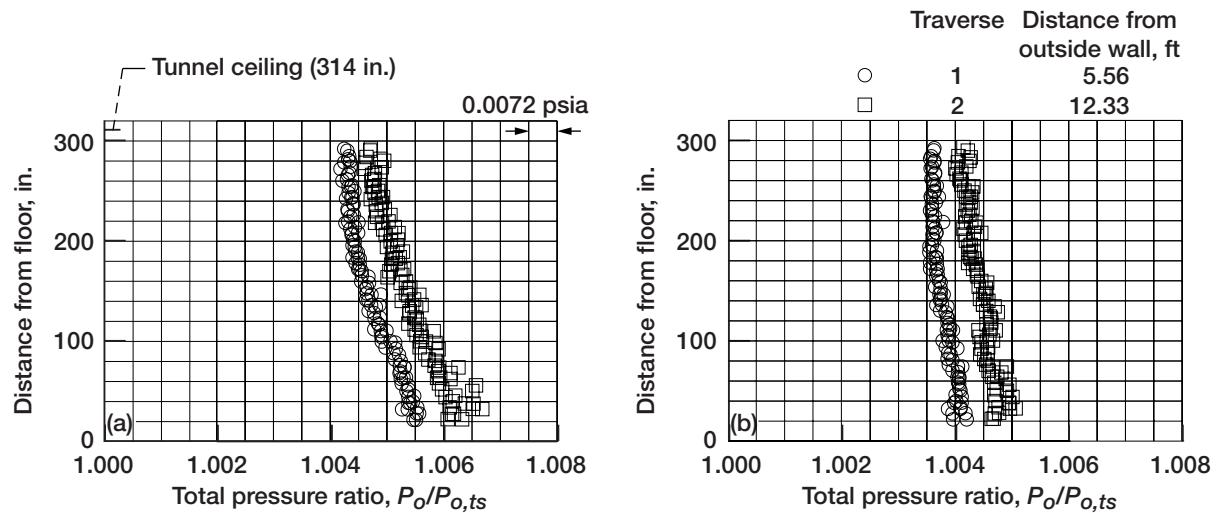


Figure 31.—Total pressure ratio distribution along vertical surveys upstream of facility heat exchanger (station 3). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

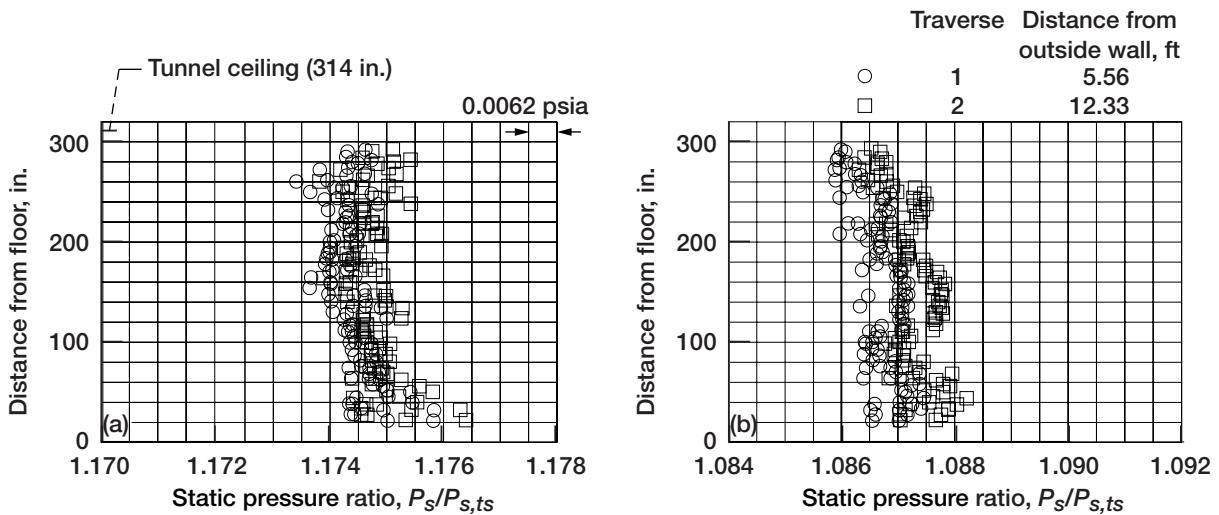


Figure 32.—Static pressure ratio distribution along vertical surveys upstream of facility heat exchanger (station 3). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

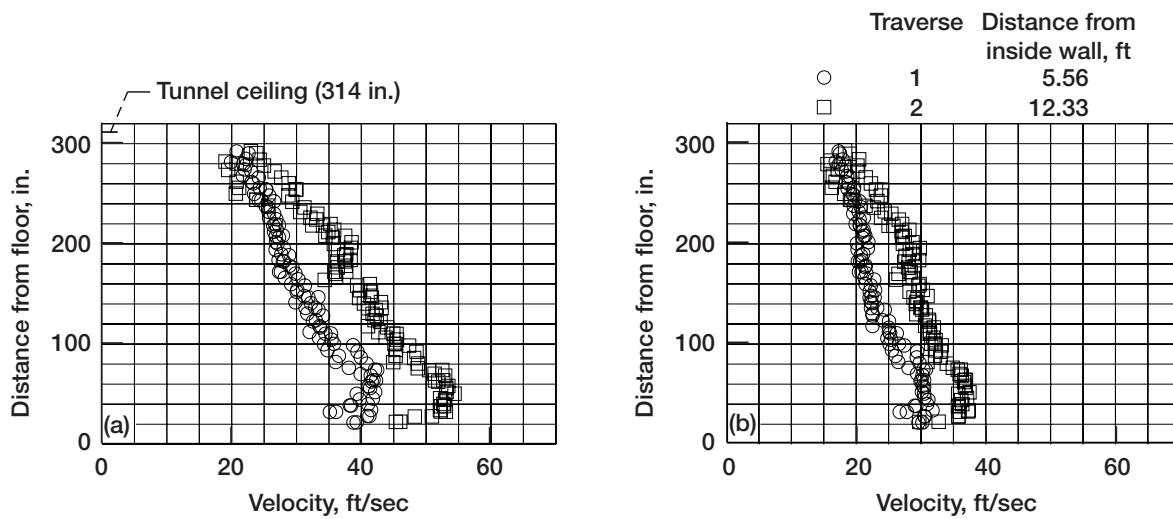


Figure 33.—Velocity distribution measured by pitot-static probes along vertical surveys upstream of facility heat exchanger (station 3). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

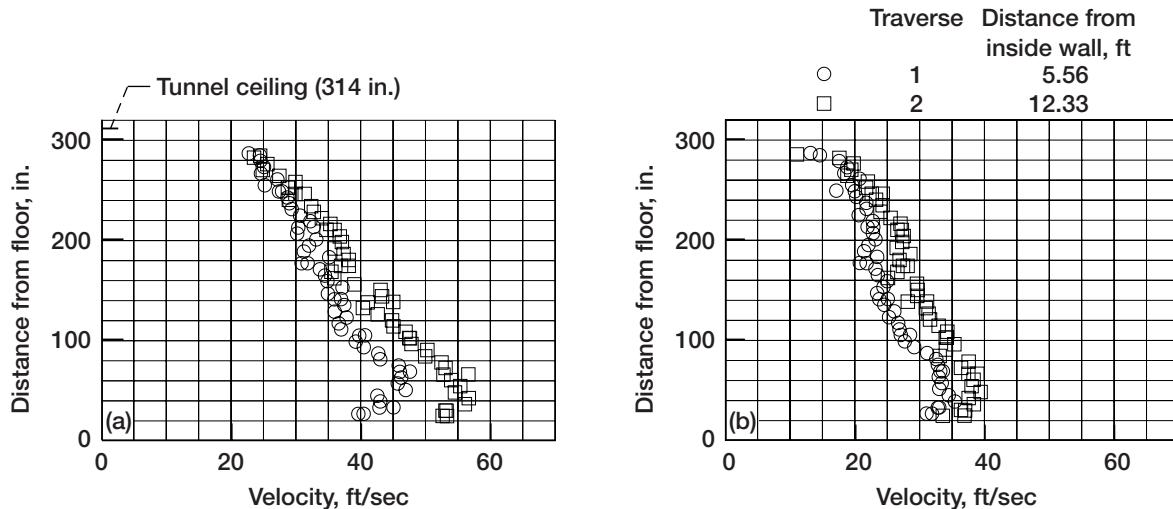


Figure 34.—Velocity distribution along vertical surveys upstream of facility heat exchanger (station 3) as measured by wind anemometers. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

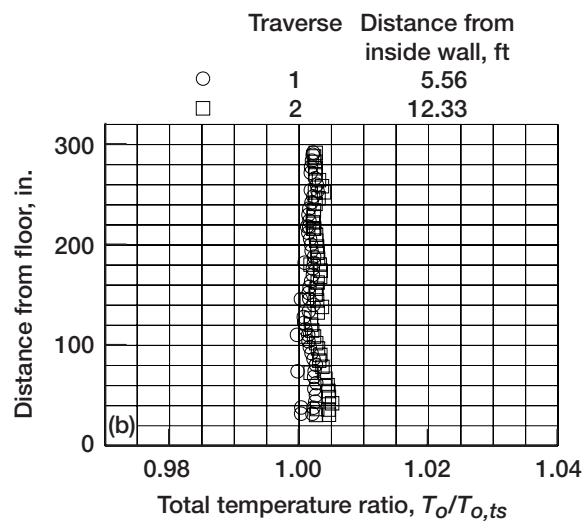
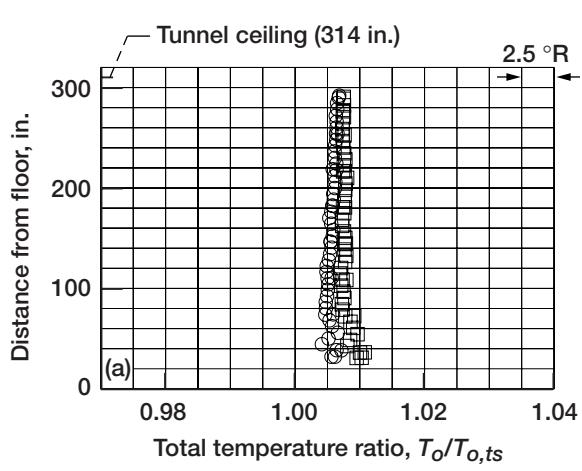


Figure 35.—Total temperature ratio distribution along vertical surveys upstream of facility heat exchanger (station 3). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

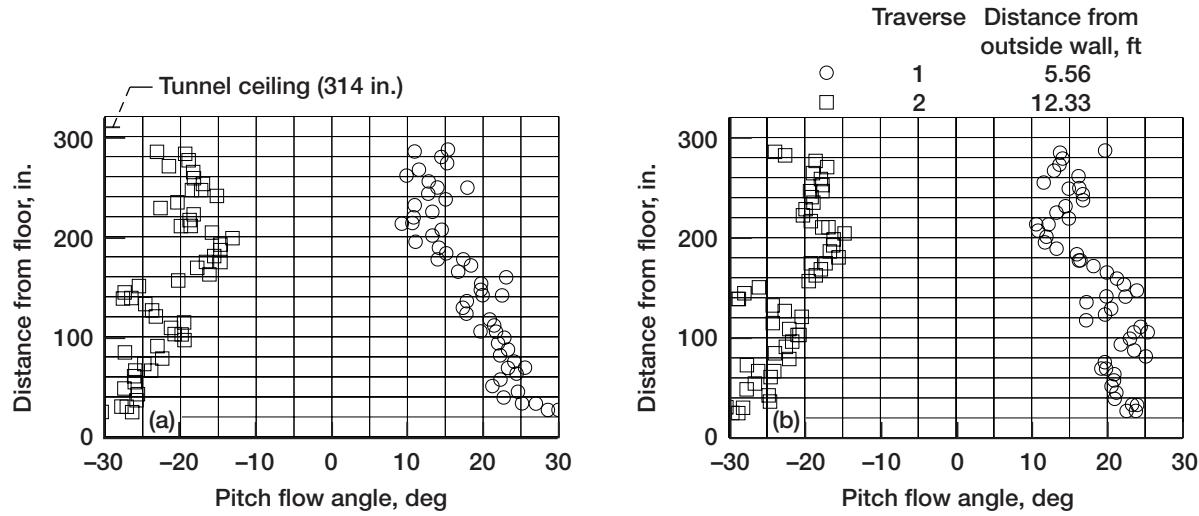


Figure 36.—Pitch flow angle distribution along vertical surveys upstream of facility heat exchanger (station 3) as measured by wind anemometers. (These data are believed to have been affected by some undetected instrumentation problem and are, therefore, of little value; they are included here only for completeness.)
(a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

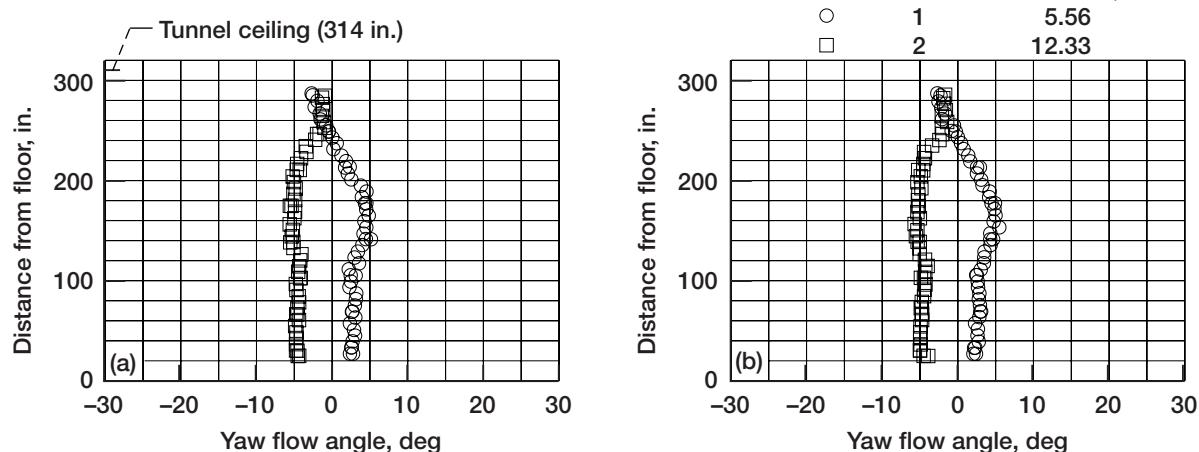


Figure 37.—Yaw flow angle distribution measured by wind anemometers along vertical surveys upstream of facility heat exchanger (station 3). (These data are believed to have been affected by some undetected instrumentation problem and are, therefore, of little value; they are included here only for completeness.)
(a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

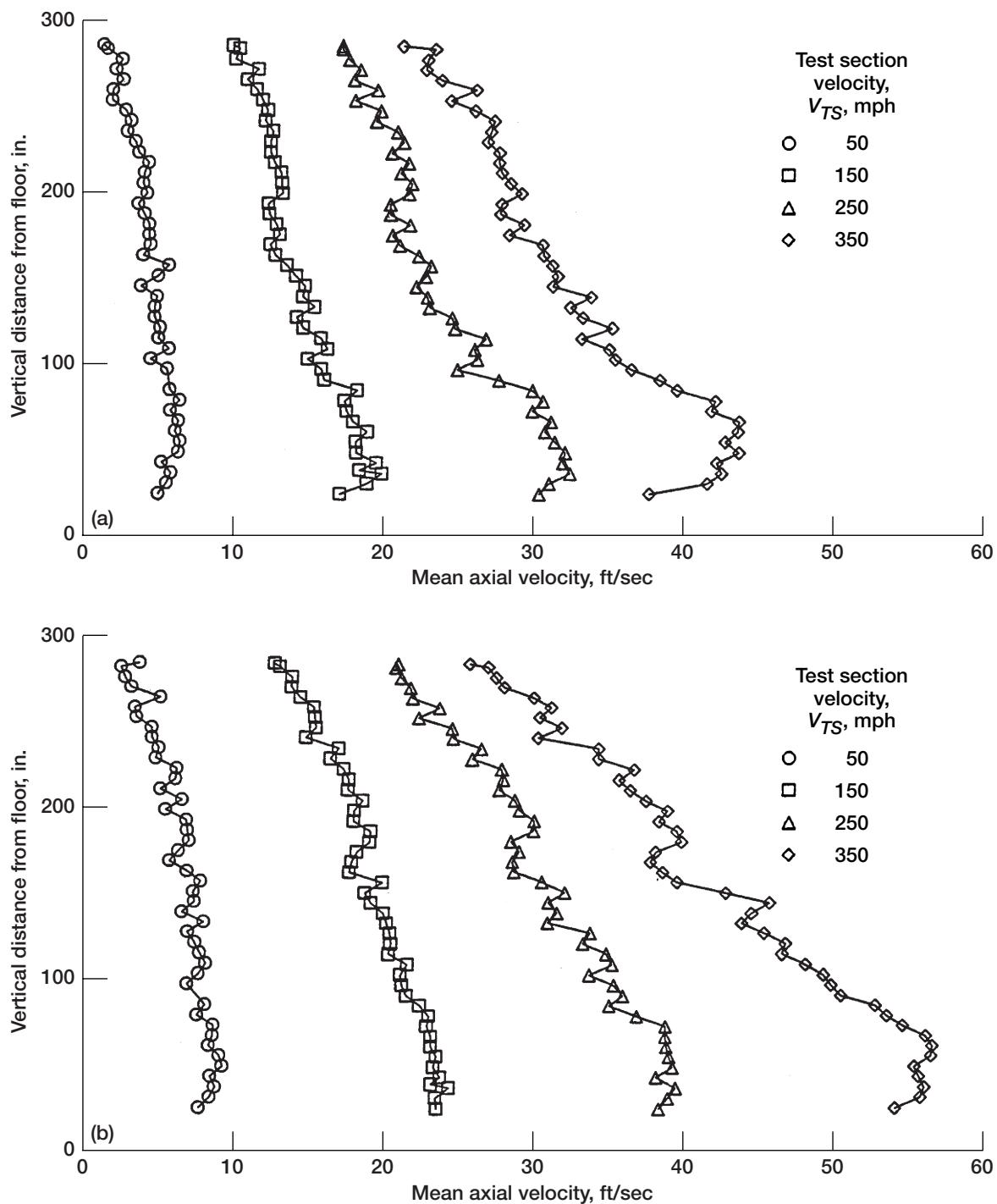


Figure 38.—Mean axial velocity distribution measured by hot-wire anemometers along vertical surveys upstream of facility heat exchanger (station 3). (a) Traverse 1 (5.56 ft from outside wall). (b) Traverse 2 (12.33 ft from outside wall).

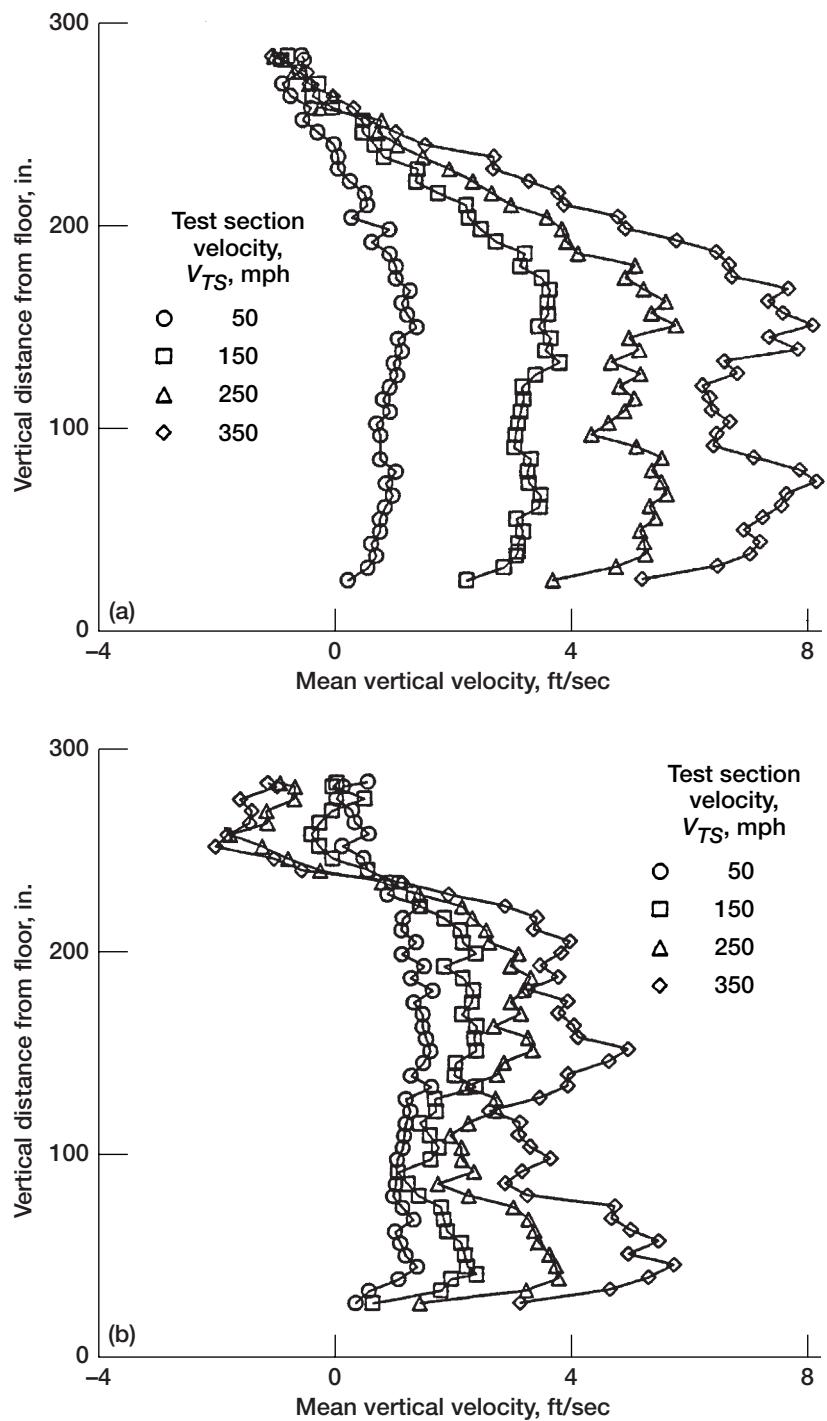
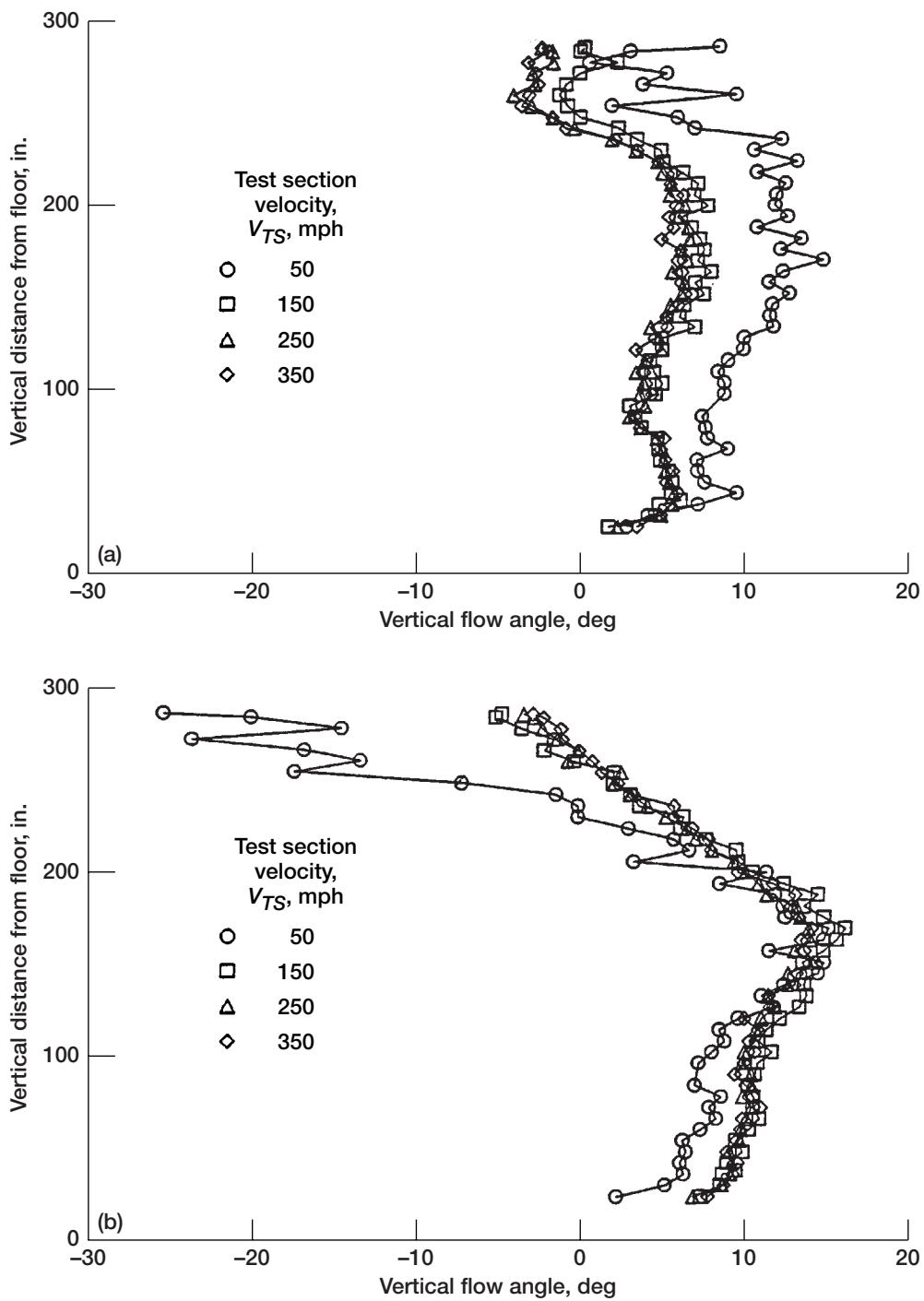


Figure 39.—Mean vertical velocity distribution along vertical surveys upstream of heat exchanger (station 3) as measured by hot-wire anemometers. (a) Traverse 1 (5.56 ft from outside wall). (b) Traverse 2 (12.33 ft from outside wall).



Figures 40.—Pitch flow angle distribution along vertical surveys upstream of facility heat exchanger (station 3) as measured by hot-wire anemometers. Traverse 1 (5.56 ft from outside wall). (b) Traverse 2 (12.33 ft from outside wall).

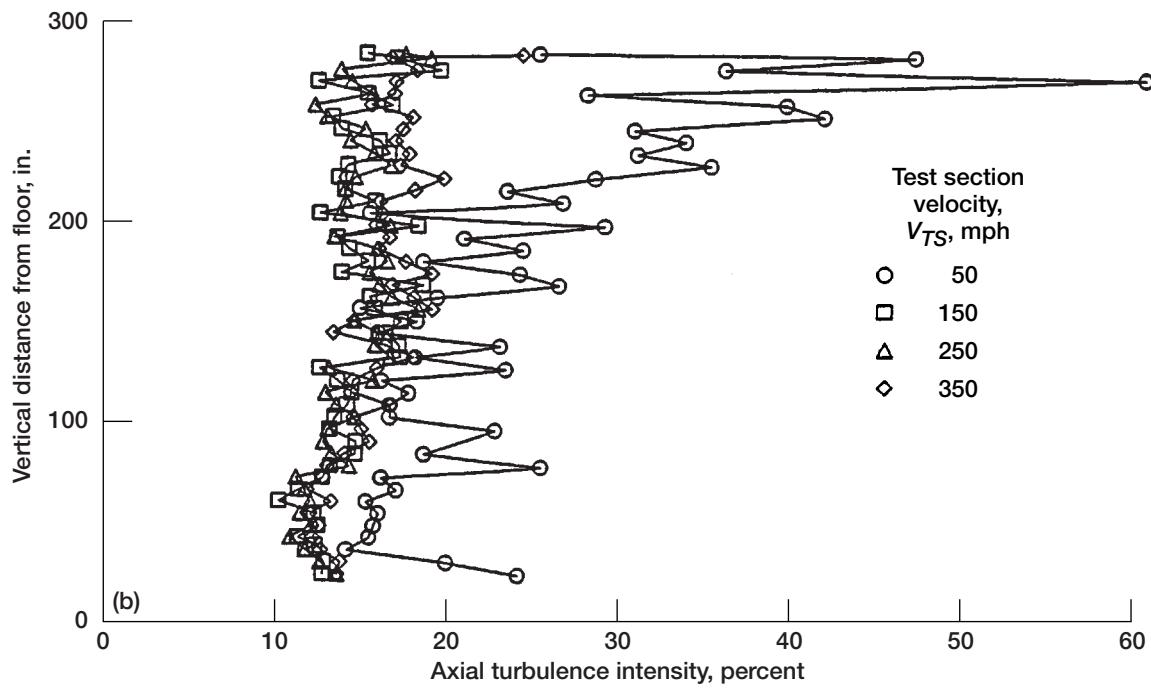
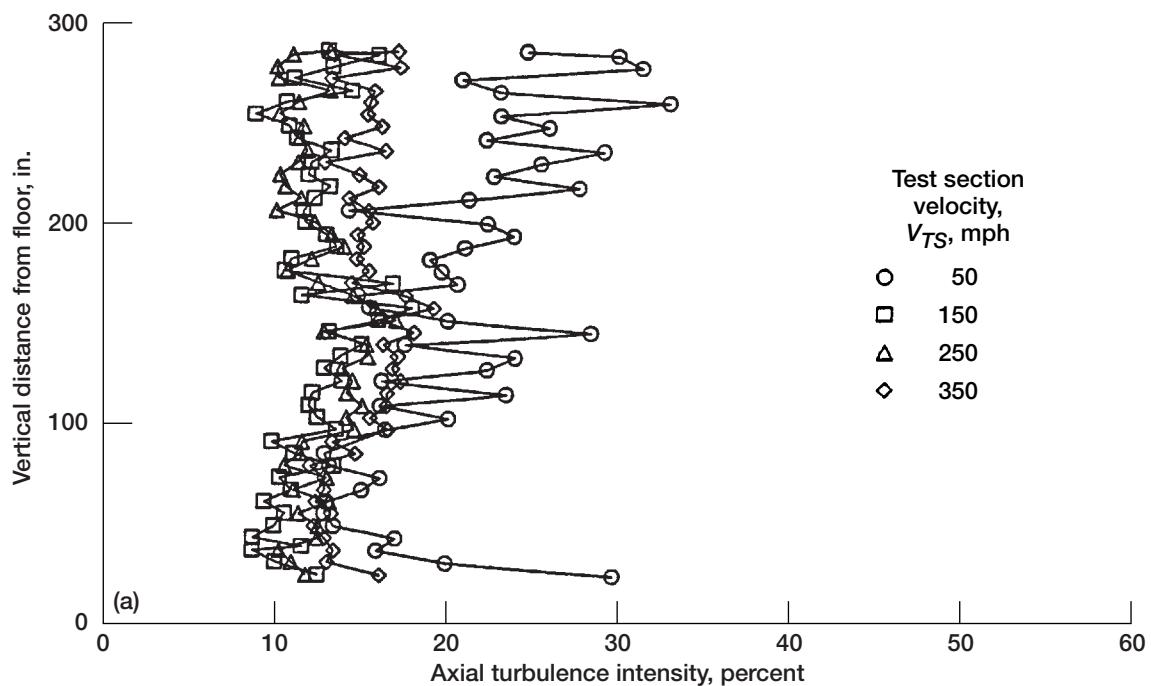


Figure 41.—Axial turbulence intensity along vertical surveys upstream of facility heat exchanger (station 3). (a) Traverse 1 (5.56 ft from outside wall). (b) Traverse 2 (12.33 ft from outside wall).

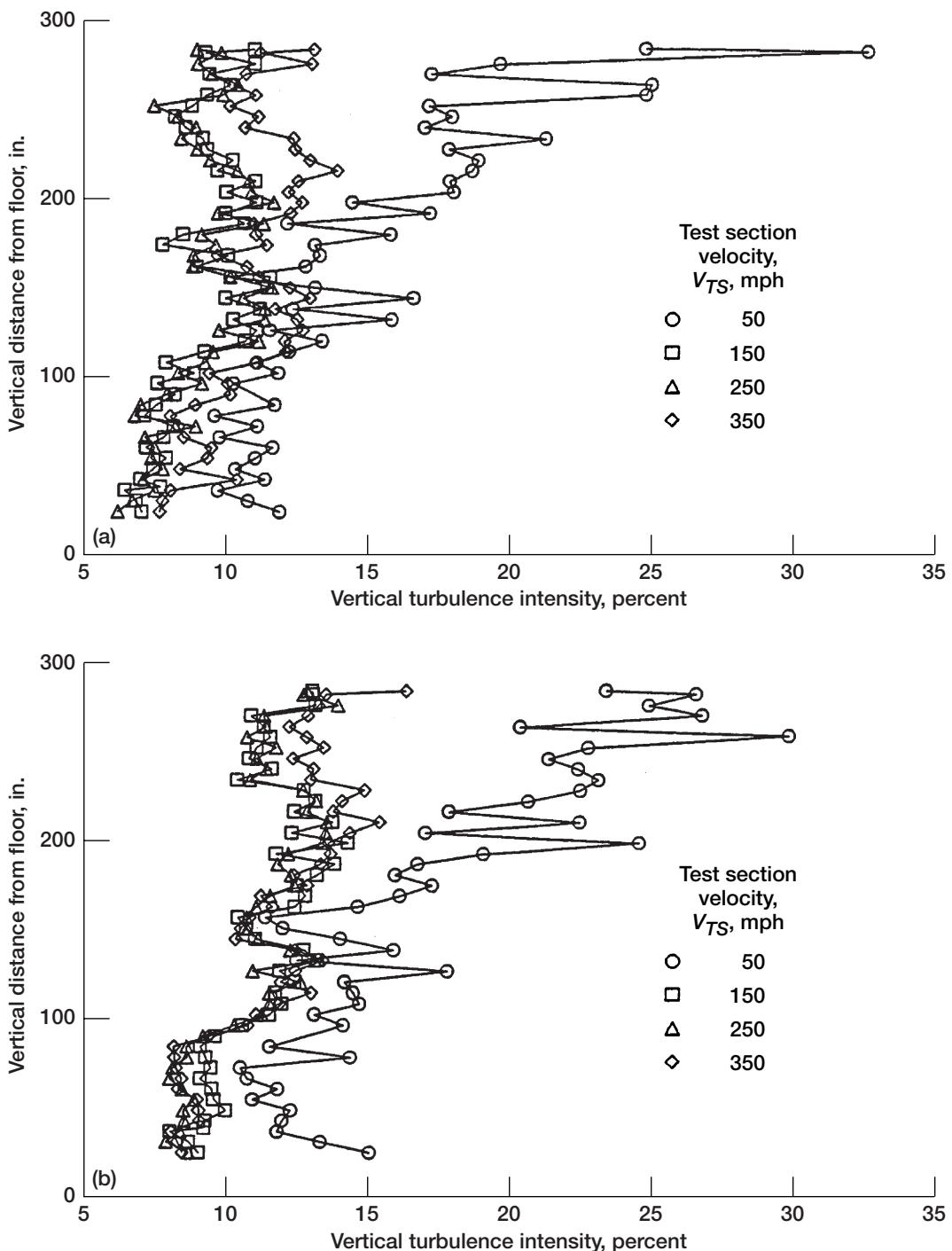


Figure 42.—Vertical turbulence intensity distribution along vertical surveys upstream of facility heat exchanger (station 3). (a) Traverse 1 (5.56 ft from outside wall). (b) Traverse 2 (12.33 ft from outside wall).

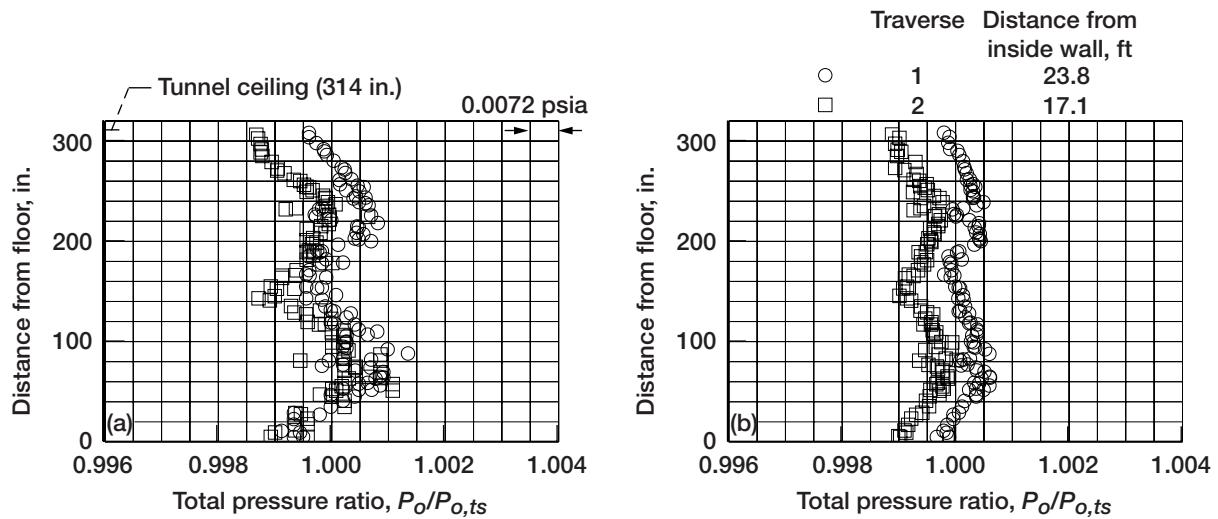


Figure 43.—Total pressure ratio distribution along vertical surveys downstream of facility heat exchanger (station 4). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

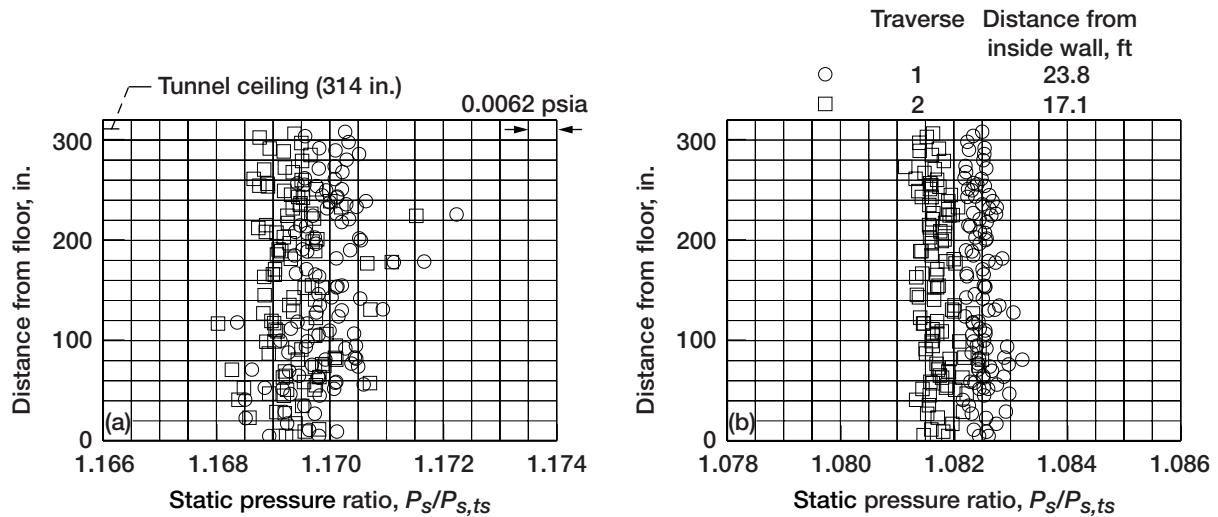


Figure 44.—Static pressure ratio distribution along vertical surveys downstream of facility heat exchanger (station 4). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

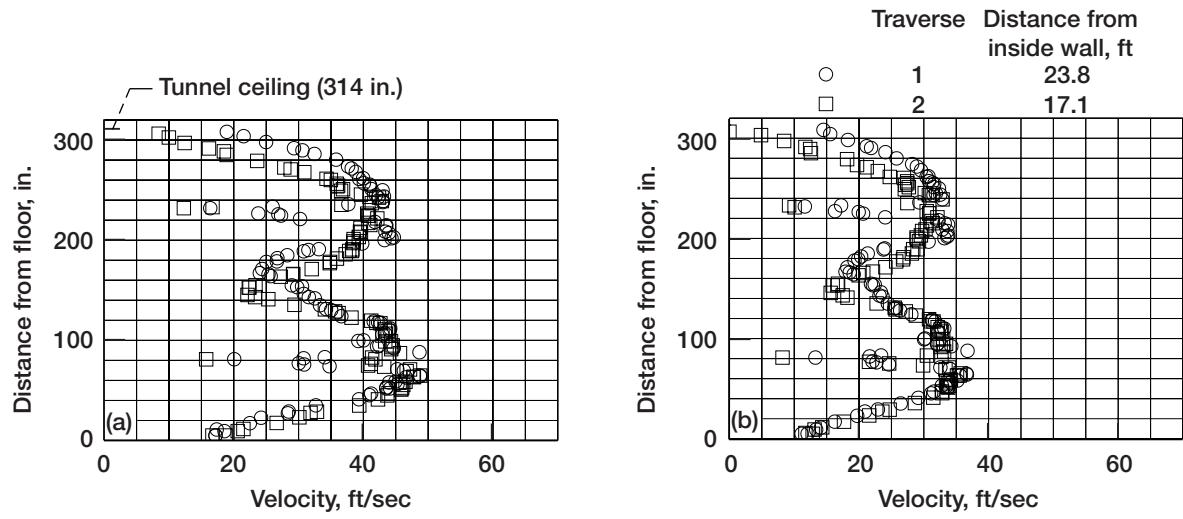


Figure 45.—Velocity distribution measured by pitot-static probes along vertical surveys downstream of heat exchanger (station 4). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

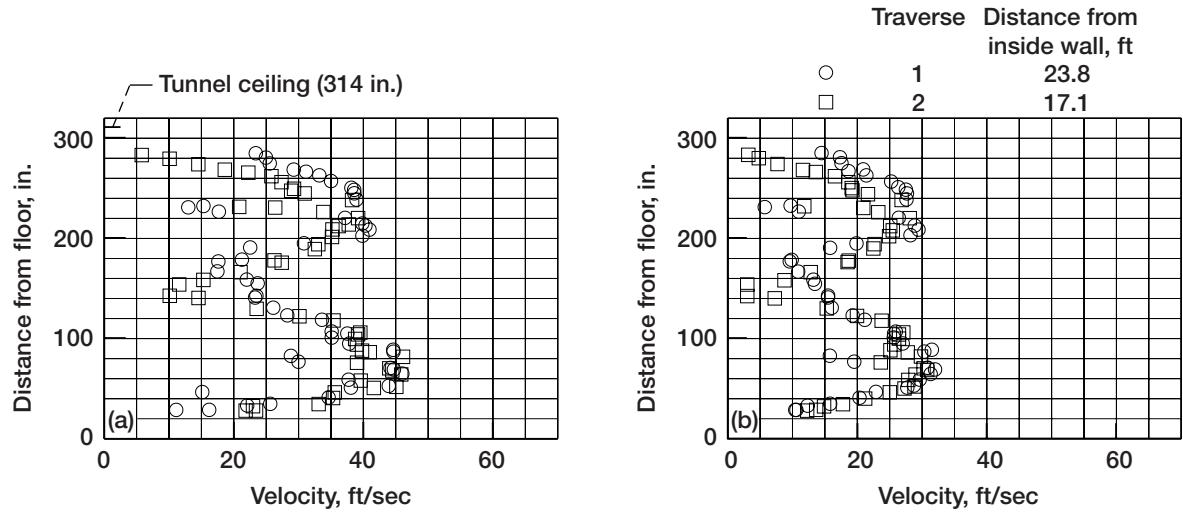


Figure 46.—Velocity distribution measured by wind anemometers along vertical surveys downstream of heat exchanger (station 4). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

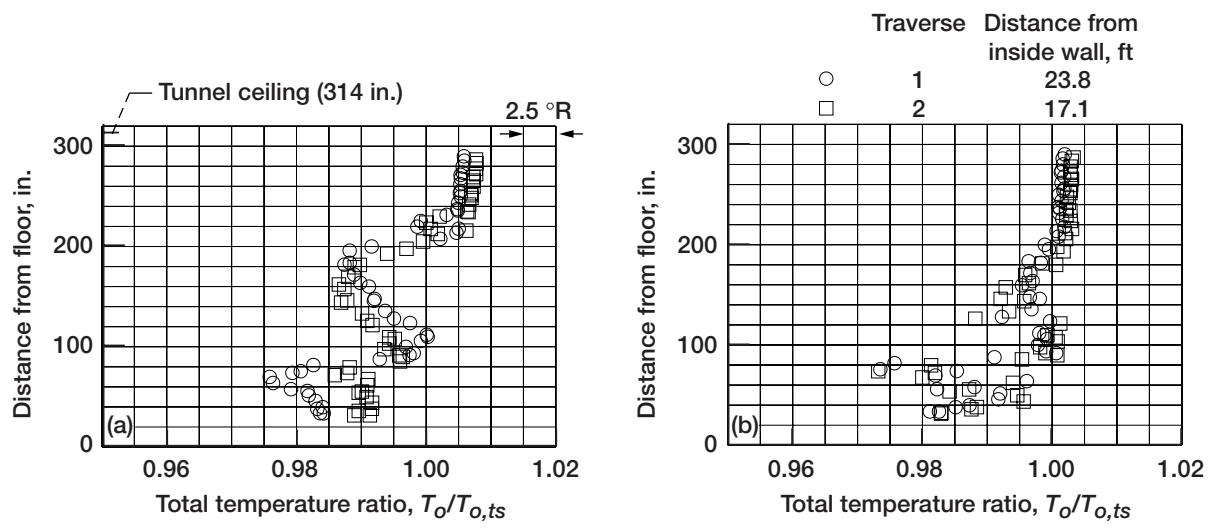


Figure 47.—Total temperature ratio distribution along vertical surveys downstream of heat exchanger (station 4). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

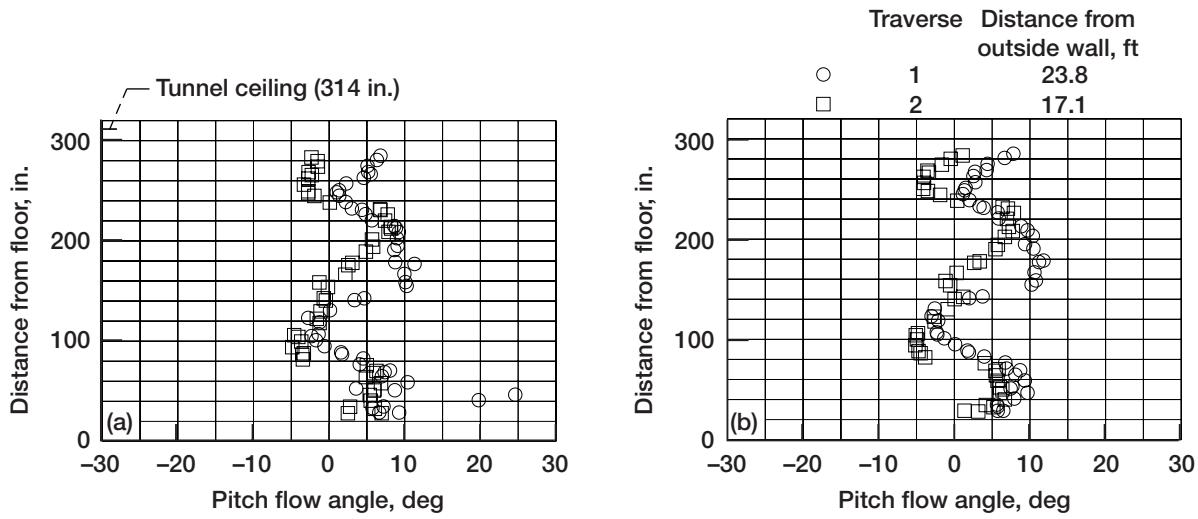


Figure 48.—Pitch flow angle distribution (positive = upflow; negative = downflow) along vertical surveys downstream of heat exchanger (station 4). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

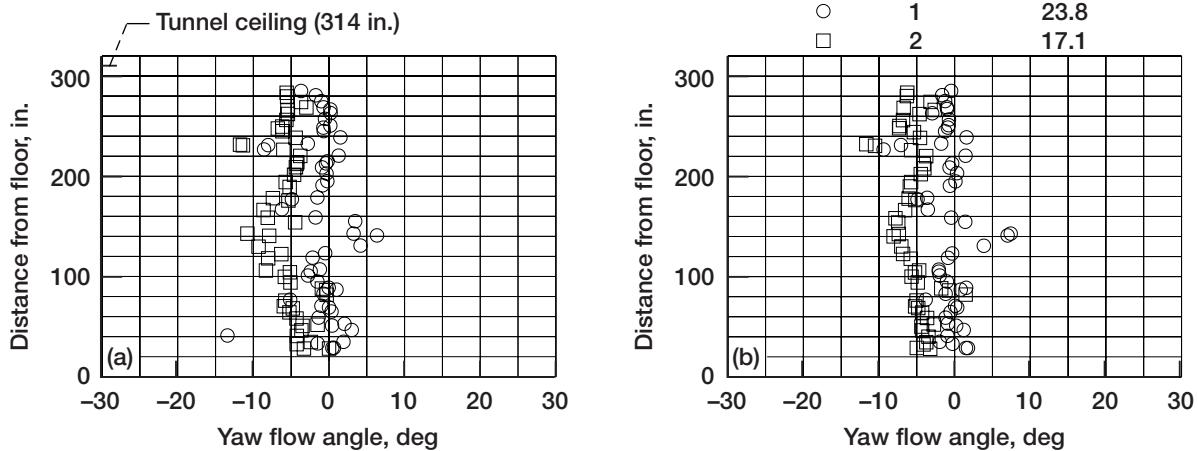


Figure 49.—Yaw flow angle distribution (positive = flow toward outside tunnel wall) along vertical surveys downstream of heat exchanger (station 4). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

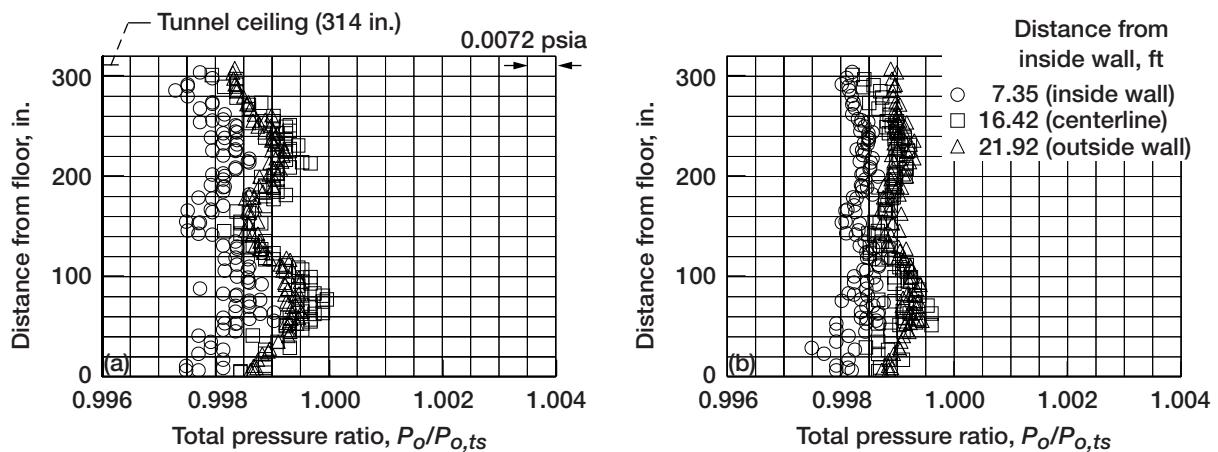


Figure 50.—Total pressure ratio distribution along vertical surveys upstream of spraybars (station 5).
 (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

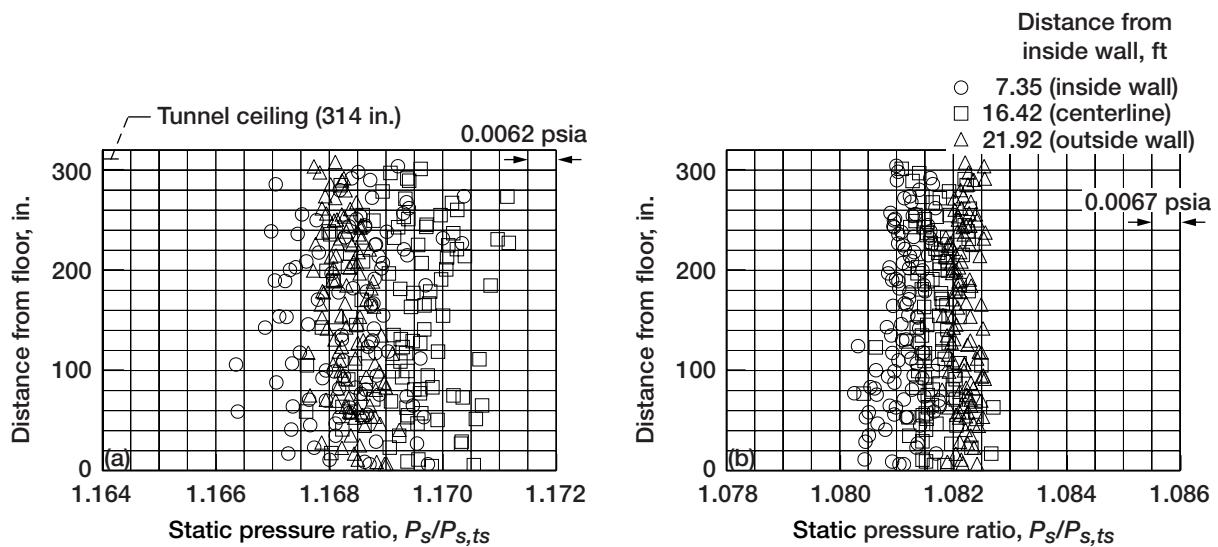


Figure 51.—Static pressure ratio distribution along vertical surveys upstream of spraybars (station 5).
 (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

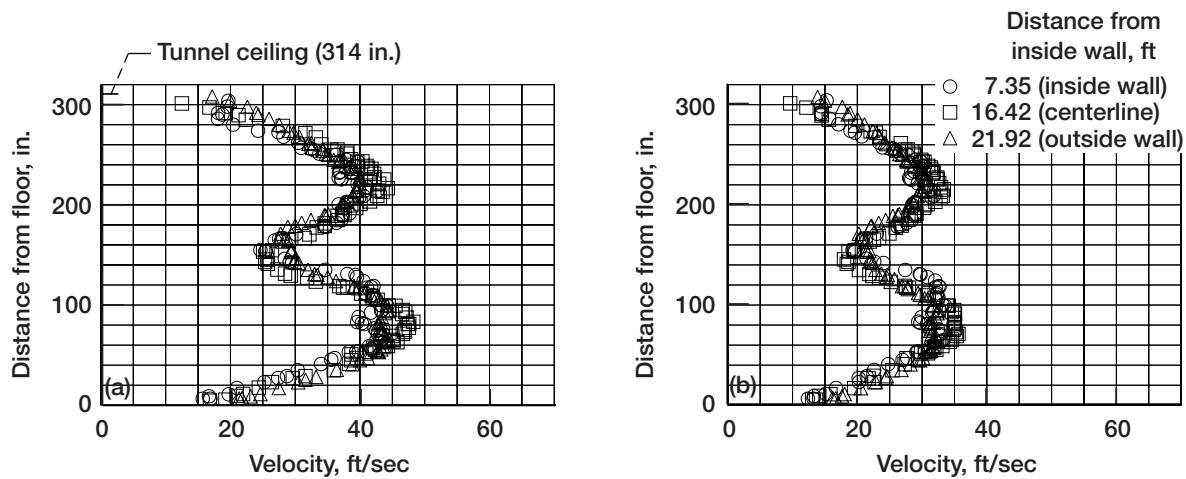


Figure 52.—Velocity distribution measured by pitot-static probes along vertical surveys upstream of spraybars (station 5). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

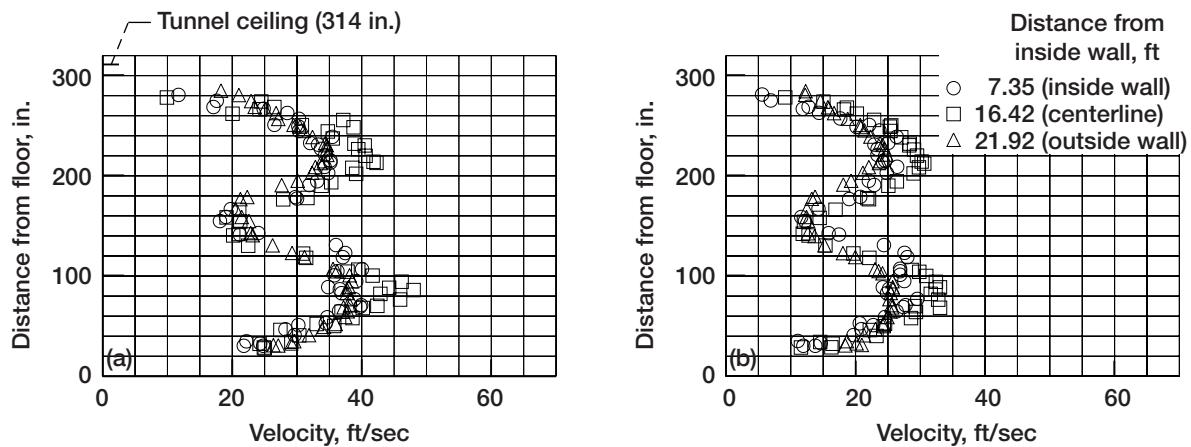


Figure 53.—Velocity distribution measured by wind anemometers along vertical surveys upstream of spraybars (station 5). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

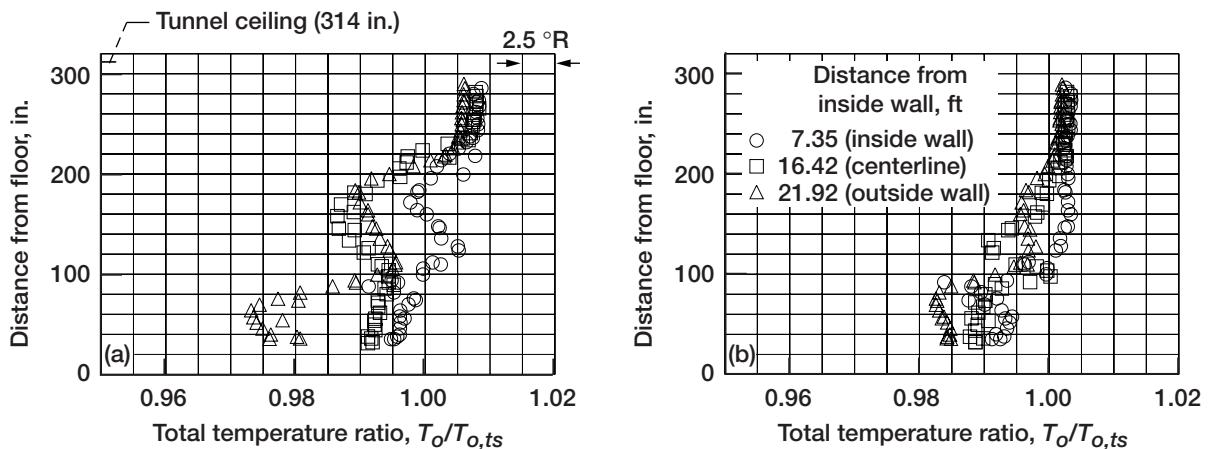


Figure 54.—Total temperature ratio distribution along vertical surveys upstream of spraybars (station 5). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

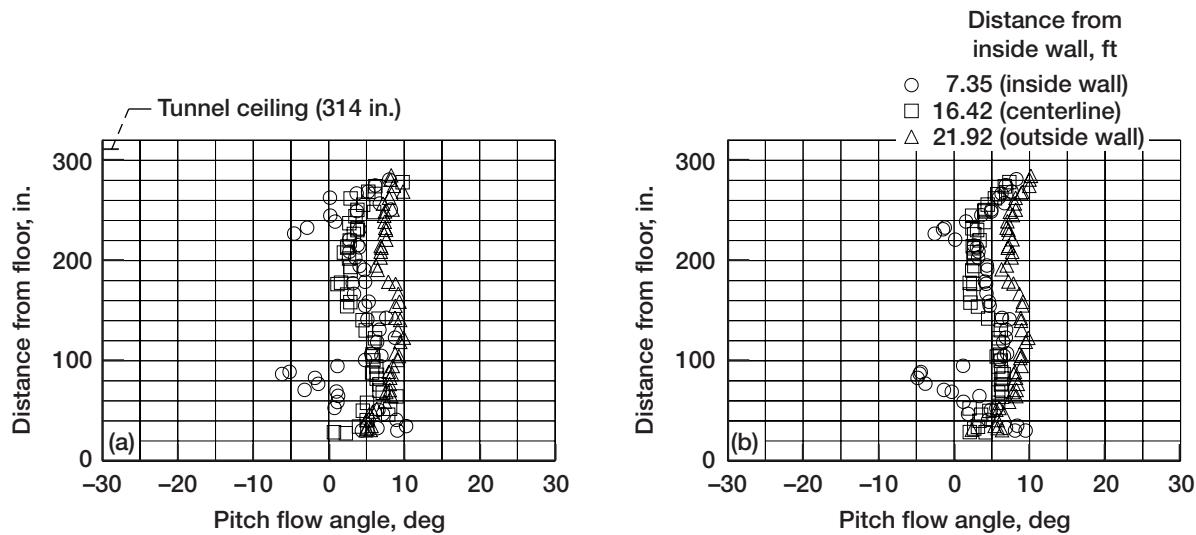


Figure 55.—Pitch flow angle distributions along vertical surveys upstream of spraybars (station 5). Positive angles indicate upflow. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

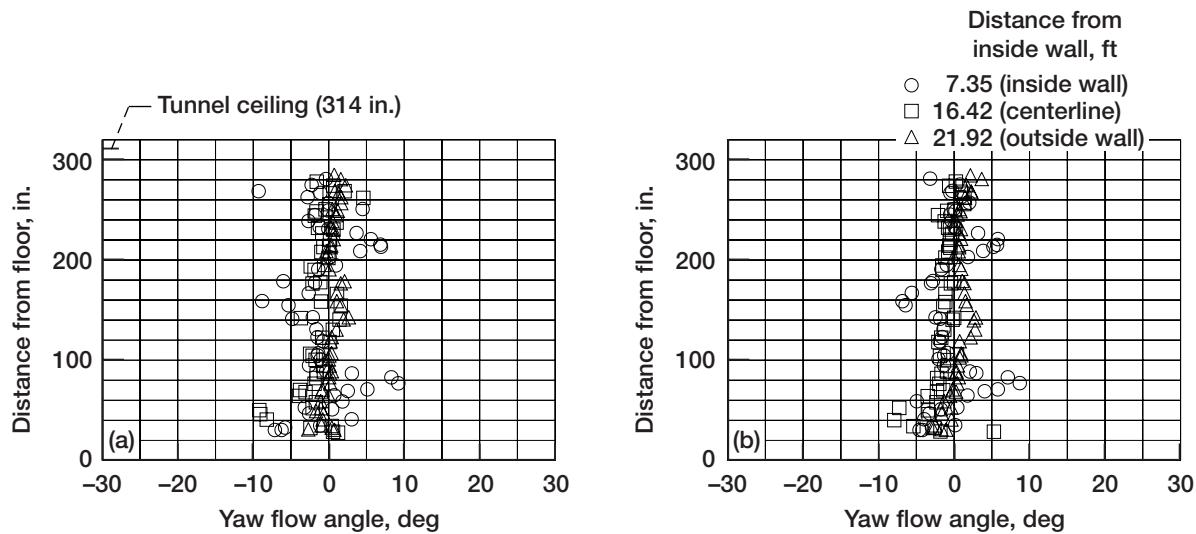


Figure 56.—Yaw flow angle distributions along vertical surveys upstream of spraybars (station 5). Positive angles indicate flow from inside to outside tunnel wall. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

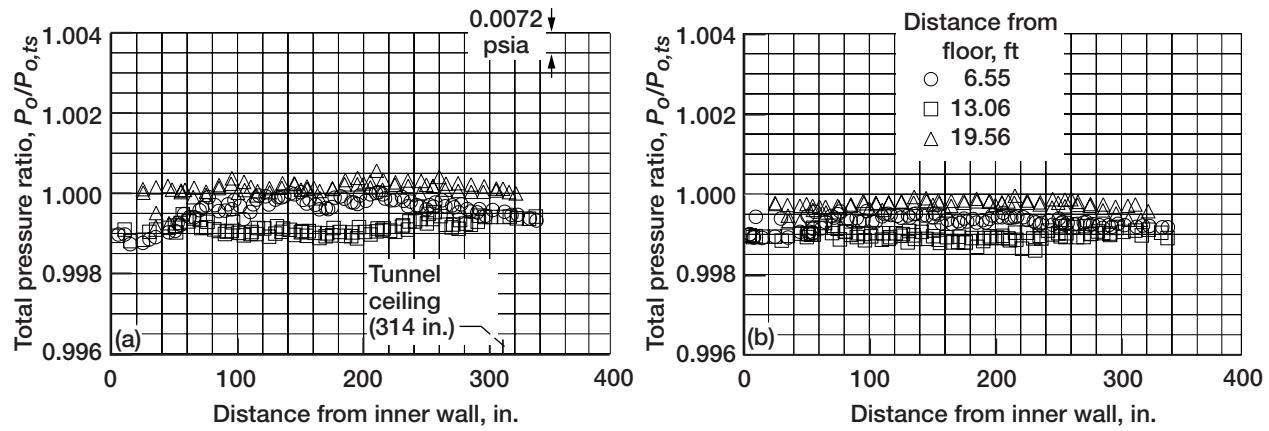


Figure 57.—Total pressure ratio distribution along horizontal surveys upstream of spraybars (station 5).
 (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

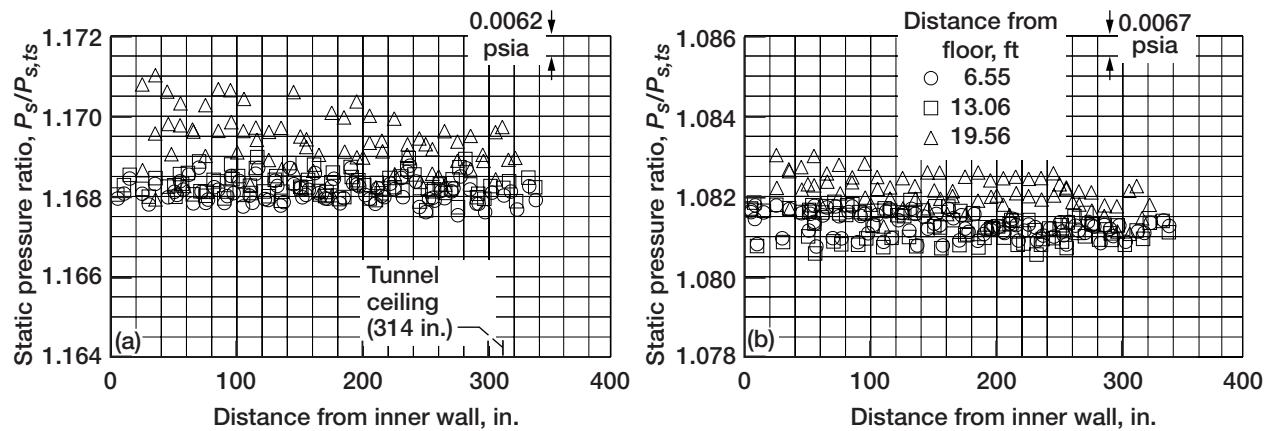


Figure 58.—Static pressure ratio distribution along horizontal surveys upstream of spraybars (station 5).
 (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

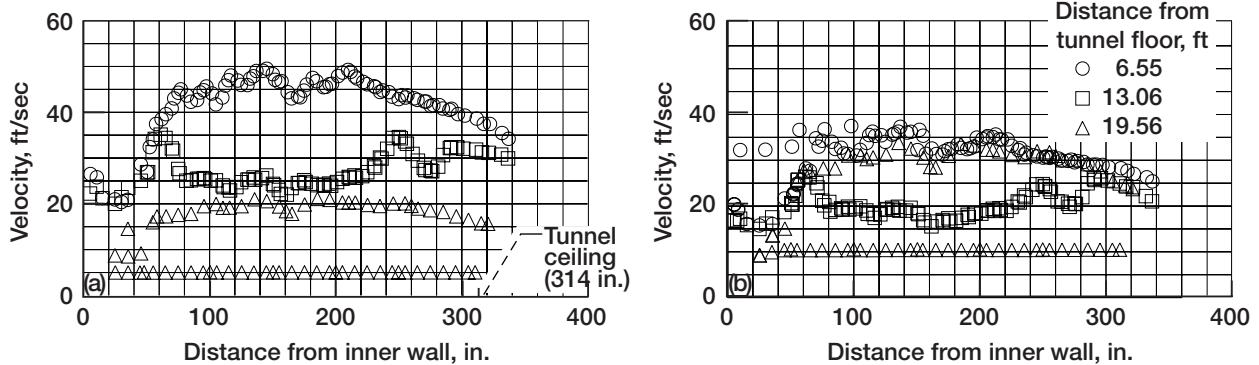


Figure 59.—Velocity distribution along horizontal surveys upstream of spraybars (station 5) as measured by pitot-static probes. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

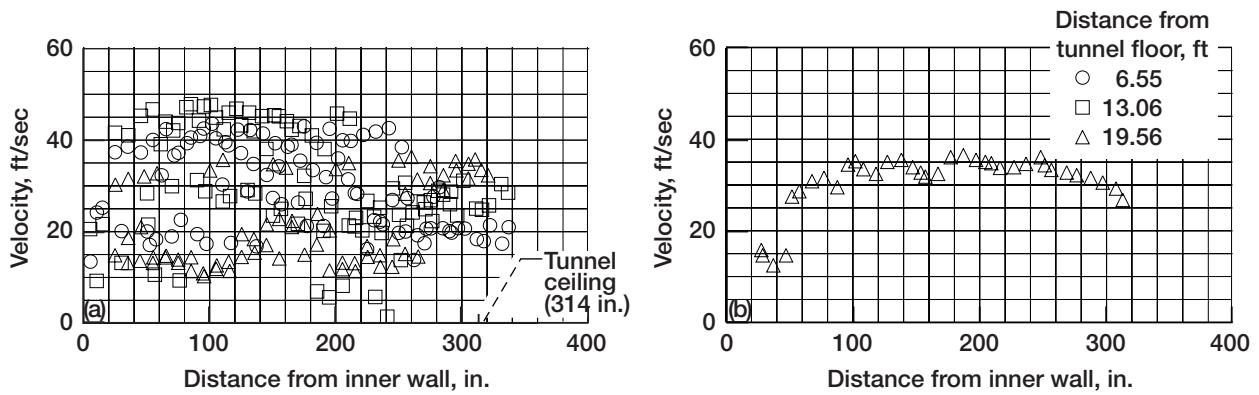


Figure 60.—Velocity distribution along horizontal surveys upstream of spraybars (station 5) as measured by wind anemometers. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

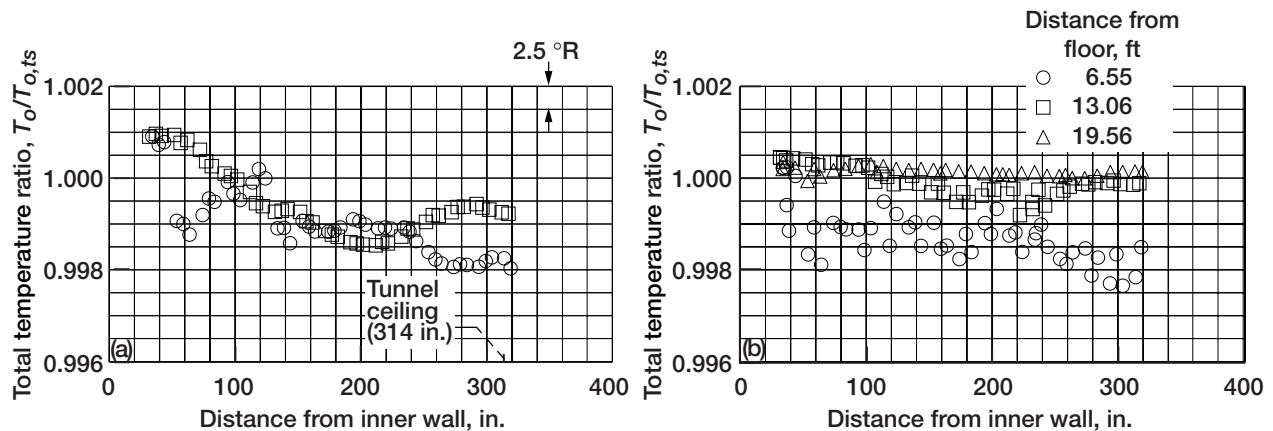


Figure 61.—Total temperature ratio distribution along horizontal surveys upstream of spraybars (station 5) as measured by wind anemometers. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

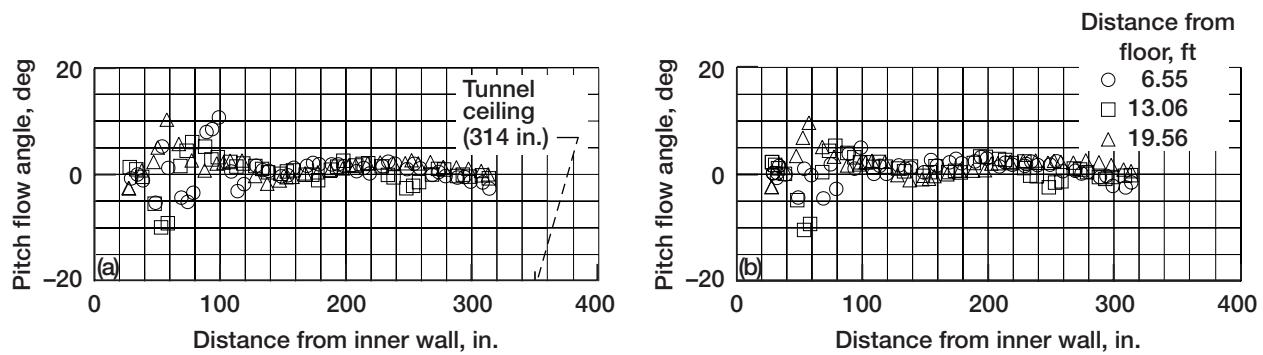


Figure 62.—Pitch flow angle distributions along horizontal surveys upstream of spraybars (station 5) as measured by wind anemometers. Positive angles indicate upflow. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

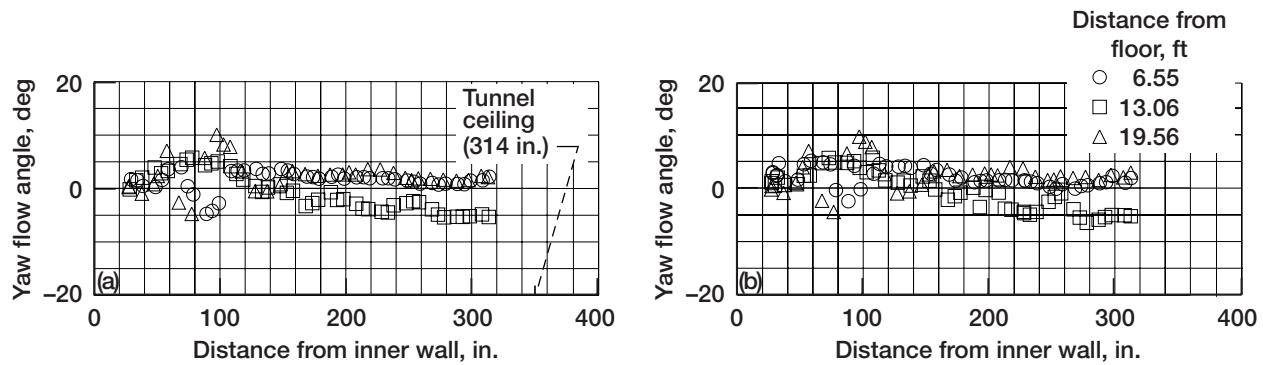


Figure 63.—Yaw flow angle distributions along horizontal surveys upstream of spraybars (station 5) as measured by wind anemometers. Positive angles indicate flow toward outside tunnel wall. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

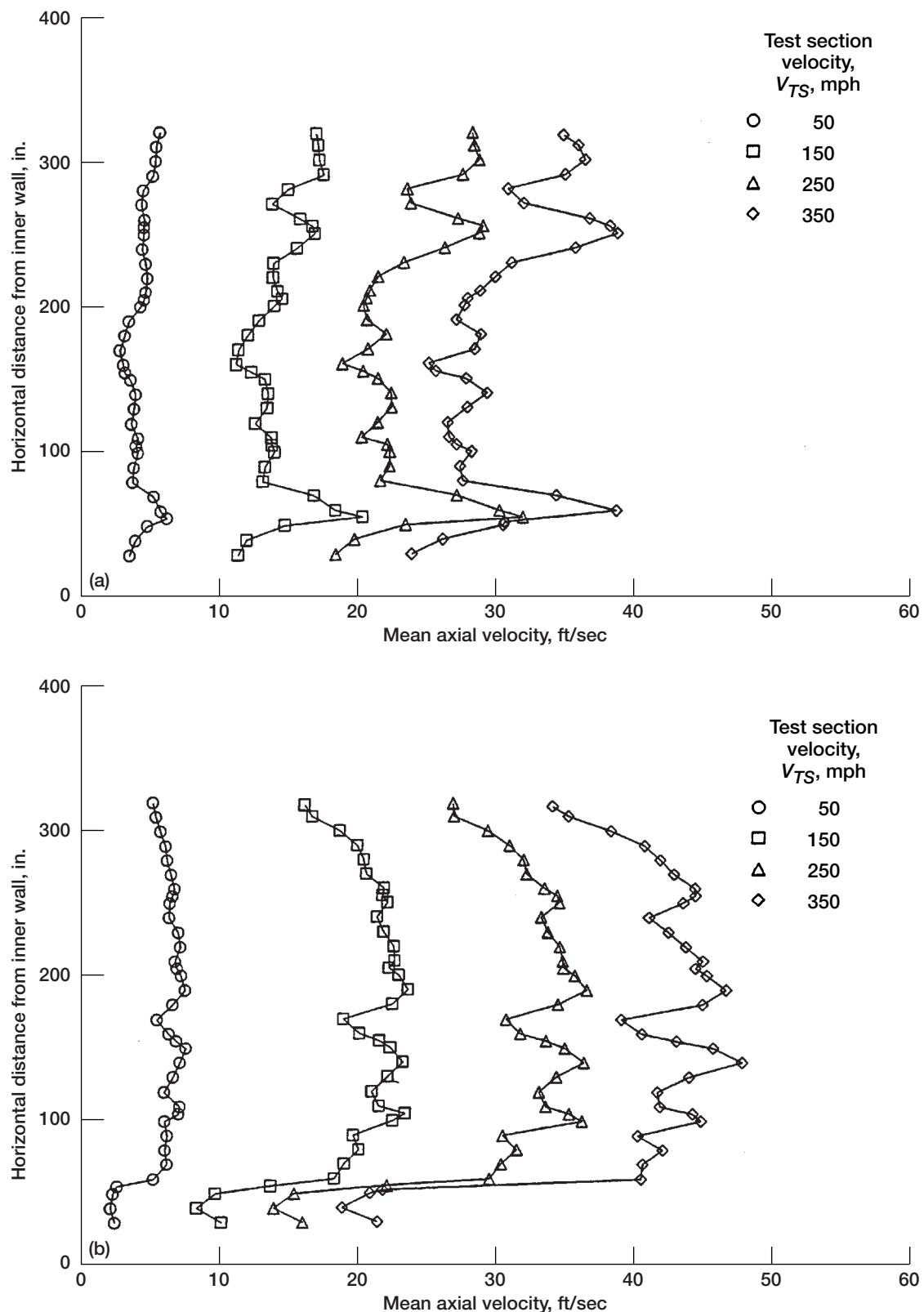


Figure 64.—Mean axial velocity distributions along horizontal surveys upstream of spraybars (station 5) as measured by hot-wire anemometers. (a) Mean axial velocity for traverse 1(13.06 ft above tunnel floor). (b) Mean axial velocity for traverse 2 (19.56 ft above the tunnel floor).

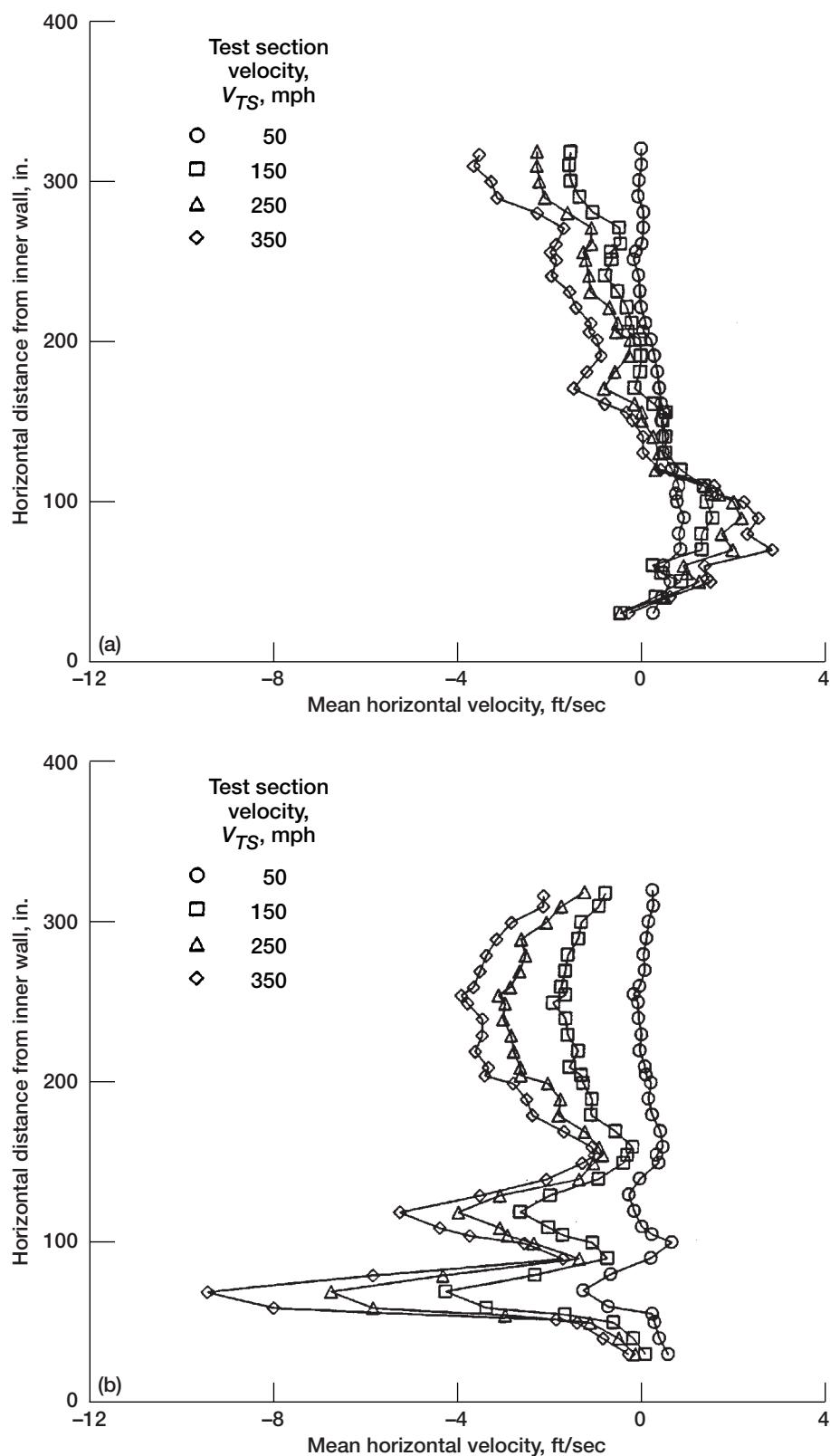


Figure 65.—Mean horizontal velocity distributions along horizontal surveys upstream of spraybars (station 5) as measured by hot-wire anemometers. (a) Mean horizontal velocity for traverse 1 (13.06 ft above tunnel floor). (b) Mean horizontal velocity for traverse 2 (19.56 ft above the tunnel floor).

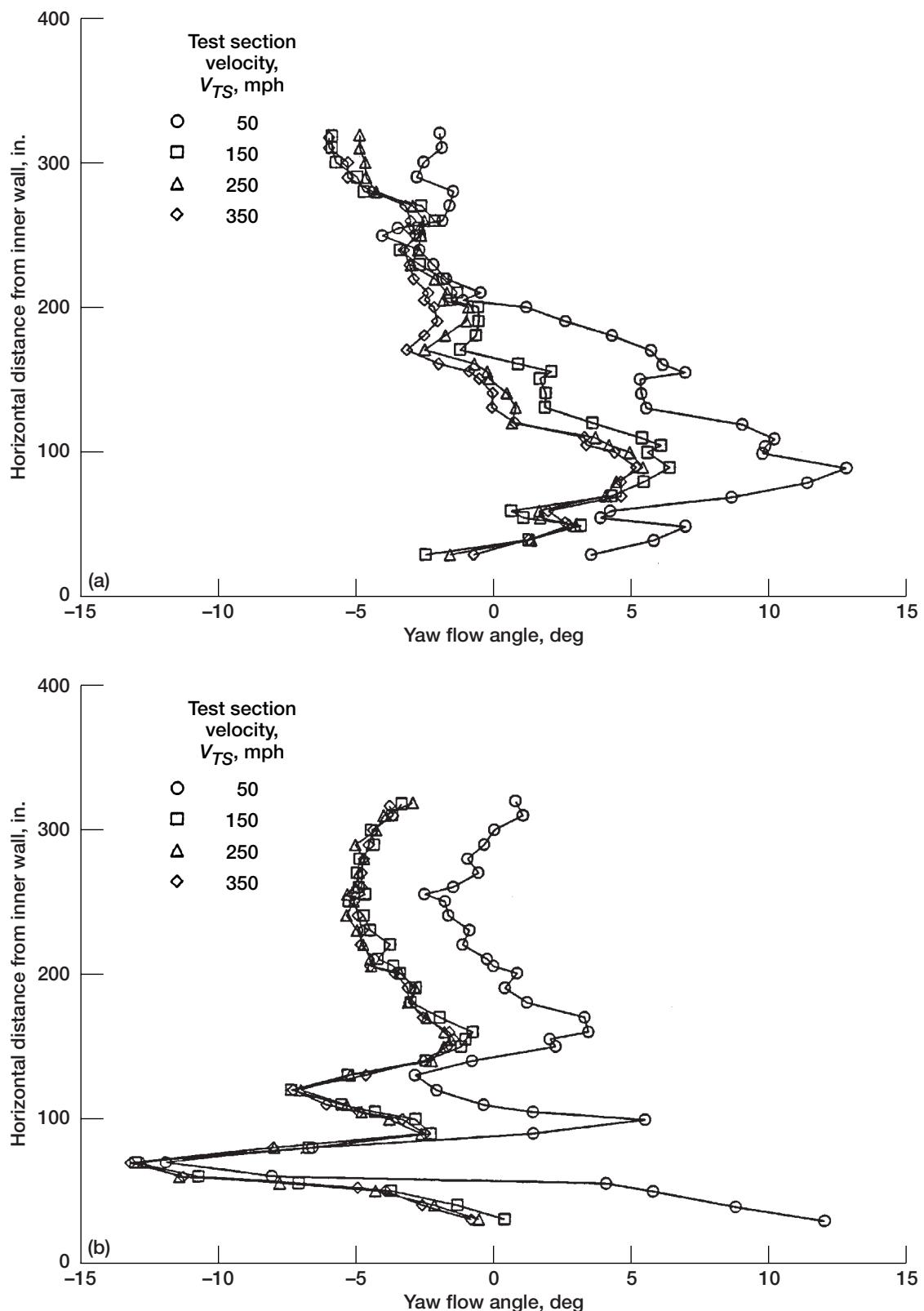


Figure 66.—Yaw flow angle distribution along horizontal surveys upstream of spraybars (station 5) as measured by hot-wire anemometers. Positive angles indicate flow toward outside tunnel wall.
 (a) Traverse 1 (centerline surveys at 13.06 ft above the tunnel floor). (b) Traverse 2 (upper survey at 19.56 ft above the tunnel floor).

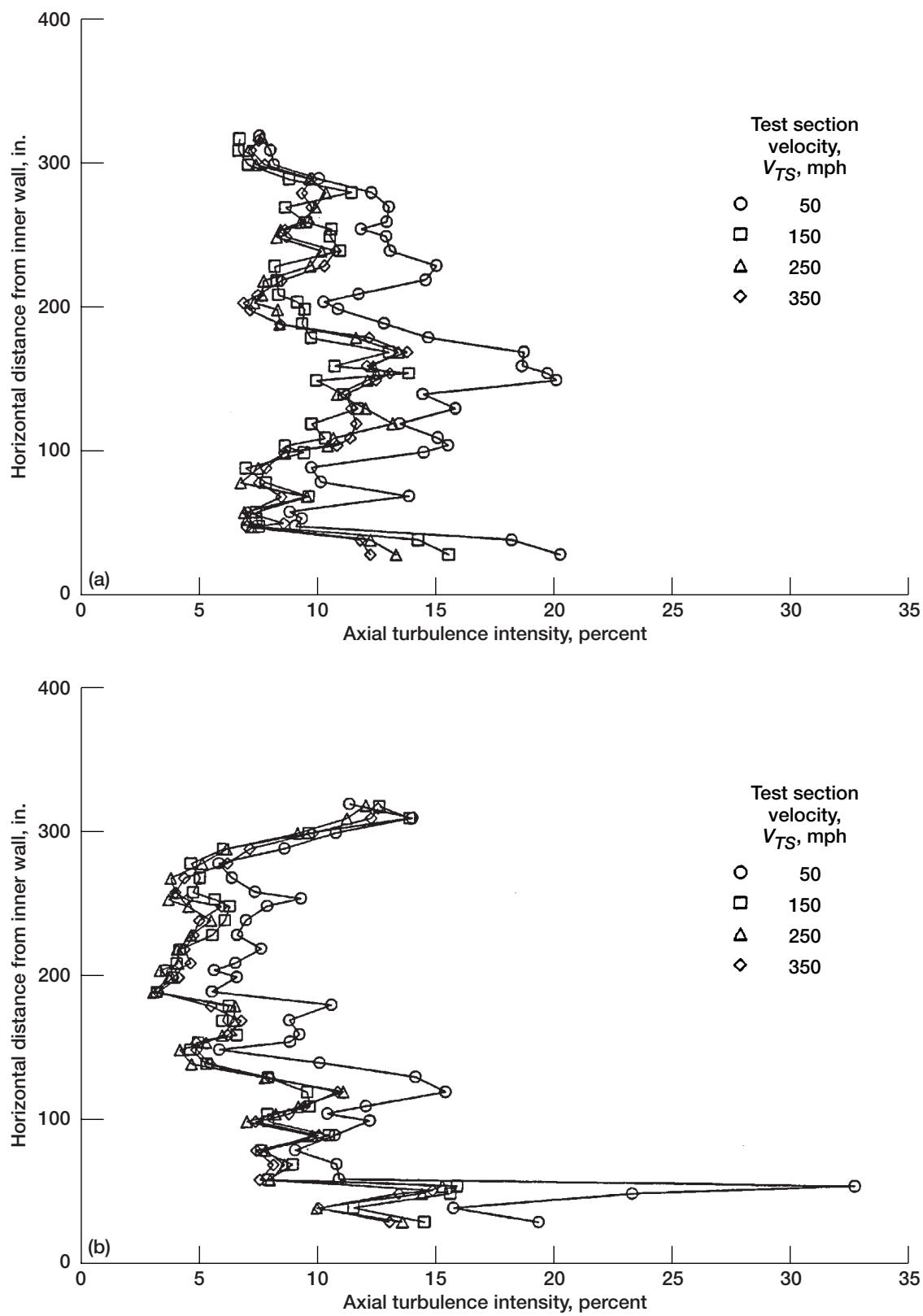


Figure 67.—Axial turbulence intensity along horizontal surveys upstream of spraybars (station 5).
(a) Traverse 1 (centerline surveys at 13.06 ft above the tunnel floor). (b) Traverse 2 (upper survey at 19.56 ft above the tunnel floor).

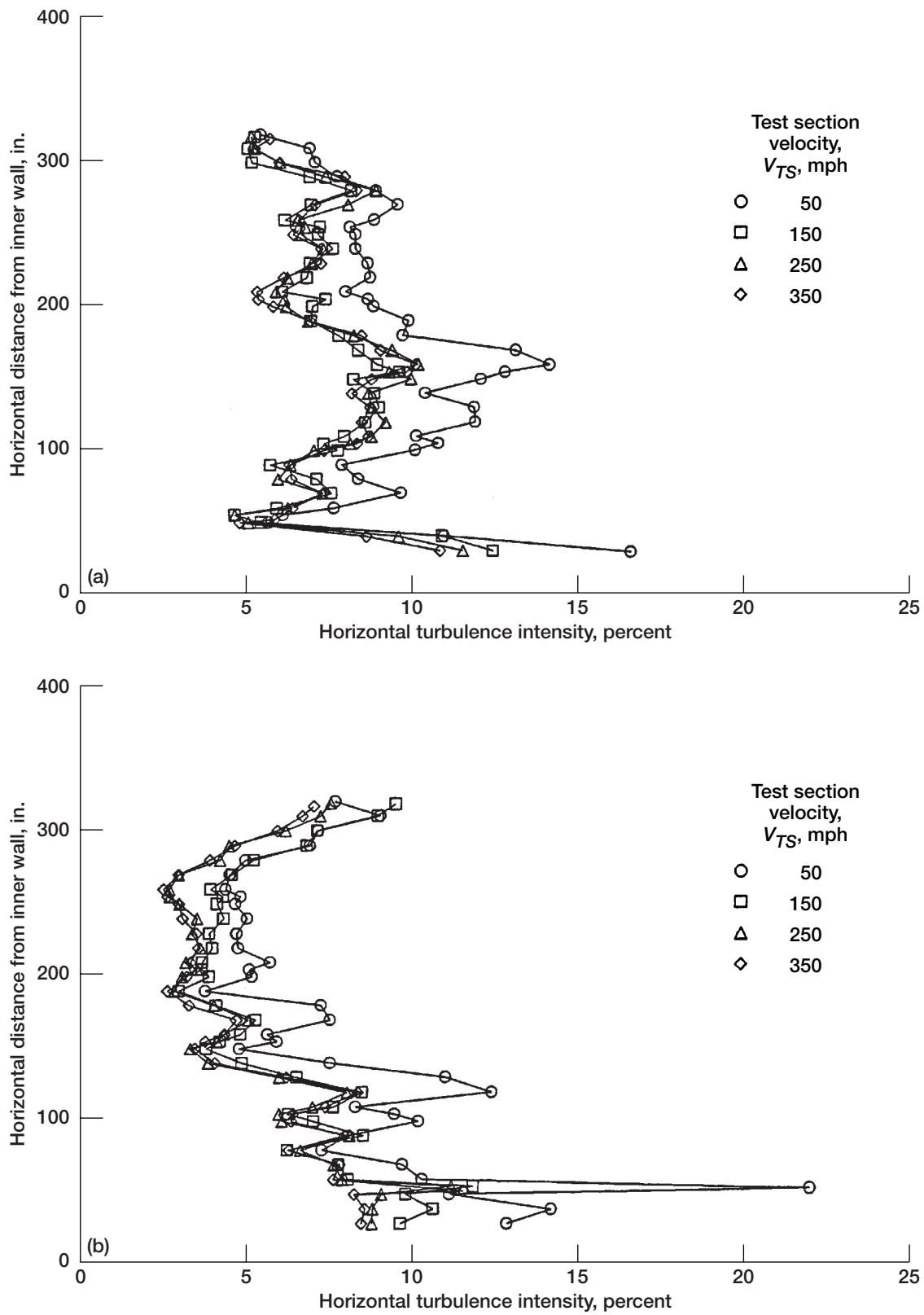


Figure 68.—Horizontal turbulence intensity along horizontal surveys upstream of spraybars (station 5).
 (a) Traverse 1 (centerline surveys at 13.06 ft above the tunnel floor). (b) Traverse 2 (upper survey at 19.56 ft above the tunnel floor).

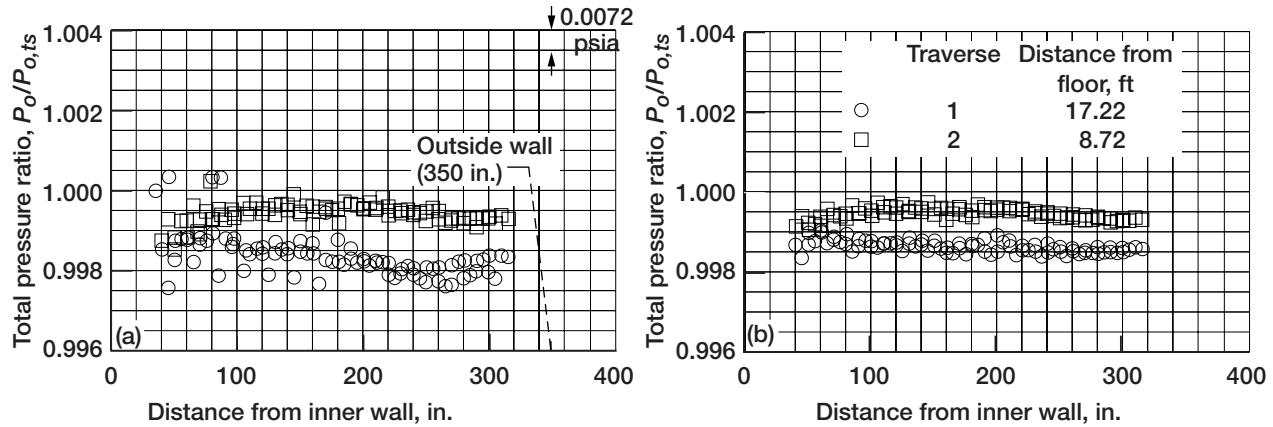


Figure 69.—Total pressure ratio distribution along horizontal surveys downstream of spraybars (station 6).
(a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

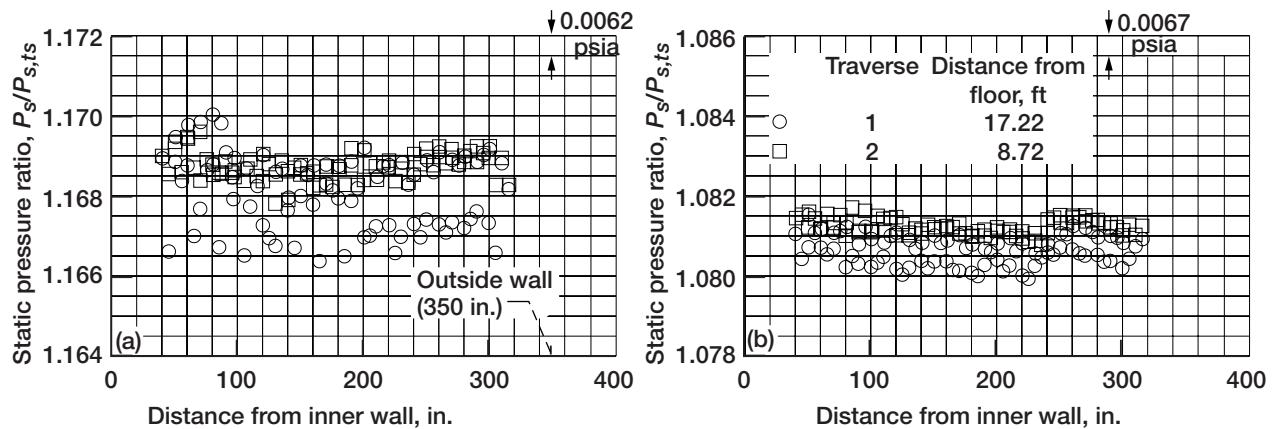


Figure 70.—Static pressure ratio distribution along horizontal surveys downstream of spraybars (station 6).
(a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

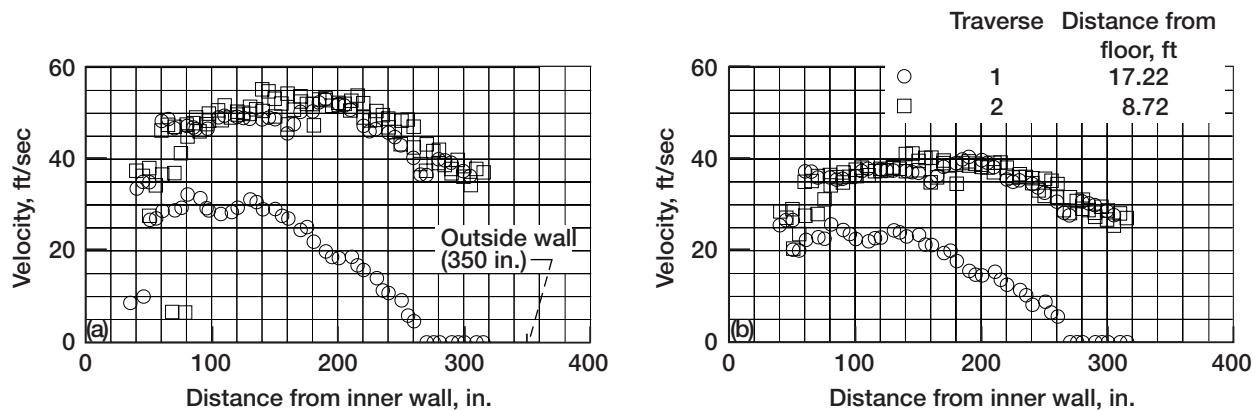


Figure 71.—Velocity distribution along horizontal surveys downstream of spraybars (station 6) as measured by pitot-static probes. (a) $V_{TS} = 350 \text{ mph}$. (b) $V_{TS} = 250 \text{ mph}$. (Note that the data provided by probe 1 on traverse 1 are in error due to an error in the measurement of ΔP ; all other data are correct.)

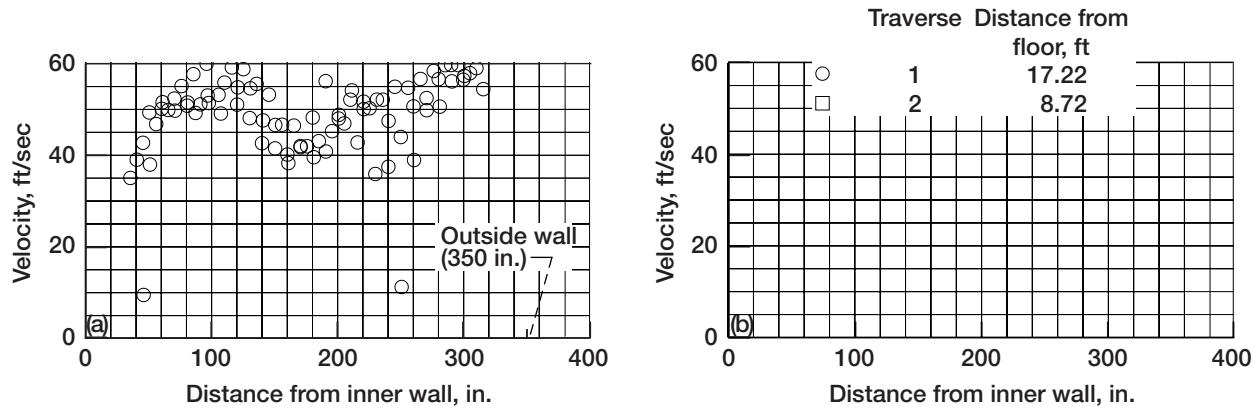


Figure 72.—Velocity distribution along horizontal surveys downstream of spraybars (station 6) as measured by wind anemometers. (a) $V_{TS} = 350 \text{ mph}$. (b) $V_{TS} = 250 \text{ mph}$.

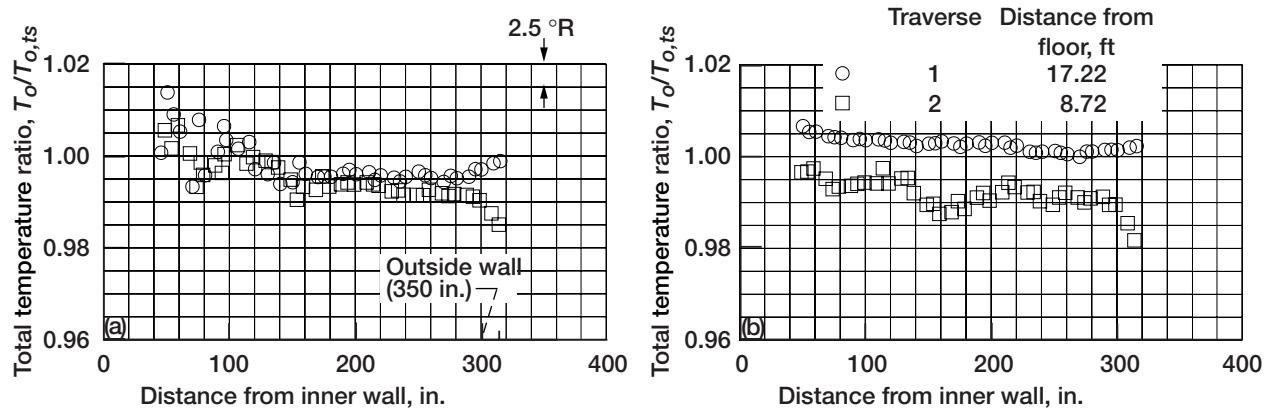


Figure 73.—Total temperature ratio distribution along horizontal surveys downstream of spraybars (station 6). (a) $V_{TS} = 350 \text{ mph}$. (b) $V_{TS} = 250 \text{ mph}$.

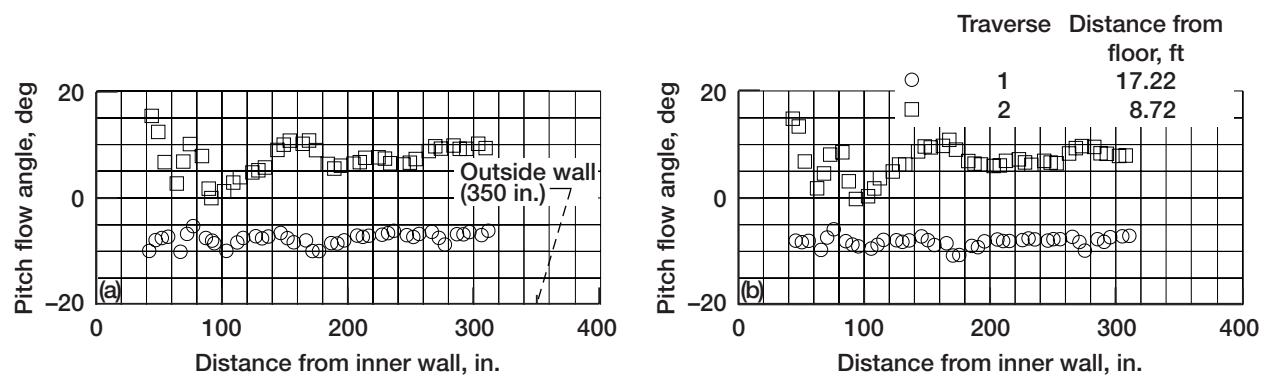


Figure 74.—Pitch flow angle distribution along horizontal surveys downstream of spraybars (station 6).
(a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

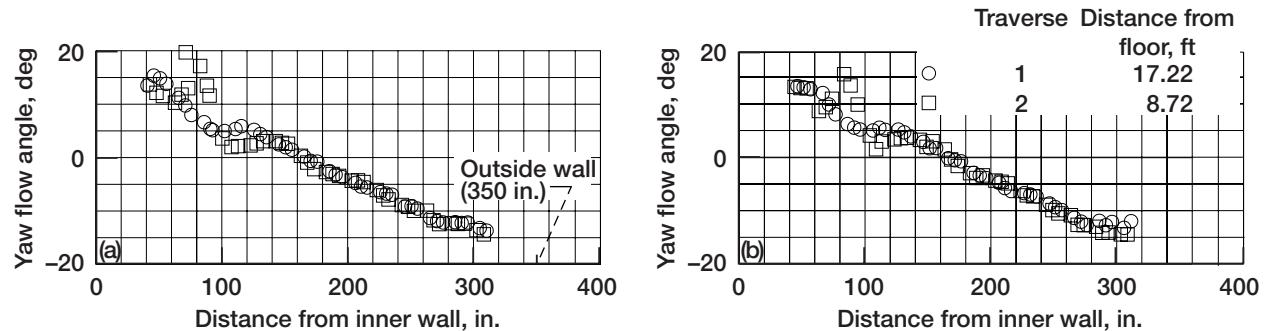


Figure 75.—Yaw flow angle distribution along horizontal surveys downstream of spraybars (station 6).
(a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

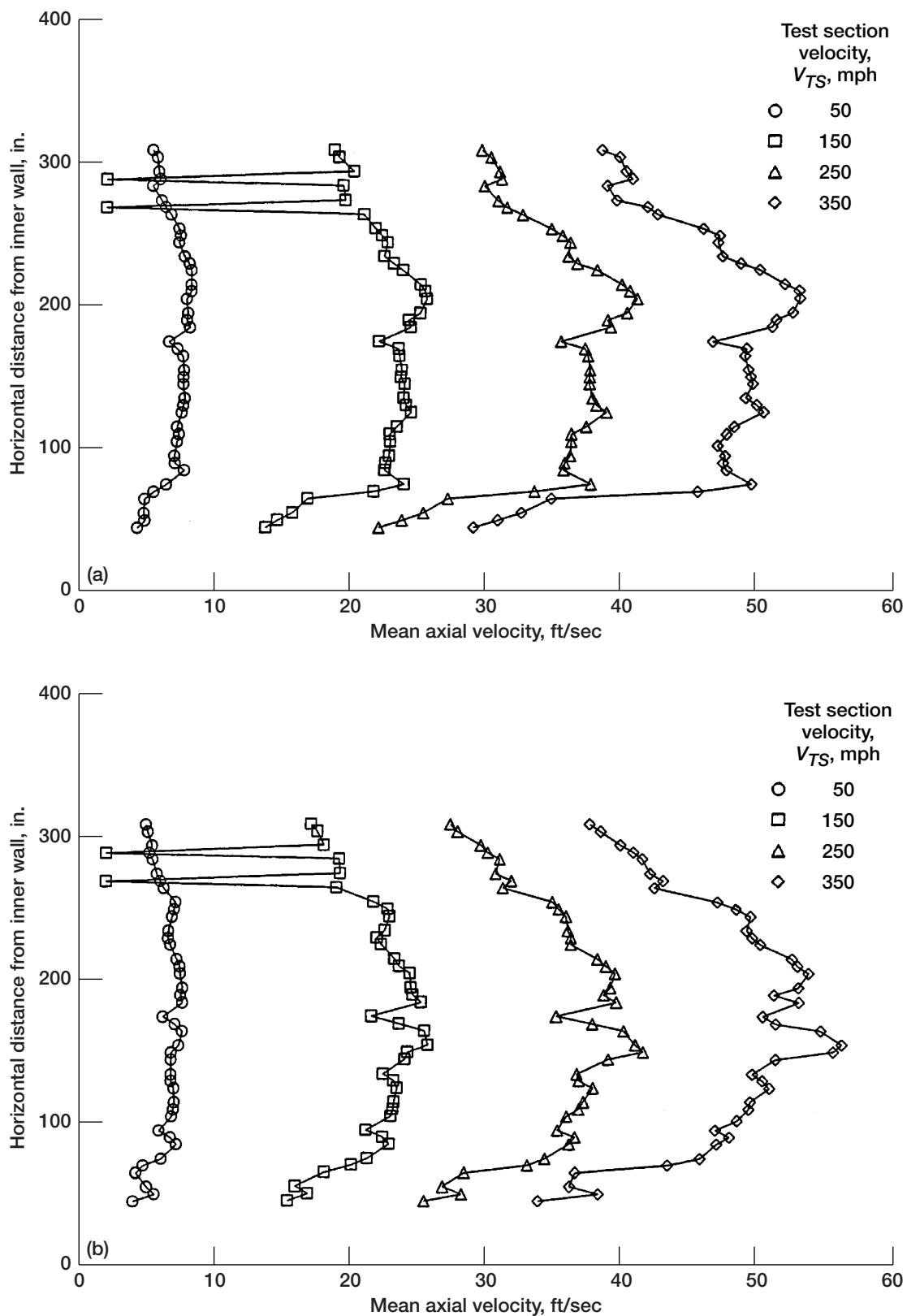


Figure 76.—Mean axial velocity distributions along horizontal surveys downstream of spraybars (station 6) as measured by hot-wire anemometers. (a) Traverse 1 (17.2 ft above tunnel floor). (b) Traverse 2 (8.72 ft above tunnel floor).

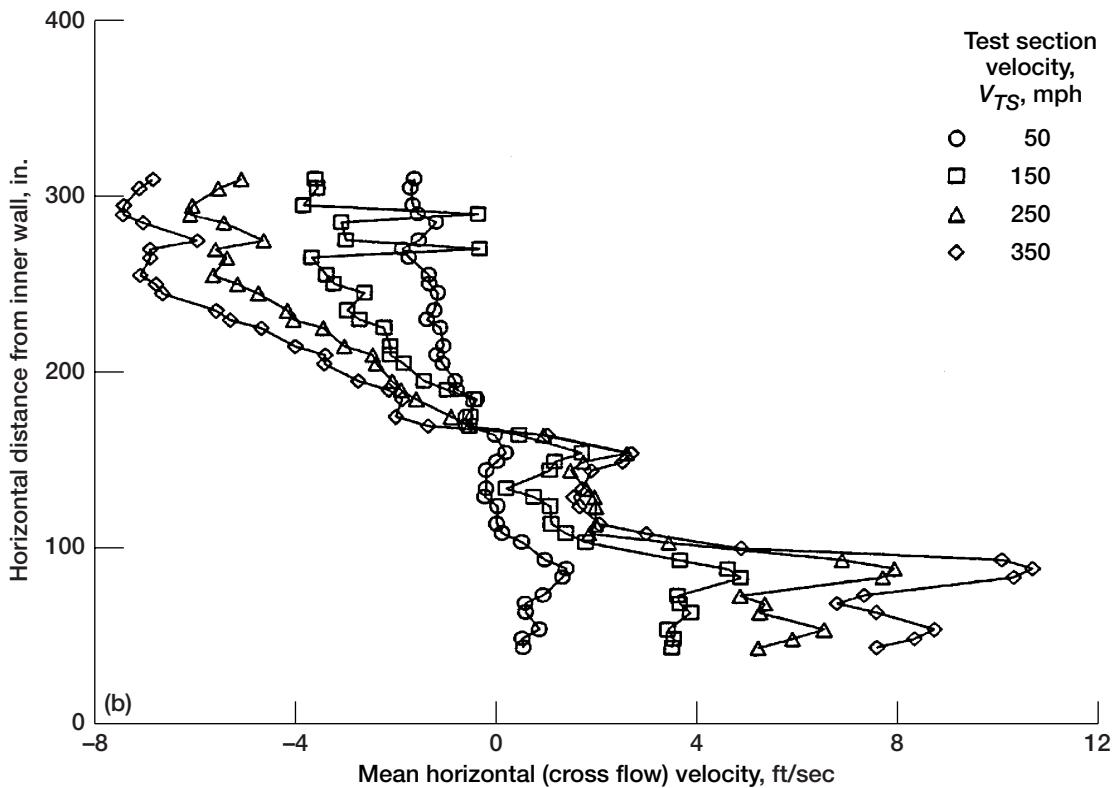
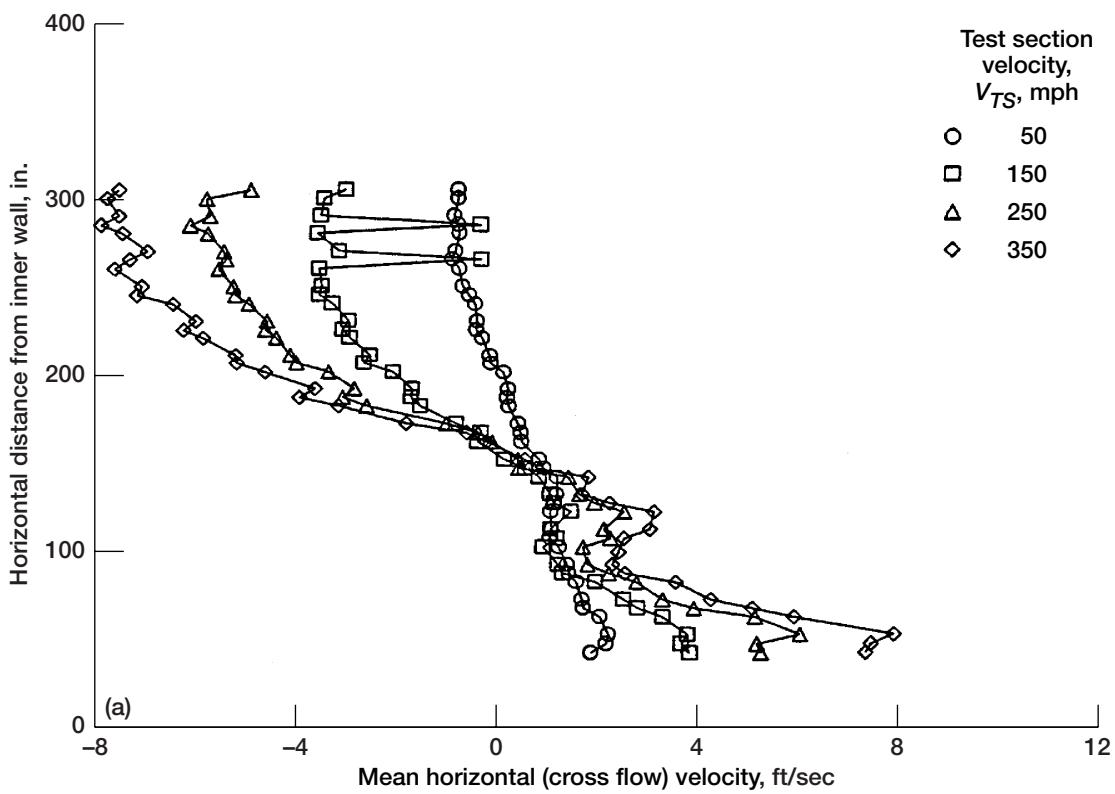


Figure 77.—Mean horizontal (cross flow) velocity distribution along horizontal surveys downstream of spraybars (station 6) as measured by hot-wire anemometers. (a) Traverse 1 (17.2 ft above tunnel floor). (b) Traverse 2 (8.72 ft above tunnel floor).

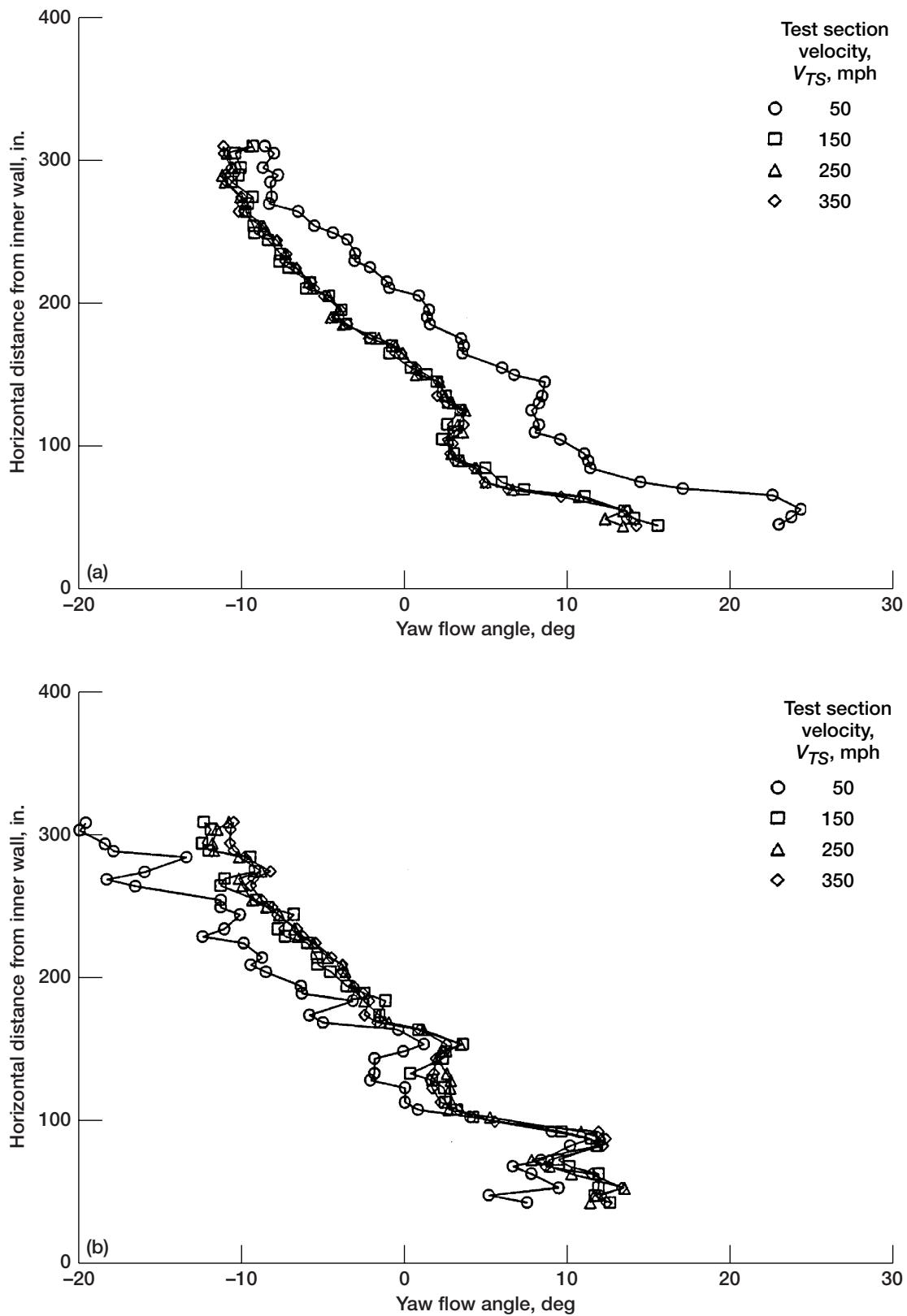


Figure 78.—Yaw flow angle distribution along horizontal surveys downstream of spraybars (station 6) as measured by hot-wire anemometers. (a) Traverse 1 (17.2 ft above tunnel floor). (b) Traverse 2 (8.72 ft above tunnel floor).

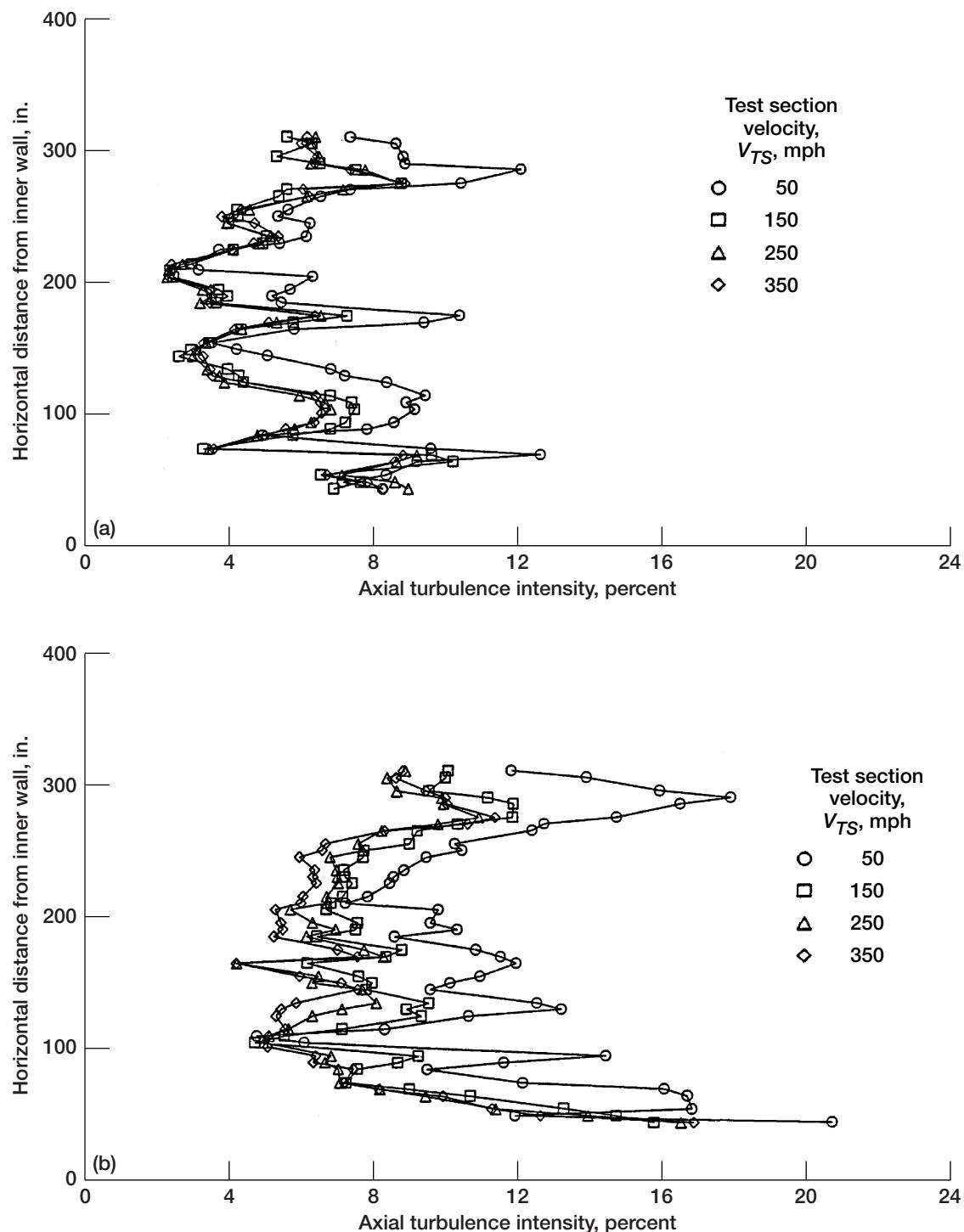


Figure 79.—Axial turbulence intensity distribution along horizontal surveys downstream of spraybars (station 6) as measured by hot-wire anemometers. (a) Traverse 1 (17.2 ft above tunnel floor). (b) Traverse 2 (8.72 ft above tunnel floor).

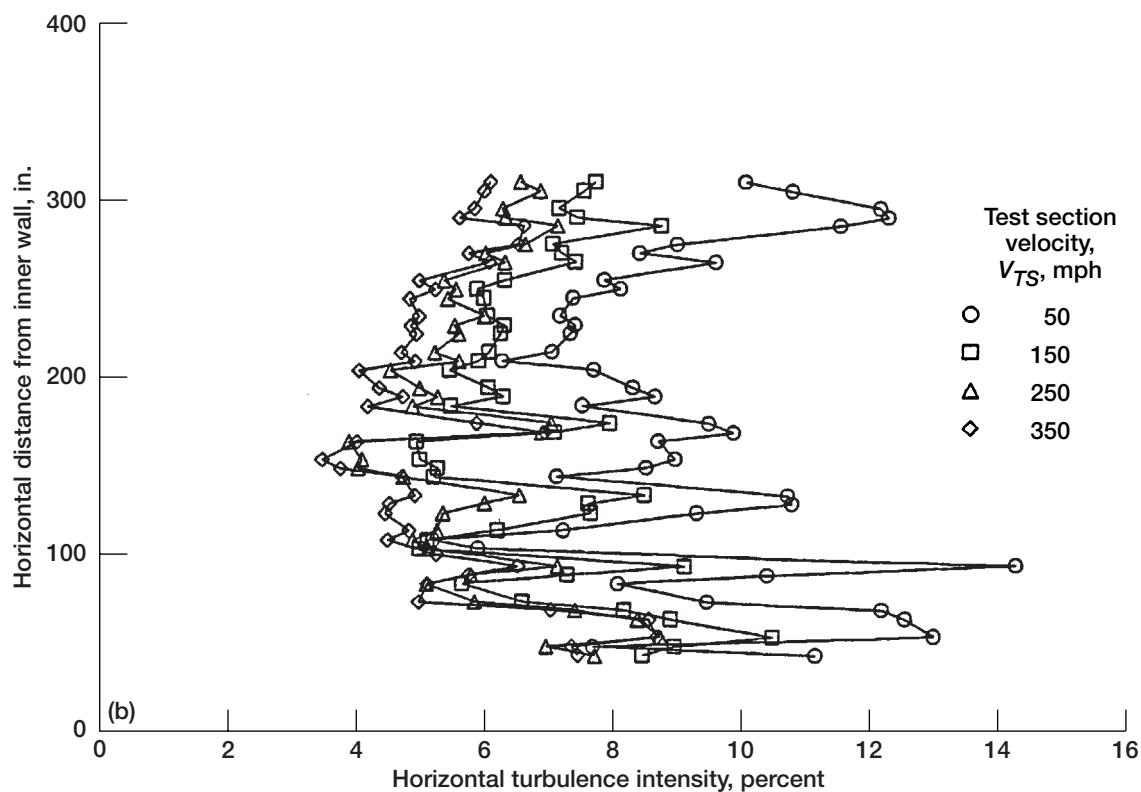
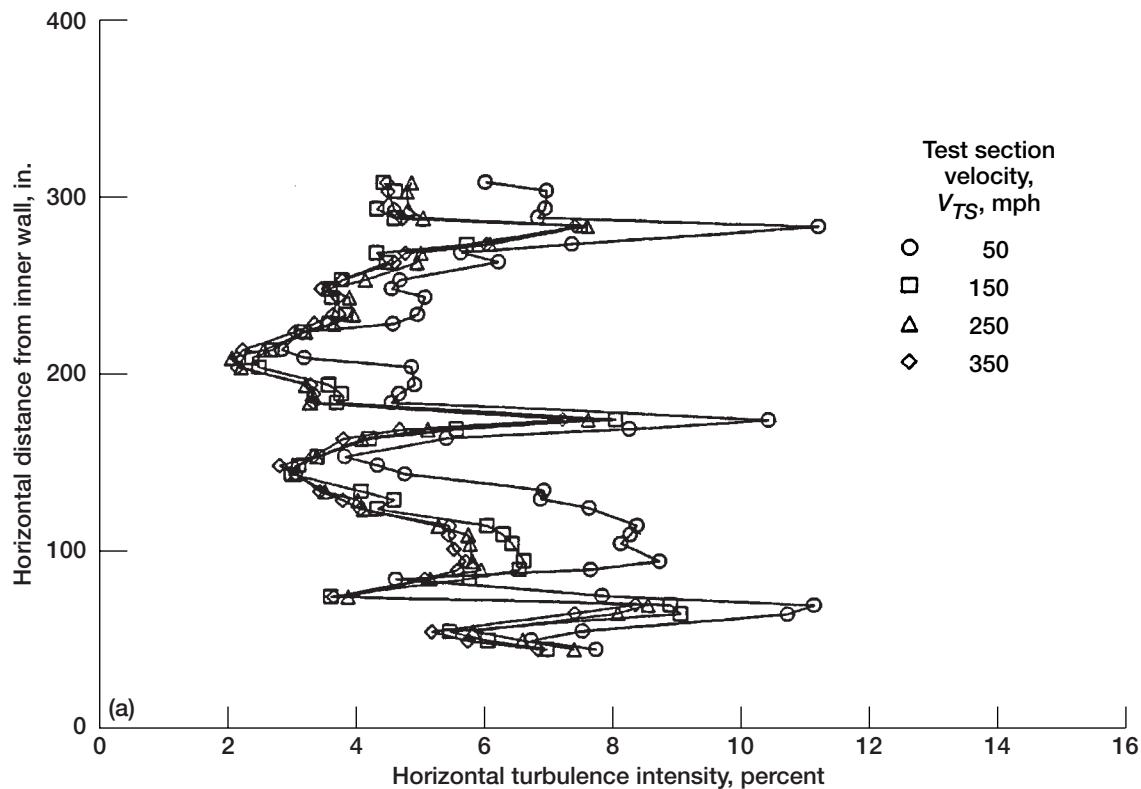


Figure 80.—Horizontal turbulence intensity distribution along horizontal surveys downstream of spraybars (station 6) as measured by hot-wire anemometers. (a) Traverse 1 (17.2 ft above tunnel floor). (b) Traverse 2 (8.72 ft above tunnel floor).

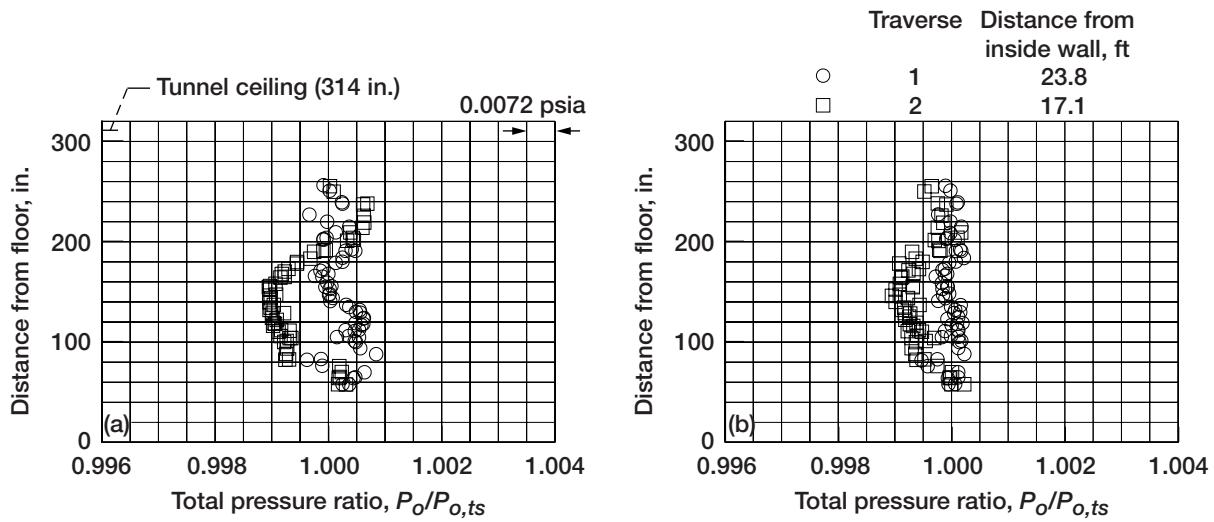


Figure 81.—Total pressure ratio distribution along vertical surveys downstream of heat exchanger (station 4). Traverse 2 was directly downstream of part of heat exchanger from which exit guide vanes had been removed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

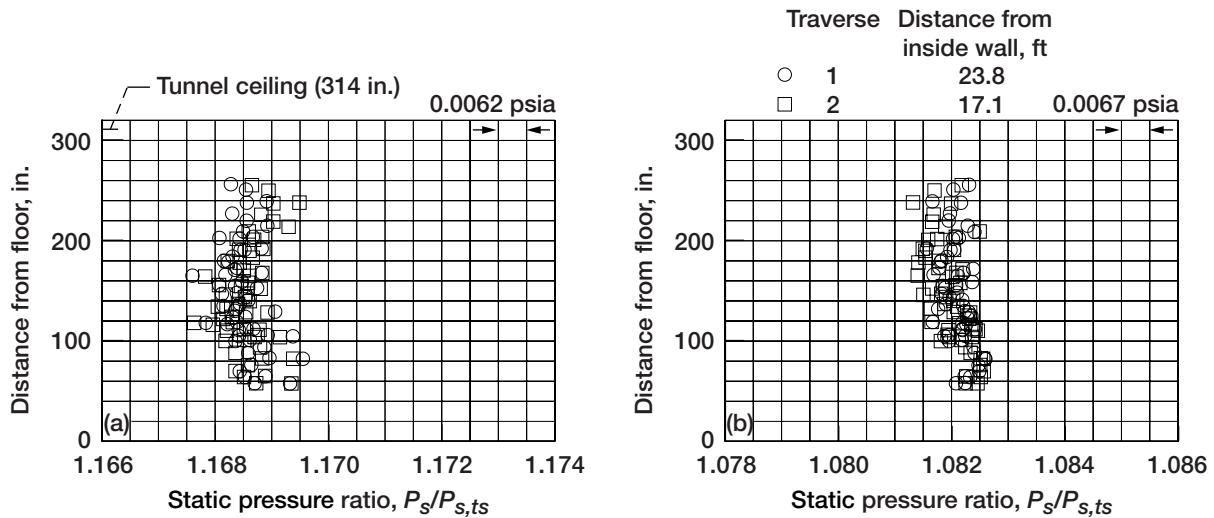


Figure 82.—Static pressure ratio distribution along vertical surveys downstream of heat exchanger (station 4). Traverse 2 was directly downstream of part of heat exchanger from which exit guide vanes had been removed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

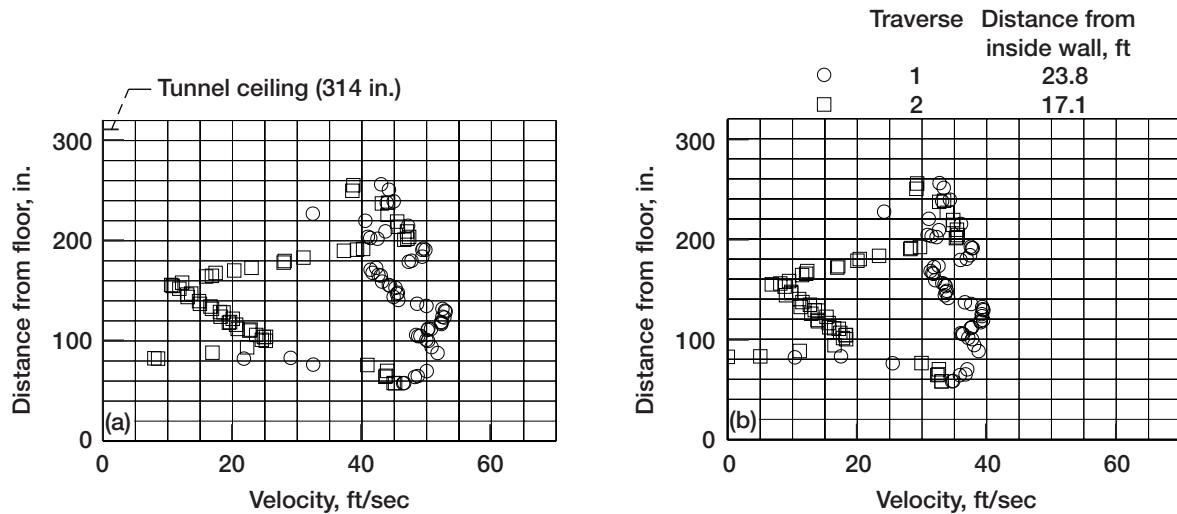


Figure 83.—Velocity distribution along vertical surveys downstream of heat exchanger (station 4) as measured by pitot-static probes. Traverse 2 was directly downstream of part of heat exchanger from which exit guide vanes had been removed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

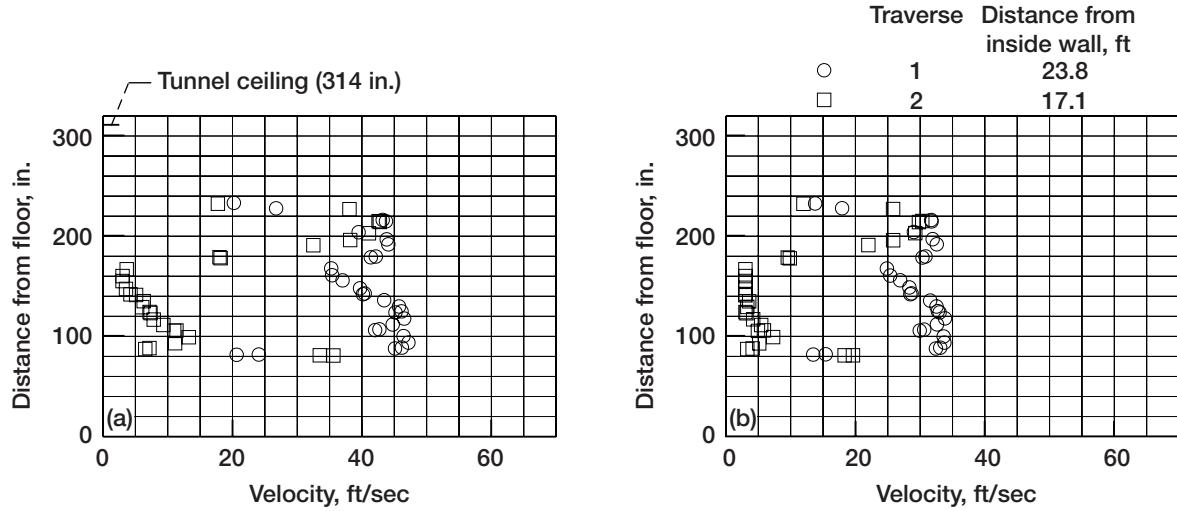


Figure 84.—Velocity distribution along vertical surveys downstream of heat exchanger (station 4) as measured by wind anemometers. Traverse 2 was directly downstream of part of heat exchanger from which exit guide vanes had been removed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

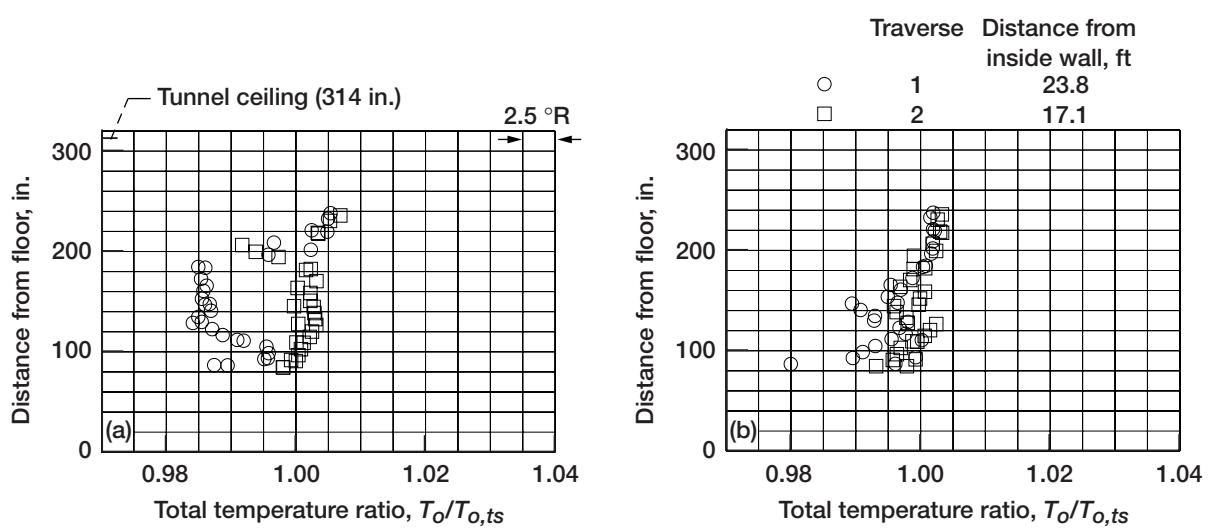


Figure 85.—Total temperature ratio along vertical surveys downstream of heat exchanger (station 4). Traverse 2 was directly downstream of part of heat exchanger from which exit guide vanes had been removed. (a) $V_{TS} = 350 \text{ mph}$. (b) $V_{TS} = 250 \text{ mph}$.

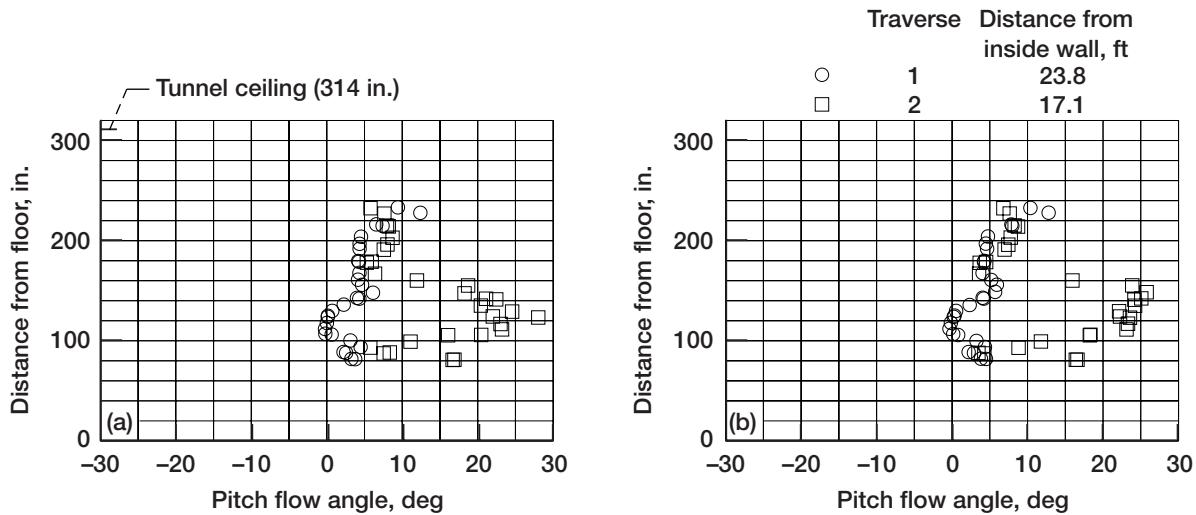


Figure 86.—Pitch flow angle distribution along vertical surveys downstream of heat exchanger (station 4) as measured by wind anemometers. Traverse 2 was directly downstream of part of heat exchanger from which exit guide vanes had been removed (positive angles indicate upflow). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

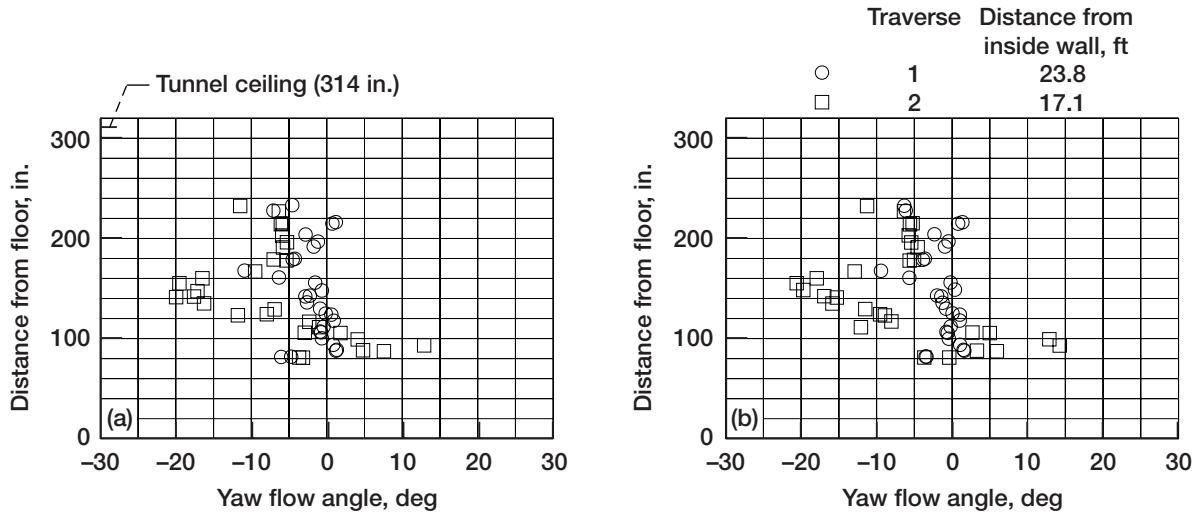


Figure 87.—Yaw flow angle distribution along vertical surveys downstream of heat exchanger (station 4). Traverse 2 was directly downstream of part of heat exchanger from which exit guide vanes had been removed (positive angles indicate flow toward outside tunnel wall). (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

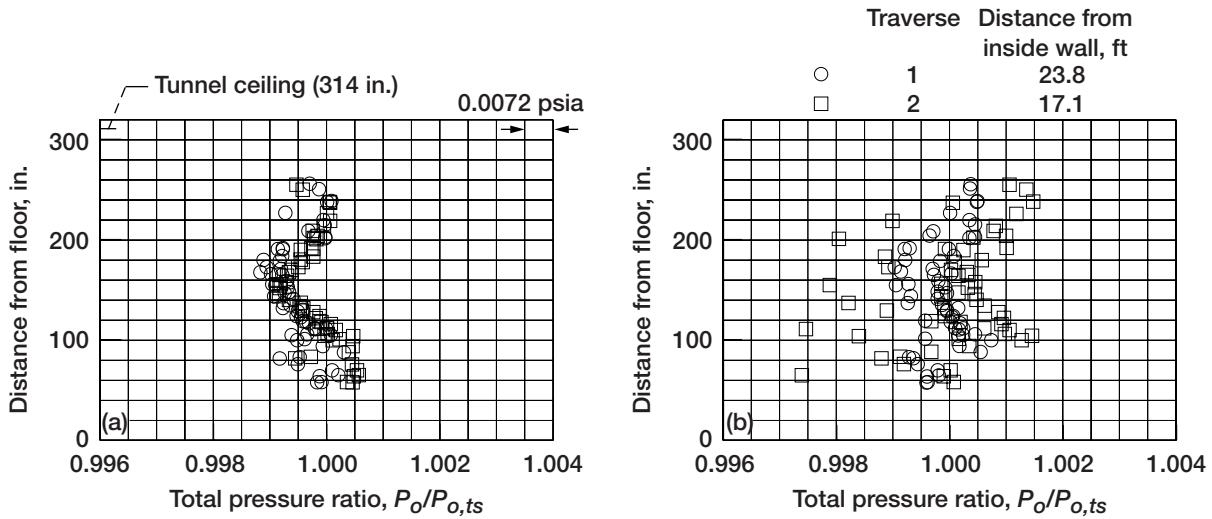


Figure 88.—Total pressure ratio distribution along vertical surveys downstream of heat exchanger (station 4). Traverse 2 was directly downstream of heat exchanger element two, where exit guide vanes had been installed but not deployed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

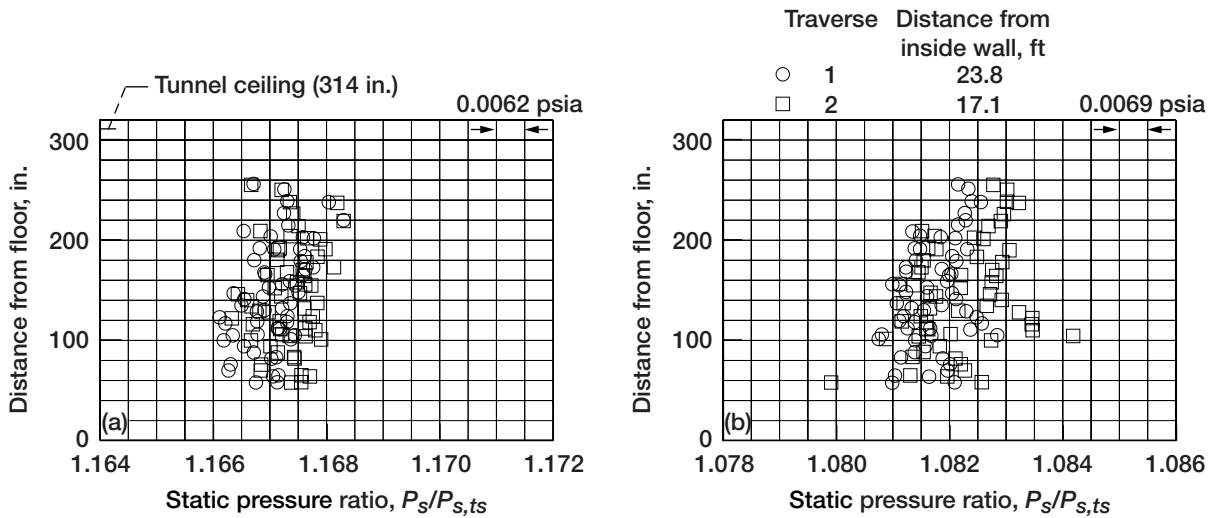


Figure 89.—Static pressure ratio distribution along vertical surveys downstream of heat exchanger (station 4). Traverse 2 was directly downstream of heat exchanger element two, where exit guide vanes had been installed but not deployed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

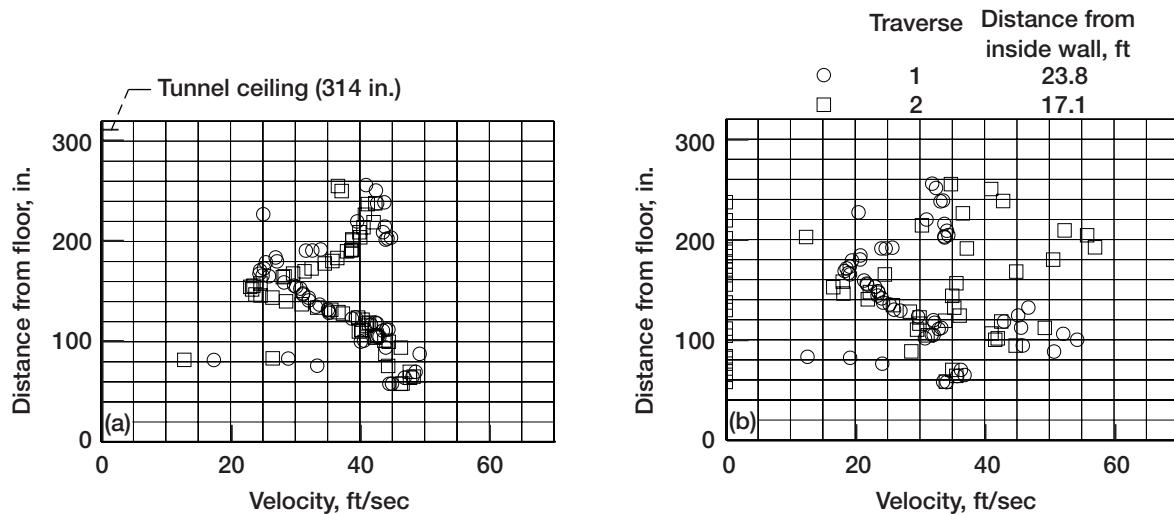


Figure 90.—Velocity distribution along vertical surveys downstream of heat exchanger (station 4) as measured by pitot-static probes. Traverse 2 was directly downstream of heat exchanger element two, where exit guide vanes had been installed but not deployed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

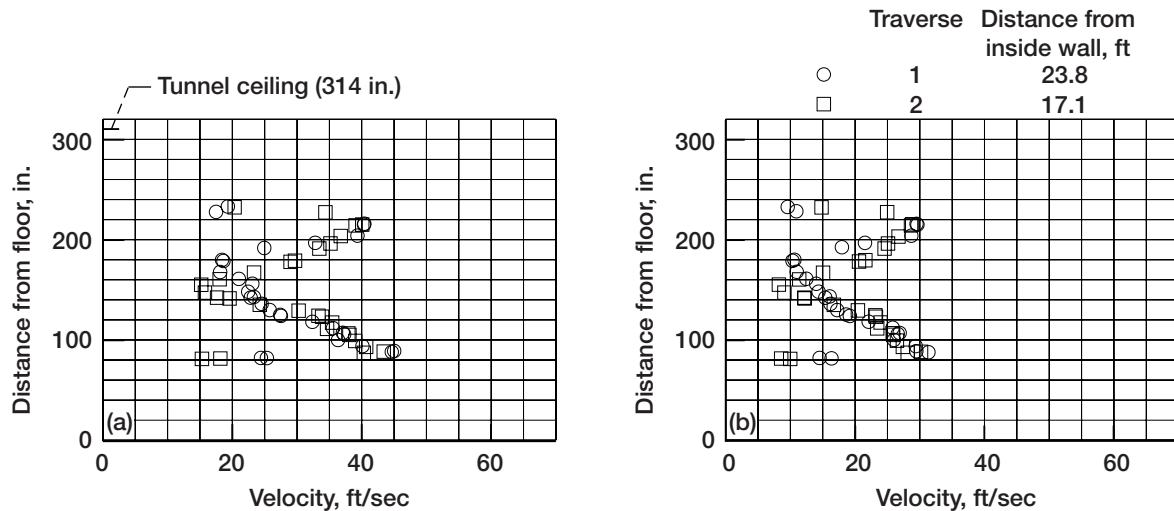


Figure 91.—Velocity distribution along vertical surveys downstream of heat exchanger (station 4) as measured by wind anemometers. Traverse 2 was directly downstream of heat exchanger element two, where exit guide vanes had been installed but not deployed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

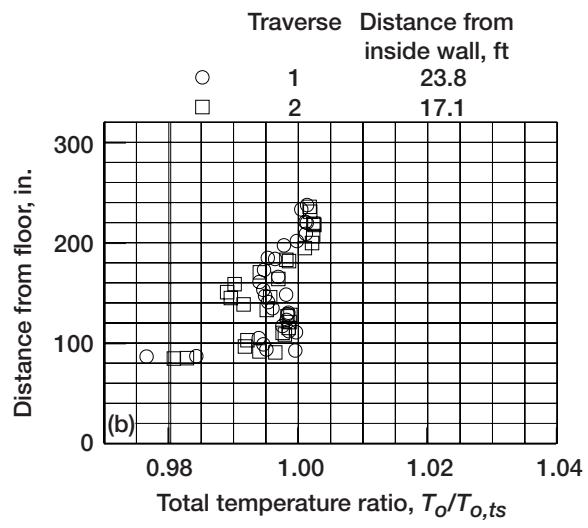
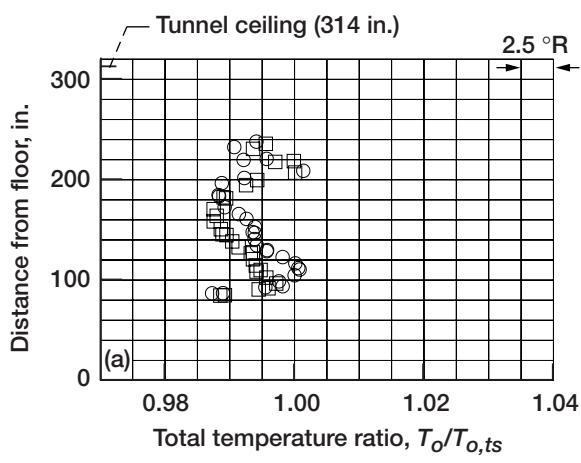


Figure 92.—Total temperature ratio distribution along vertical surveys downstream of heat exchanger (station 4) as measured by wind anemometers. Traverse 2 was directly downstream of heat exchanger element two, where exit guide vanes had been installed but not deployed. (a) $V_{TS} = 350$ mph.
 (b) $V_{TS} = 250$ mph.

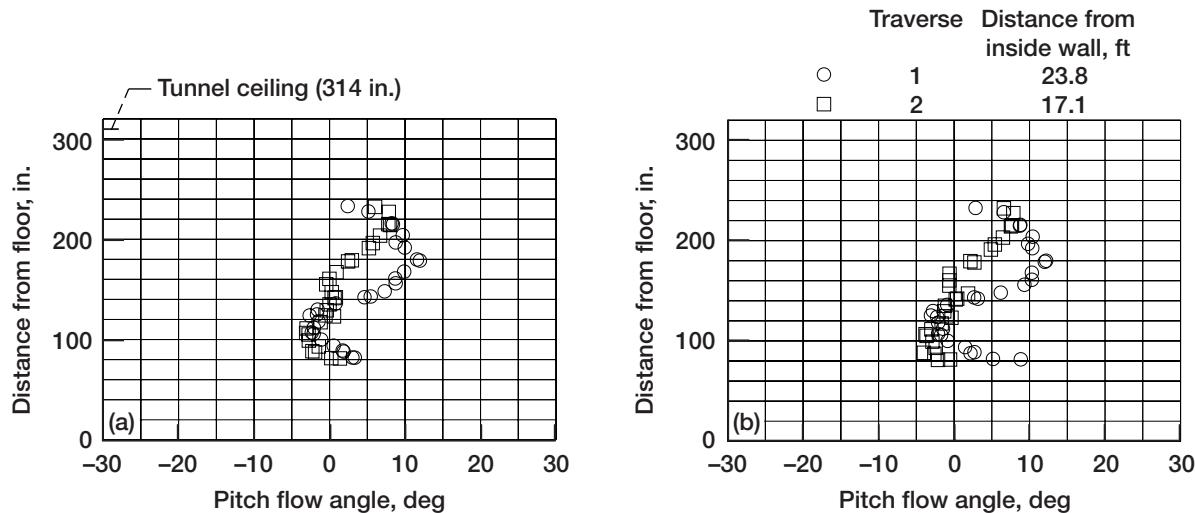


Figure 93.—Pitch flow angle distribution along vertical surveys downstream of heat exchanger (station 4) as measured by wind anemometers. Traverse 2 was directly downstream of heat exchanger element two, where exit guide vanes had been installed but not deployed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

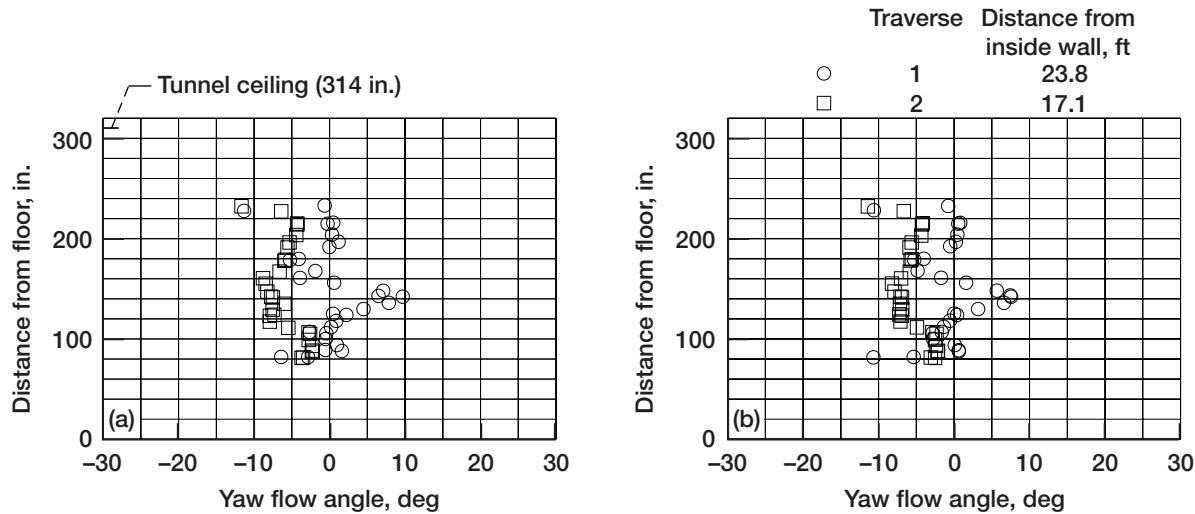


Figure 94.—Yaw flow angle distribution along vertical surveys downstream of heat exchanger (station 4) as measured by wind anemometers. Traverse 2 was directly downstream of heat exchanger element two, where exit guide vanes had been installed but not deployed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

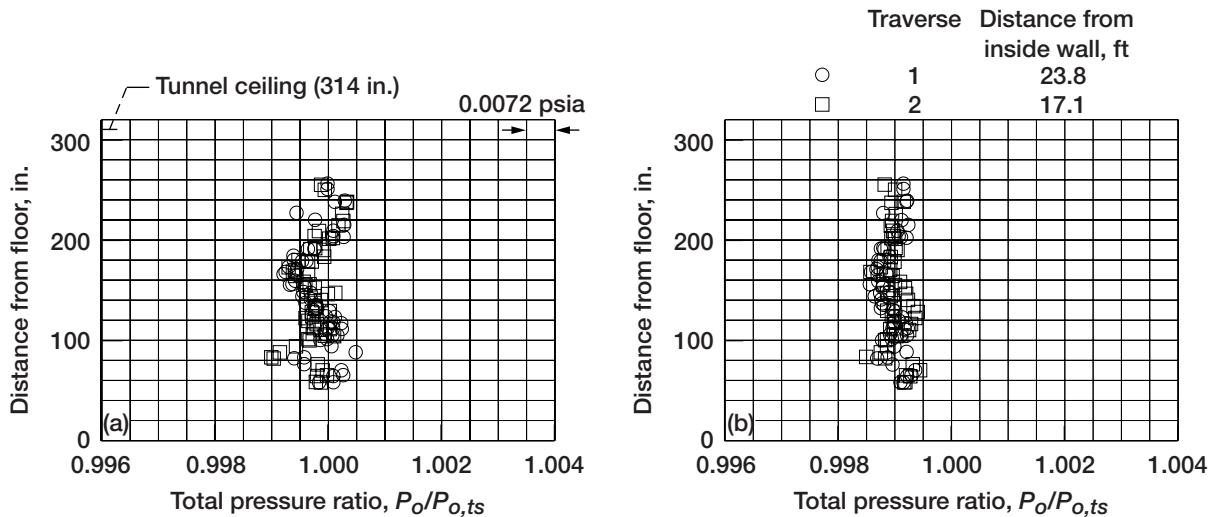


Figure 95.—Total pressure ratio distribution along vertical surveys downstream of heat exchanger (station 4). Traverse 2 was directly downstream of heat exchanger element two, where exit guide vanes had been installed and deployed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

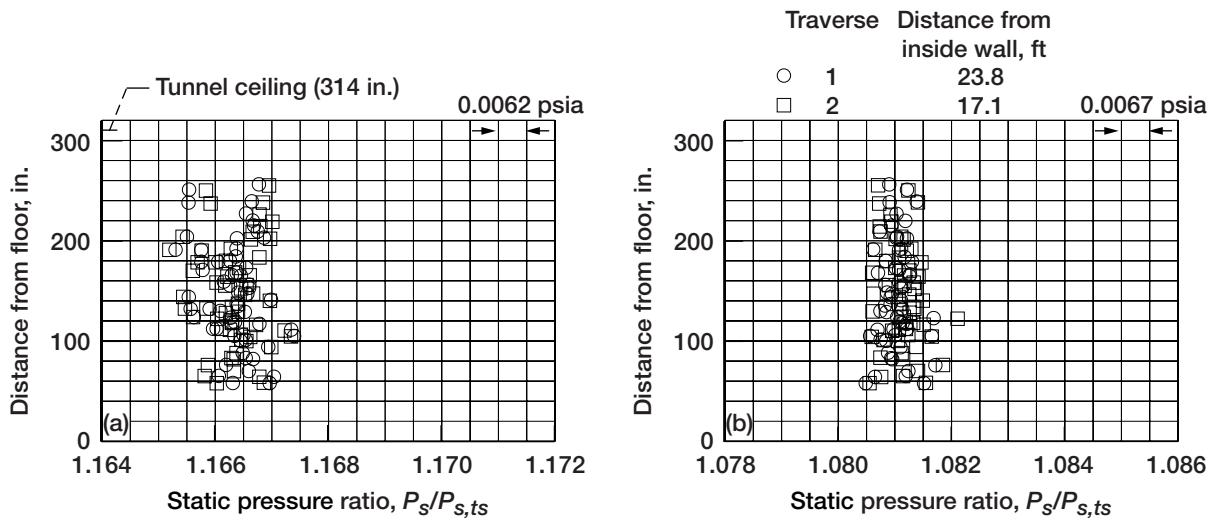


Figure 96.—Static pressure ratio distribution along vertical surveys downstream of heat exchanger (station 4). Traverse 2 was directly downstream of heat exchanger element two, where exit guide vanes had been installed but not deployed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

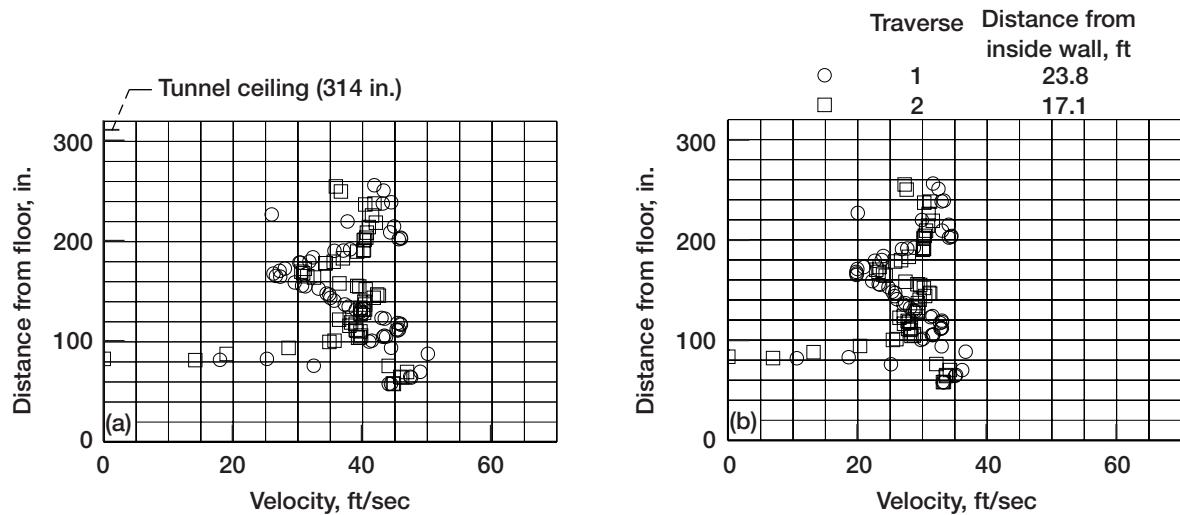


Figure 97.—Velocity distribution along vertical surveys downstream of heat exchanger (station 4) as measured by pitot-static probes. Traverse 2 was directly downstream of heat exchanger element two, where exit guide vanes had been installed and deployed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

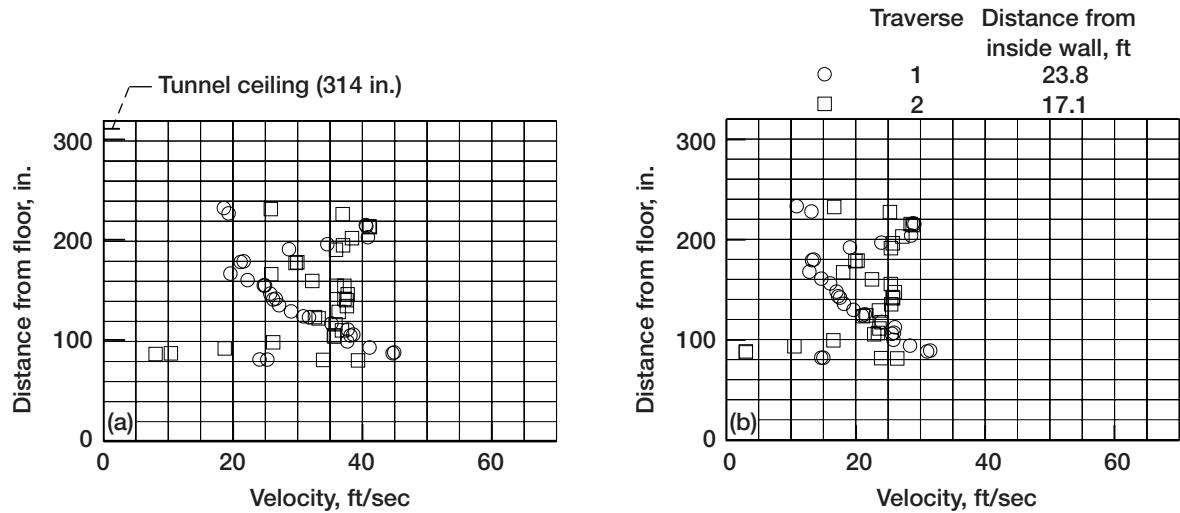


Figure 98.—Velocity distribution along vertical surveys downstream of heat exchanger (station 4) as measured by wind anemometers. Traverse 2 was directly downstream of heat exchanger element two, where exit guide vanes had been installed and deployed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

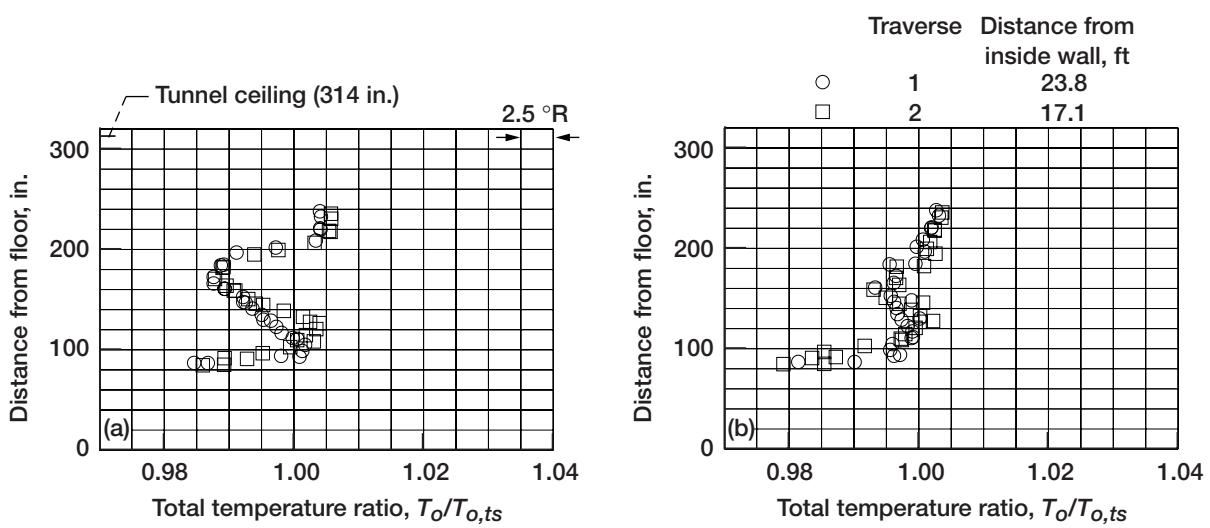


Figure 99.—Total temperature ratio distribution along vertical surveys downstream of heat exchanger (station 4) as measured by wind anemometers. Traverse 2 was directly downstream of heat exchanger element two, where exit guide vanes had been installed and deployed. (a) $V_{TS} = 350$ mph.
(b) $V_{TS} = 250$ mph.

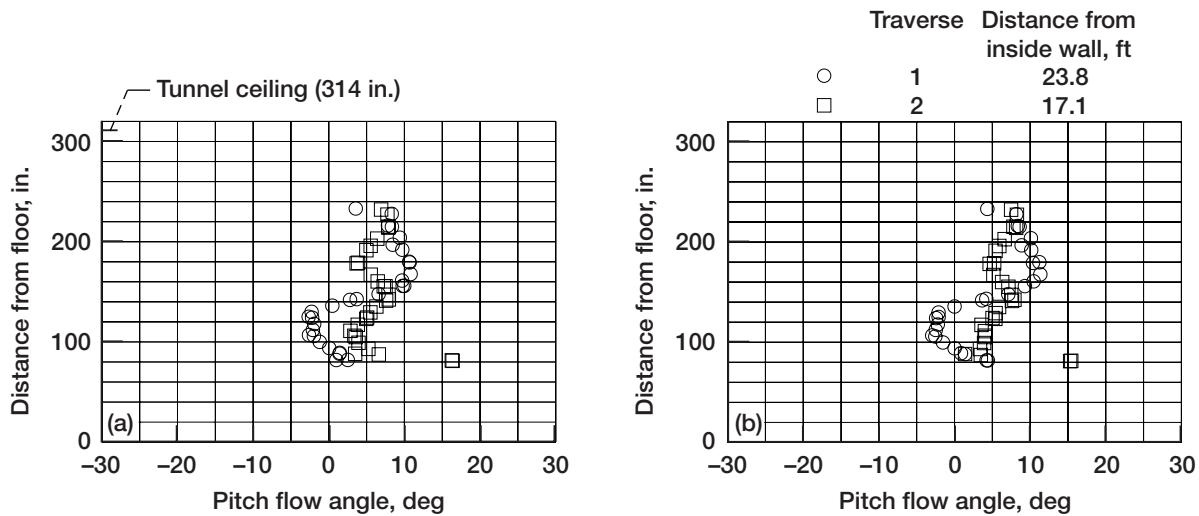


Figure 100.—Pitch flow angle distribution along vertical surveys downstream of heat exchanger (station 4). Traverse 2 was directly downstream of heat exchanger element two, where exit guide vanes had been installed and deployed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

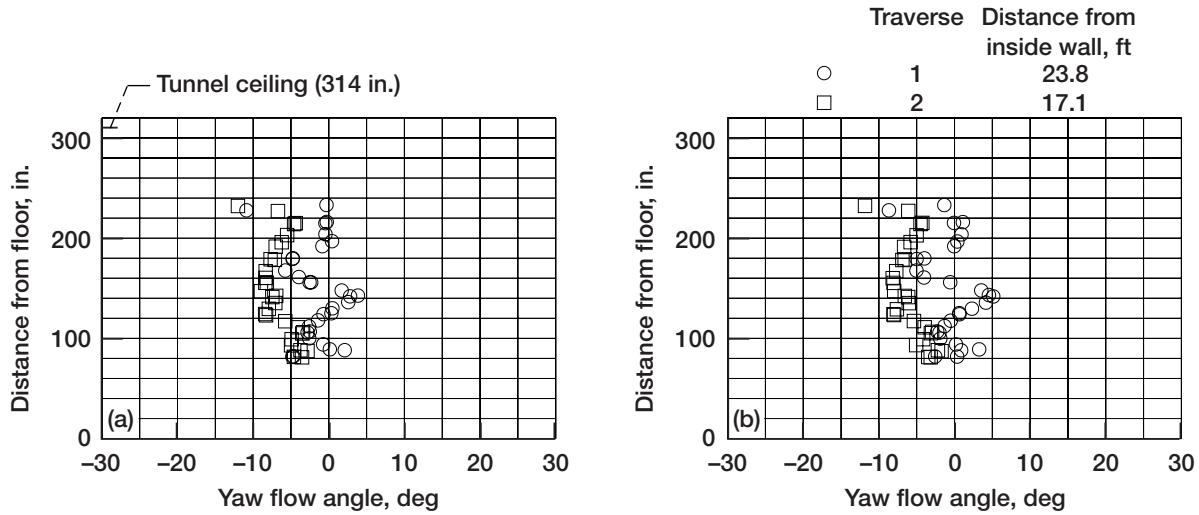


Figure 101.—Yaw flow angle distribution along vertical surveys downstream of heat exchanger (station 4). Traverse 2 was directly downstream of heat exchanger element two, where exit guide vanes had been installed and deployed. (a) $V_{TS} = 350$ mph. (b) $V_{TS} = 250$ mph.

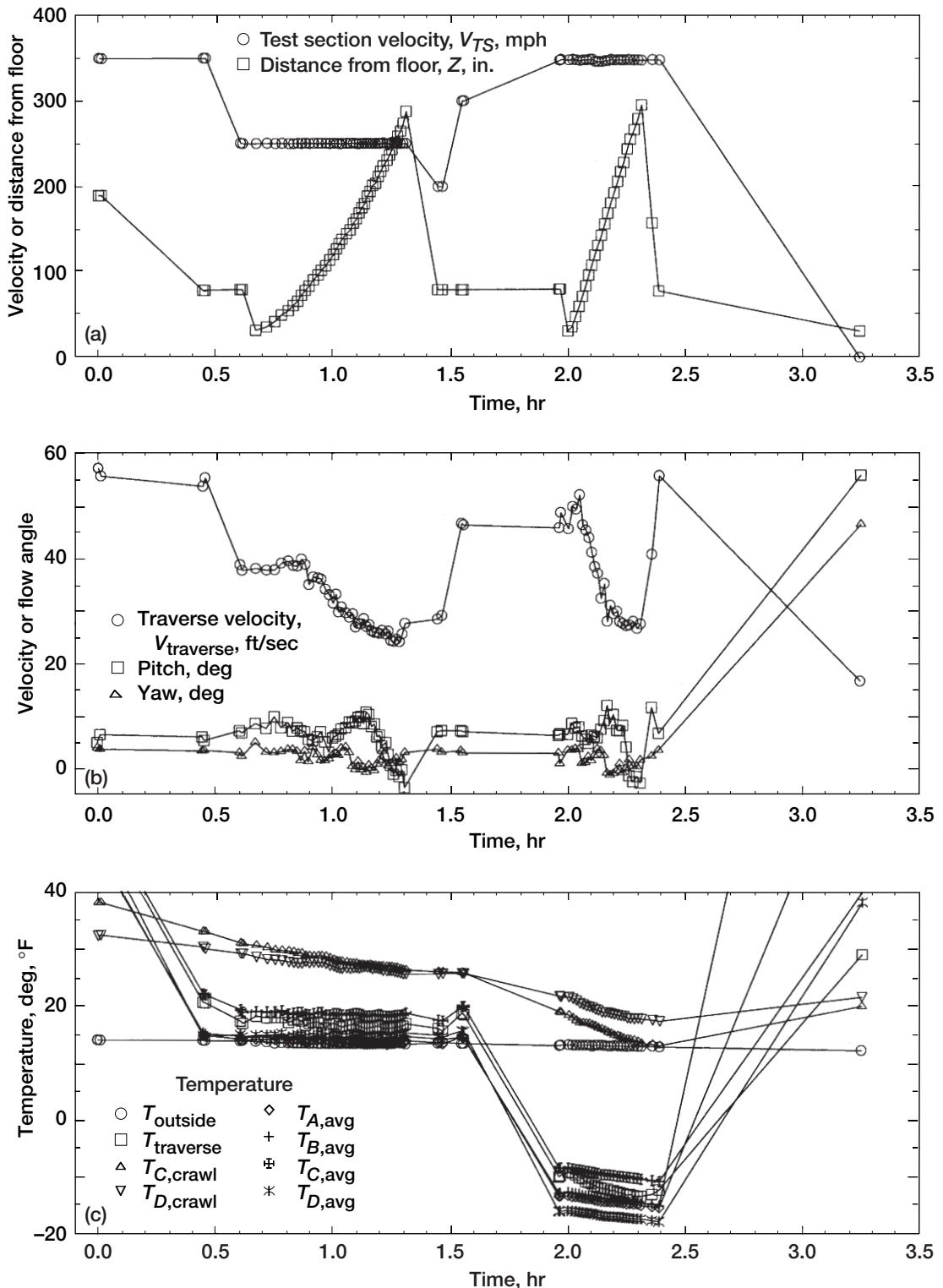


Figure 102.—Time histories. (a) Test section velocity and cable traverse position. (b) Air speed, pitch flow angle, and yaw flow angle measured by the wind anemometer on the cable traverse. (c) Air temperatures measured outside, near the cable traverse, in the crawl spaces, and in tunnel corners C and D.

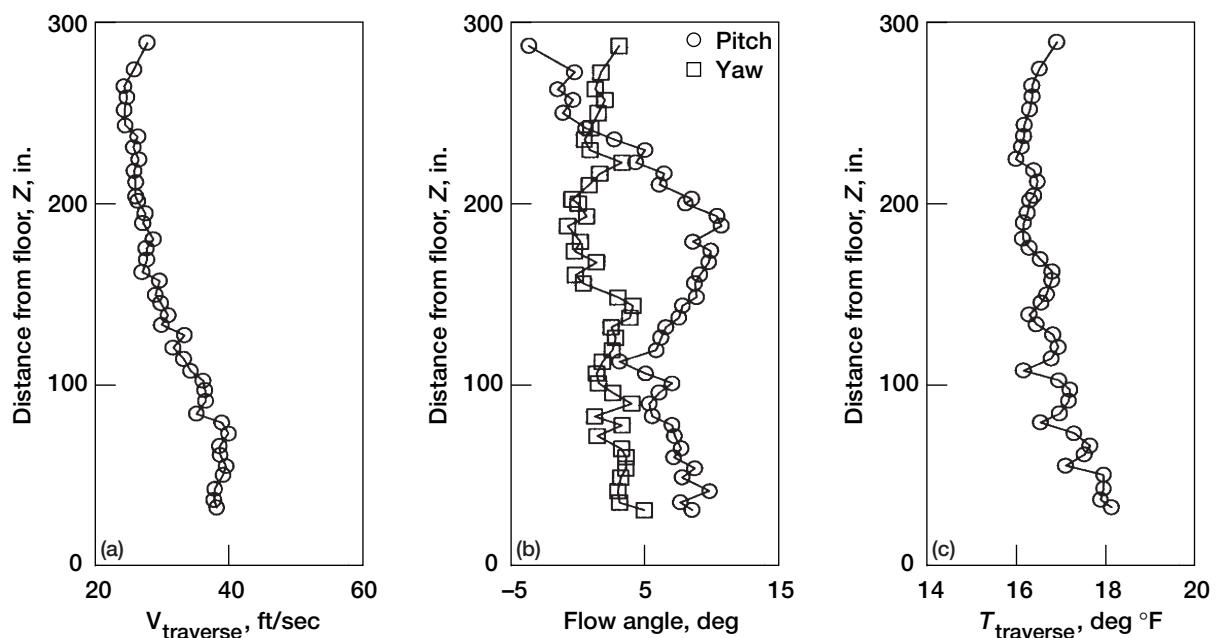


Figure 103.—Measurements made by the wind anemometer and thermocouple probes on the cable traverse for a test section air velocity, V_{TS} , of 250 mph and a tunnel total temperature $T_{D,\text{avg}}$, of 15 °F. (a) Air velocity. (b) Pitch and yaw flow angles. (c) Air temperature.

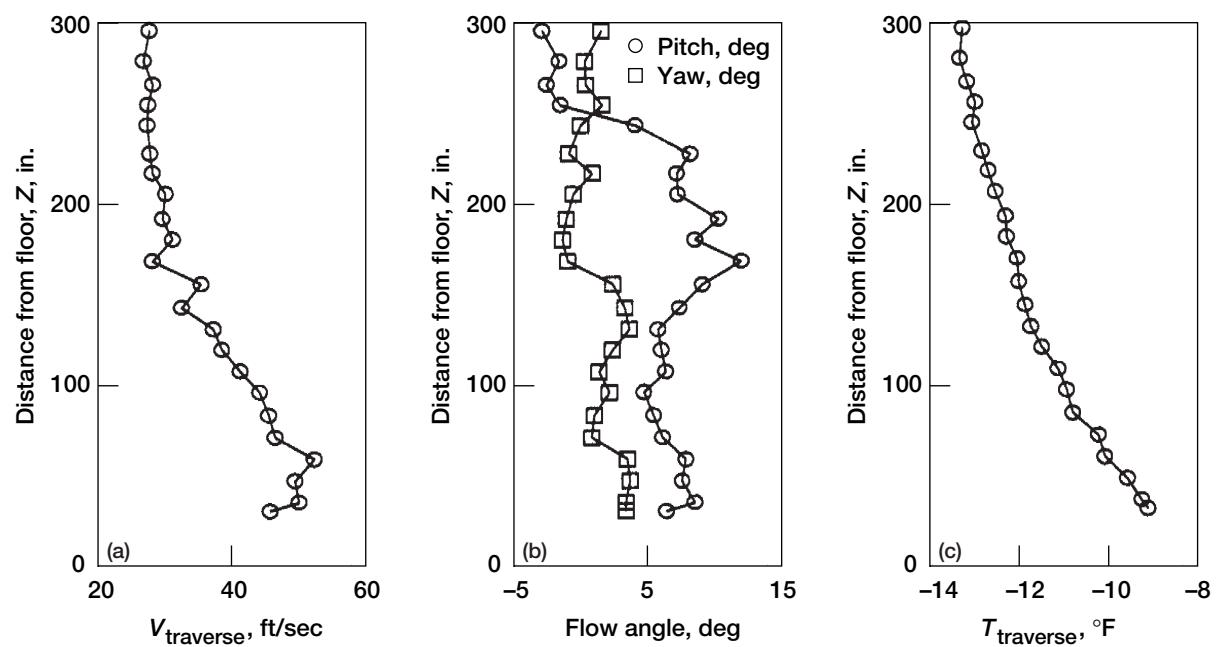


Figure 104.—Measurements made by the wind anemometer and thermocouple probes on the cable traverse for a test section air velocity, V_{TS} , of 350 mph and a tunnel total temperature $T_{D,\text{avg}}$, of 17 °F. (a) Air velocity. (b) Pitch and yaw flow angles. (c) Air temperature.

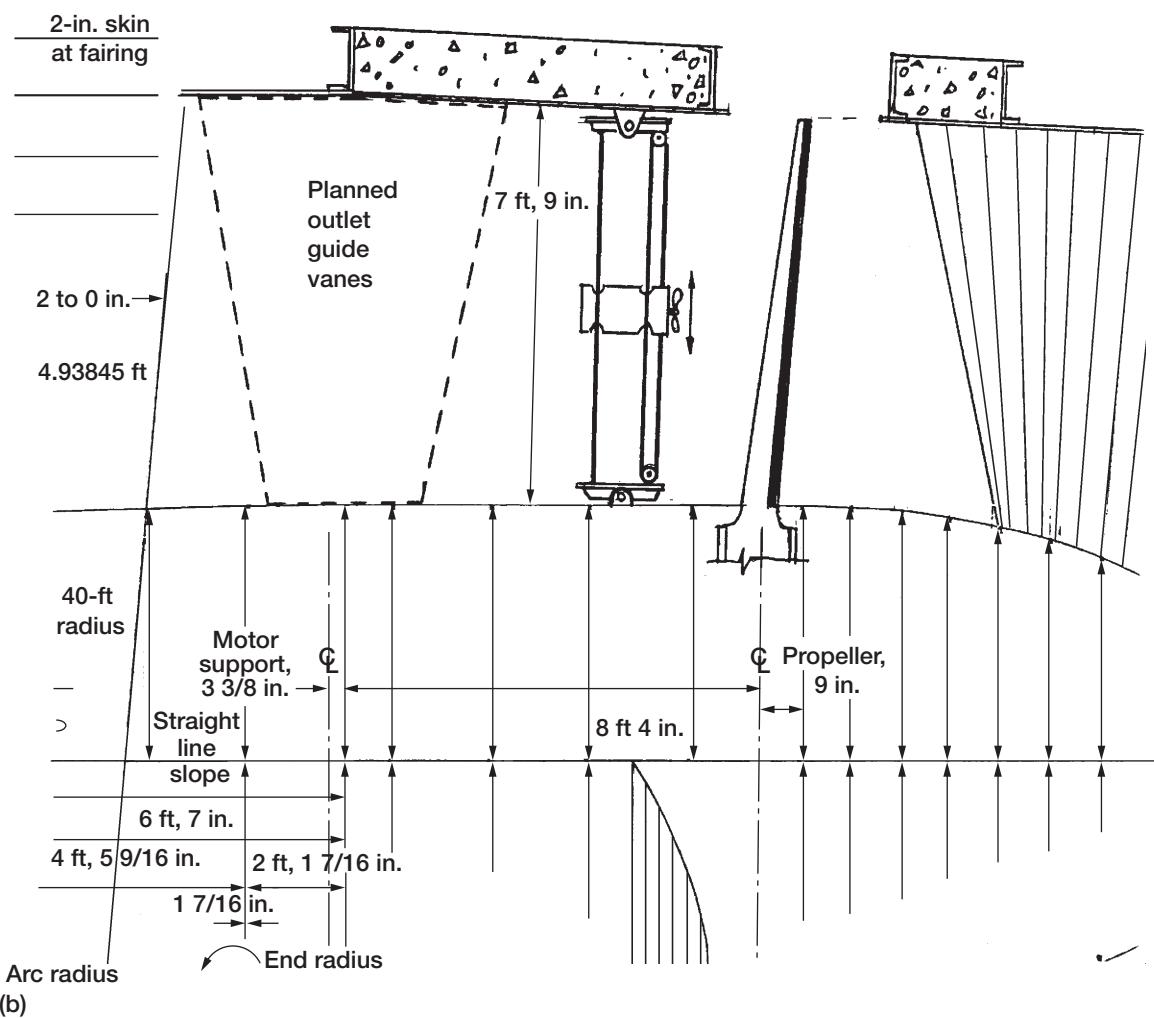
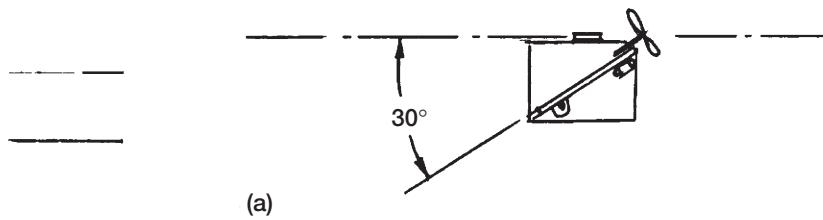


Figure 105.—Cable traverse installed at the IRT fan exit (Copyright David A. Spera; used with permission.)
(a) Top view. (b) Side view.

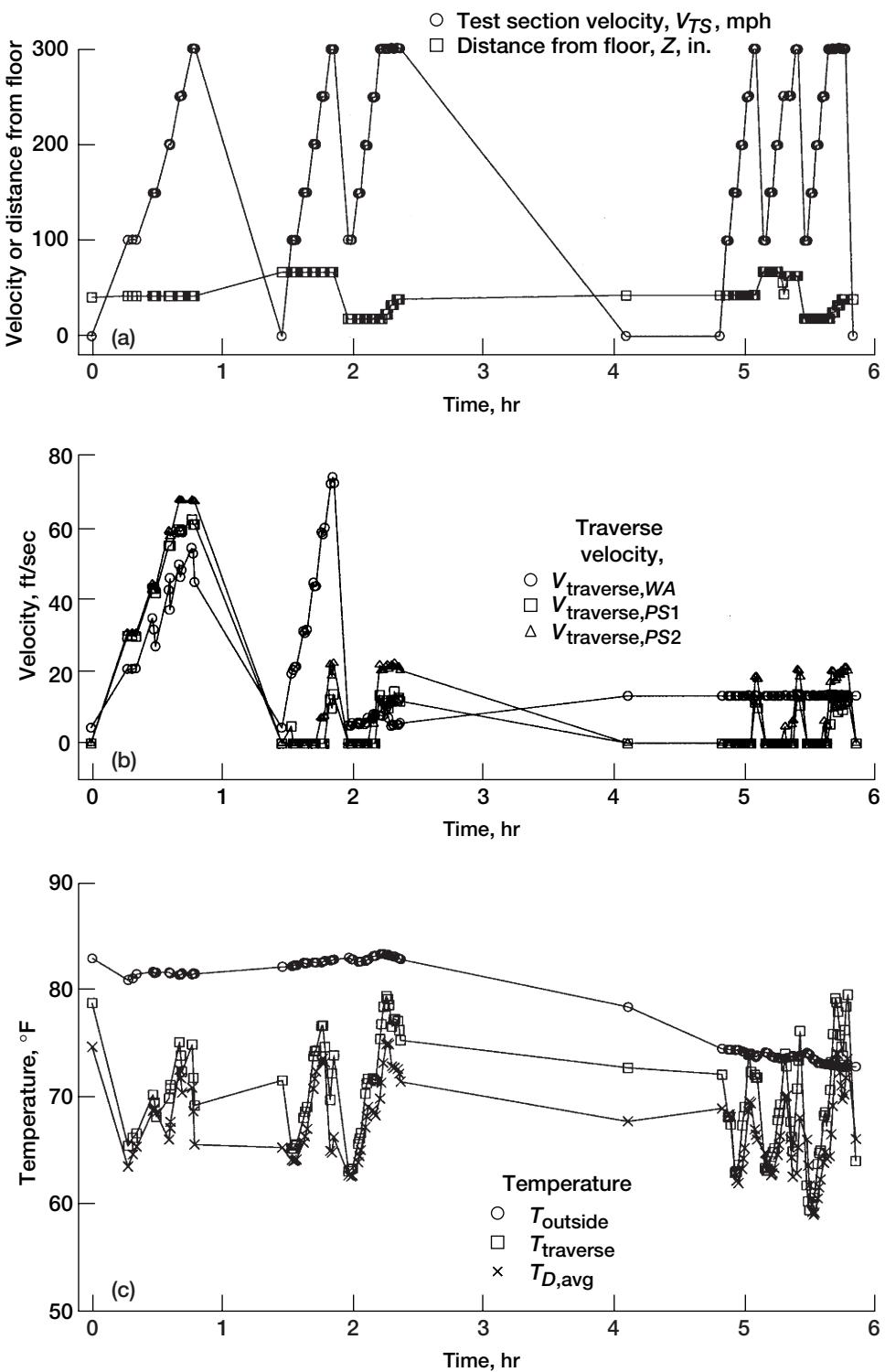


Figure 106.—Time histories. (a) Test section velocity, V_{TS} , and cable traverse position, Z .
 (b) Air velocity measured by the wind anemometer and the two traverse pitot-static probes.
 (c) Outside air temperature, cable traverse temperature, and corner D average temperature.

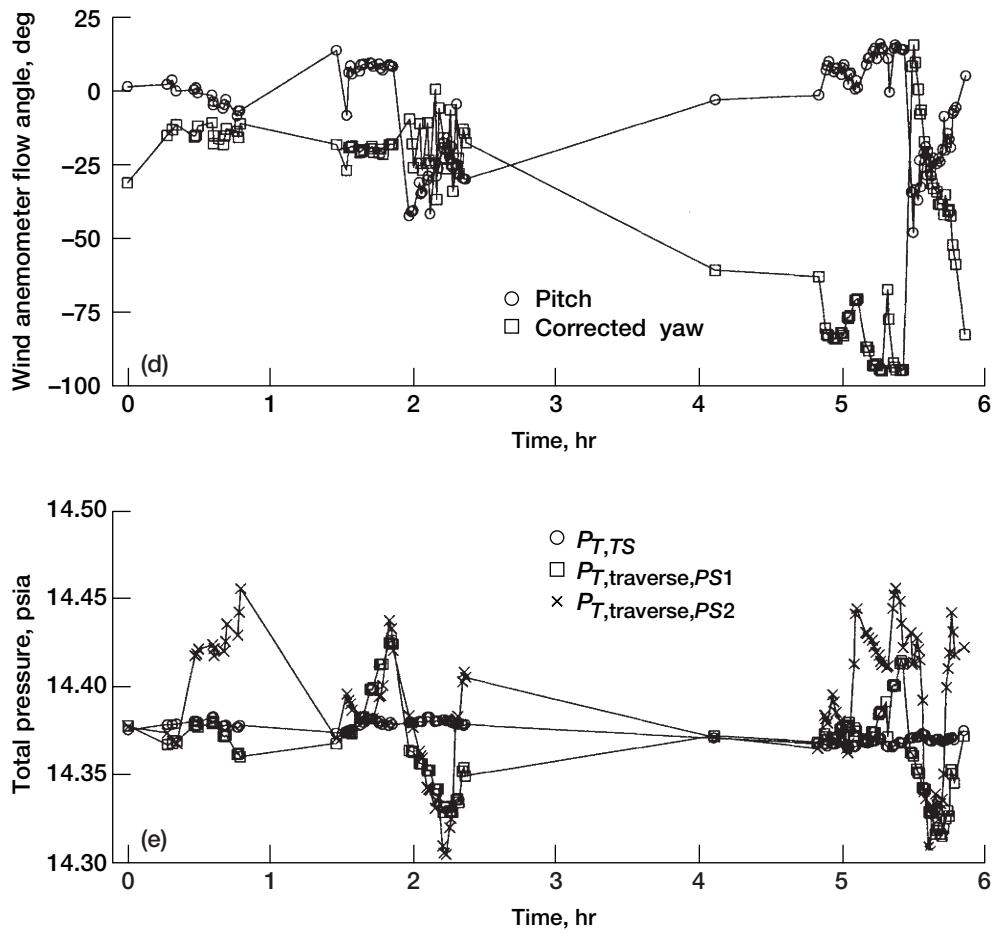


Figure 106.—Concluded. (d) Wind anemometer pitch and corrected yaw angle. (e) Total pressure measured in the test section and by the two traverse pitot-static probes.

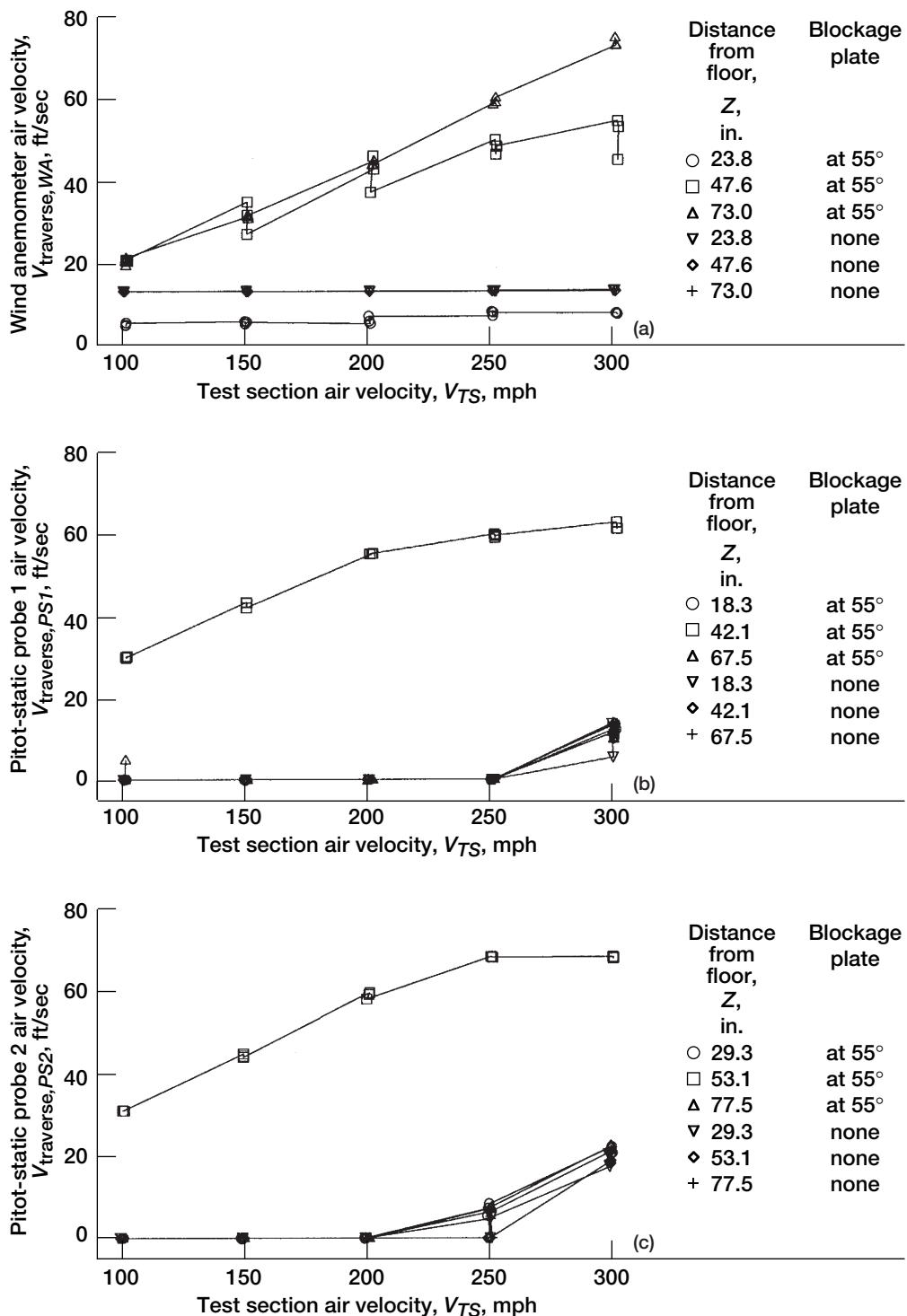


Figure 107.—Traverse air velocities downstream of the Icing Research Tunnel fan. (a) Measured by the wind anemometer. (b) Measured by pitot-static probe 1. (c) Measured by pitot-static probe 2.

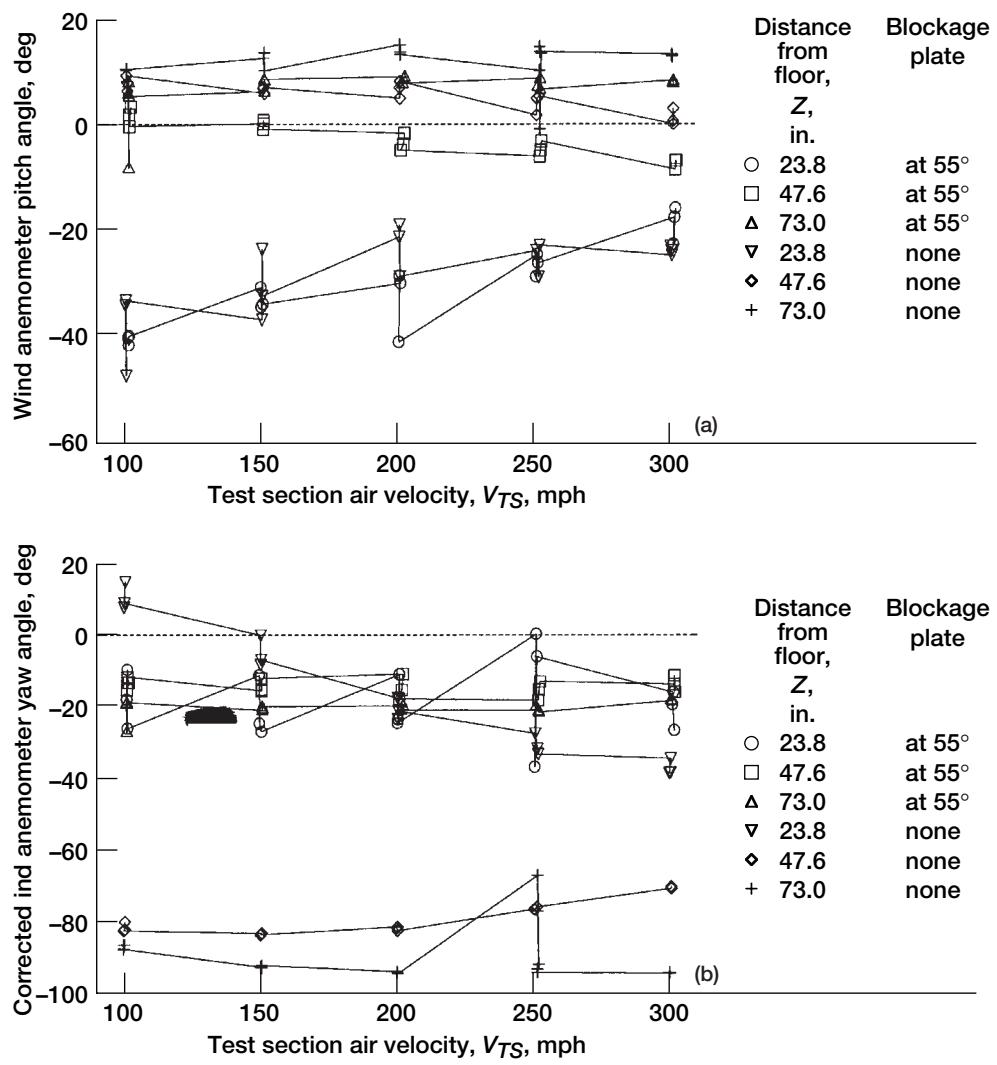


Figure 108.—Flow angles measured by the traverse wind anemometer downstream of the Icing Research Tunnel fan. (a) Pitch. (b) Corrected yaw.

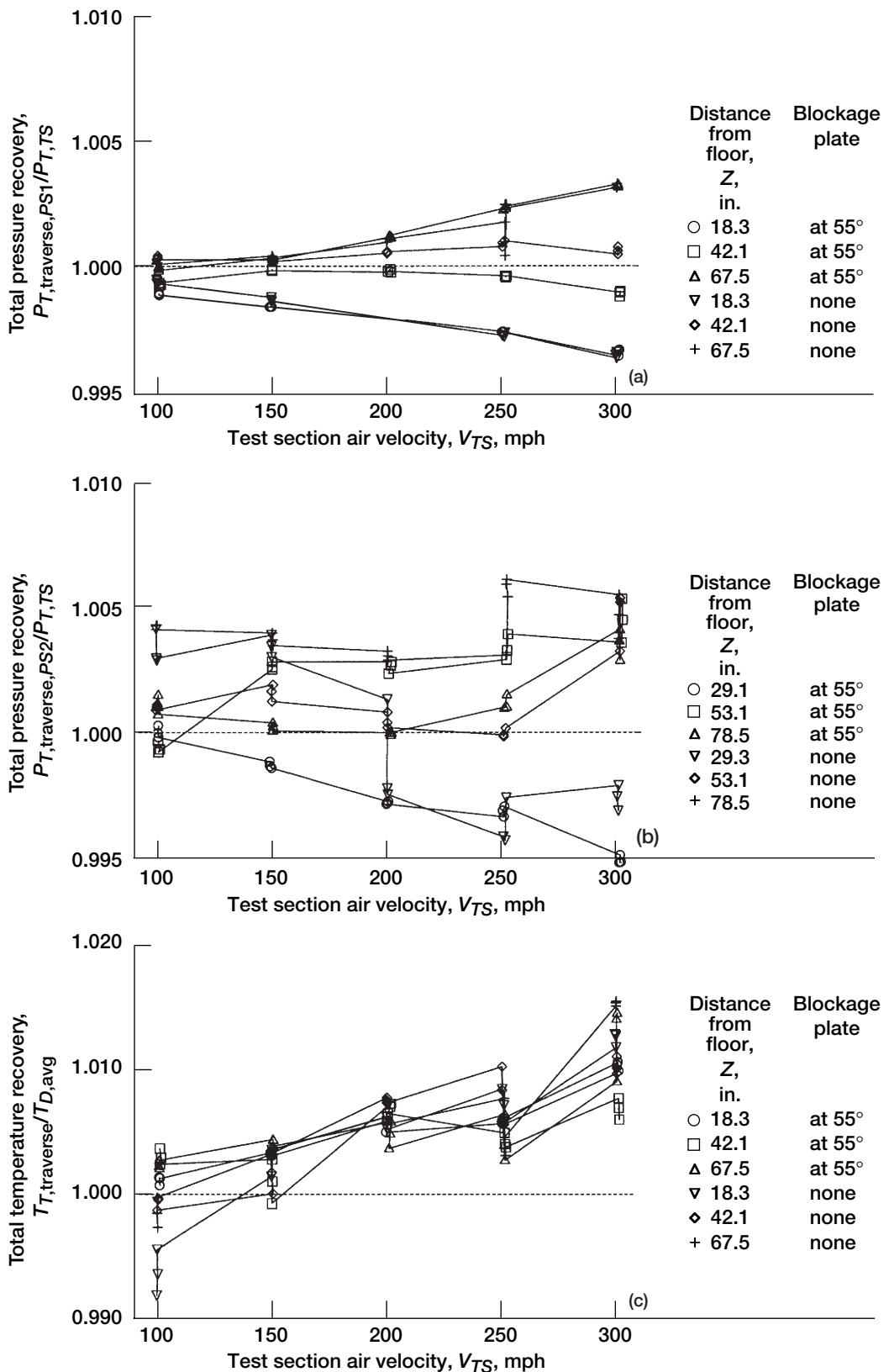


Figure 109.—Flow recoveries measured by traverse probe downstream of the Icing Research Tunnel fan. (a) Total pressure from pitot-static probe 1. (b) Total pressure from pitot-static probe 2. (c) Total temperature from thermocouple probe.

| REPORT DOCUMENTATION PAGE | | | <i>Form Approved OMB No. 0704-0188</i> |
|---|--|--|--|
| Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503. | | | |
| 1. AGENCY USE ONLY (Leave blank) | 2. REPORT DATE | 3. REPORT TYPE AND DATES COVERED | |
| | March 2000 | Technical Memorandum | |
| 4. TITLE AND SUBTITLE | | 5. FUNDING NUMBERS | |
| Flow Quality Studies of the NASA Glenn Research Center Icing Research Tunnel Circuit (1995 Tests) | | WU-523-90-1A-00 | |
| 6. AUTHOR(S) | | 7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) | |
| E. Allen Arrington, Jose C. Gonsalez, and Bonnie A. Kee-Bowling | | National Aeronautics and Space Administration John H. Glenn Research Center at Lewis Field Cleveland, Ohio 44135-3191 | |
| 8. PERFORMING ORGANIZATION REPORT NUMBER | | 9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) | |
| E-10767 | | National Aeronautics and Space Administration Washington, DC 20546-0001 | |
| 10. SPONSORING/MONITORING AGENCY REPORT NUMBER | | 11. SUPPLEMENTARY NOTES | |
| NASA TM—2000-107479 | | E. Allen Arrington and Jose C. Gonsalez, NYMA, Inc, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3-27186) (currently with Dynacs Engineering Company, Inc., 2001 Aerospace Parkway, Brook Park, Ohio 44142); Bonnie A. Kee-Bowling, NASA Lewis Research Center. Responsible person, E. Allen Arrington, organization code 2830, (216) 433-8507. (On March 1, 1999, the center was renamed the NASA John H. Glenn Research Center at Lewis Field.) | |
| 12a. DISTRIBUTION/AVAILABILITY STATEMENT | | 12b. DISTRIBUTION CODE | |
| Unclassified - Unlimited Subject Category: 09 | | Distribution: Nonstandard | |
| This publication is available from the NASA Center for AeroSpace Information, (301) 621-0390. | | | |
| 13. ABSTRACT (Maximum 200 words) | | | |
| The purpose of conducting the flow-field surveys described in this report was to more fully document the flow quality in several areas of the tunnel circuit in the NASA Glenn Research Center Icing Research Tunnel. The results from these surveys provide insight into areas of the tunnel that were known to exhibit poor flow quality characteristics and provide data that will be useful to the design of flow quality improvements and a new heat exchanger for the facility. An instrumented traversing mechanism was used to survey the flow field at several large cross sections of the tunnel loop over the entire speed range of the facility. Flow-field data were collected at five stations in the tunnel loop, including downstream of the fan drive motor housing, upstream and downstream of the heat exchanger, and upstream and downstream of the spraybars located in the settling chamber upstream of the test section. The data collected during these surveys greatly expanded the data base describing the flow quality in each of these areas. The new data matched closely the flow quality trends recorded from earlier tests. Data collected downstream of the heat exchanger and in the settling chamber showed how the configuration of the folded heat exchanger affected the pressure, velocity, and flow angle distributions in these areas. Smoke flow visualization was also used to qualitatively study the flow field in an area downstream of the drive fan and in the settling chamber/contraction section. | | | |
| 14. SUBJECT TERMS | | | 15. NUMBER OF PAGES |
| Wind tunnel; Flow quality | | | 171 |
| | | | 16. PRICE CODE |
| | | | A08 |
| 17. SECURITY CLASSIFICATION OF REPORT | 18. SECURITY CLASSIFICATION OF THIS PAGE | 19. SECURITY CLASSIFICATION OF ABSTRACT | 20. LIMITATION OF ABSTRACT |
| Unclassified | Unclassified | Unclassified | |